







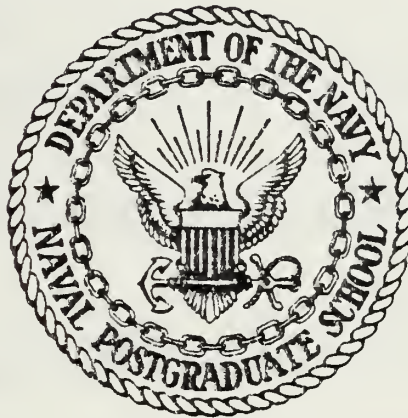






# NAVAL POSTGRADUATE SCHOOL

## Monterey, California



# THESIS

MULTIPLE TARGET IDENTIFICATION  
AND DIRECTION FINDING  
USING MATCHED FILTERING TECHNIQUES

by

James L. Johnston

December 1983

Thesis Advisor:

H. A. Titus

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Multiple Target Identification and Direction Finding  
Using Matched Filtering Techniques

by

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Submitted in partial fulfillment of the  
requirements for the degree of

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## ABSTRACT

This research investigates seismic signal processing techniques for battlefield target classification and acquisition. Multiple target classification is performed by discrete time domain matched filtering. Multiple target directions are determined using the responses of the matched filters and least mean squares polynomial curve fitting. The least mean squares polynomial curve fitting procedure is also used for direction finding for recoil/blast sources, using the unfiltered seismic signals.



## TABLE OF CONTENTS

I.	INTRODUCTION . . . . .	12
II.	THEORY OF SEISMIC SENSORS . . . . .	15
III.	DEVELOPMENTAL REQUIREMENTS AND PROBLEM DEFINITION . . . . .	18
	A. PASSIVE TARGET ACQUISITION AND SURVEILLANCE . . . . .	18
	B. CURRENT CAPABILITIES AND DEFICIENCIES . . . . .	20
IV.	MATCHED FILTER CONCEPT AND DISCRETE ALGORITHM . . . . .	21
	A. MATCHED FILTER THEORY . . . . .	21
	B. MATCHED FILTER ALGORITHM . . . . .	22
	C. MULTIPLE TARGET MATCHED FILTERING . . . . .	26
	D. COMPUTATIONAL REQUIREMENTS . . . . .	26
	E. SUPPORT SOFTWARE . . . . .	27
	1. Amplitude Analysis ( Timeout ) . . . . .	27
	2. Frequency Analysis ( Freqot ) . . . . .	28
	3. Simulation and Validation Software (SIMULT) . . . . .	31
V.	MULTIPLE TARGET DIRECTION . . . . .	34
	A. THEORY AND DESIGN CRITERION . . . . .	34
	B. MULTIPLE TARGET FILTERING ALGORITHM (MULTI) . . . . .	35
	1. Multiple Target Direction Phase Difference Algorithm . . . . .	37
	2. Least Mean Square Polynomial Direction Finding . . . . .	39
	3. Least Mean Squares Polynomial Algorithm Derivation . . . . .	41





4.	Adaptive Target Direction Finding . . . . .	44
5.	Software features of the Multiple Target Direction Routine . . . . .	44
C.	MULTIPLE TARGETS OF THE SAME TARGET CLASS . . .	45
VI.	ANALYSIS OF SEISMIC DATA . . . . .	47
VII.	CONCLUSIONS AND RECOMMENDATIONS . . . . .	116
	APPENDIX A: USERS MANUAL . . . . .	118
	APPENDIX B: SAMPLE INTERACTIVE PROGRAM SESSION . . . .	127
	APPENDIX C: PROGRAM LISTING . . . . .	132
	LIST OF REFERENCES . . . . .	168
	INITIAL DISTRIBUTION LIST . . . . .	169





## LIST OF TABLES

I.	Target Detection Radii . . . . .	19
II.	Test Plan for Simulated Data . . . . .	48
III.	Matched Filter for Simulated Targets . . . . .	48
IV.	Test Plan for Experimental Data . . . . .	49
V.	Matched Filter for Experimental Data . . . . .	49
VI.	Summary of Direction Finding Results . . . . .	50
VII.	Missed or Incorrectly Identified Targets . . . . .	51



## LIST OF FIGURES

4.1	Working Array Configuration . . . . .	24
4.2	Sample Matched Filter Output . . . . .	25
4.3	Windowing of Experimental Data . . . . .	26
4.4	Data Window Size vs Number of Operations . . . . .	28
4.5	Sample Amplitude versus Time Output . . . . .	29
4.6	Sample Frequency versus Power Output . . . . .	30
4.7	Simulation of a Zero Degree Target . . . . .	32
4.8	Sample Multiple Target and Simulated Target Output . . . . .	33
5.1	Two Target Matched Filter Response . . . . .	36
5.2	Circular Sensor Array Geometry . . . . .	38
5.3	Relative Delay Times in a Nine Sensor Ring . . . . .	40
5.4	Relative Time Delay versus Sensor Angle . . . . .	42
6.1	Sample Least Mean Squares Initial Direction for Event 001 . . . . .	52
6.2	Sample Matched Filter Response for Event 001 . . . . .	53
6.3	Sample Amplitude Response for Event 001 . . . . .	54
6.4	Sample Frequency Response for Event 001 . . . . .	55
6.5	LMSP Matched Filter Direction for Event 001 . . . . .	56
6.6	LMSP Multiple Target Direction Summary for Event 001 . . . . .	57
6.7	LMSP Matched Filter Direction for Event 001 . . . . .	58
6.8	LMSP Multiple Target Direction Summary for Event 001 . . . . .	59
6.9	LMSP Matched Filter Direction for Event 001 . . . . .	60
6.10	LMSP Multiple Target Direction Summary for Event 001 . . . . .	61
6.11	LMSP Matched Filter Direction for Event 001 . . . . .	62



6.12	LMSP Multiple Target Direction Summary for Event 001 . . . . .	63
6.13	LMSP Initial Direction for Event 383 . . . . .	64
6.14	Matched Filter Response for Event 383 . . . . .	65
6.15	Amplitude Response for Event 383 . . . . .	66
6.16	Frequency Response for Event 383 . . . . .	67
6.17	Fourth Degree LMSP Matched Filter Direction for Event 383 . . . . .	68
6.18	Second Degree LMSP Matched Filter Direction for Event 383 . . . . .	69
6.19	LMSP Multiple Target Direction Summary for Event 383 . . . . .	70
6.20	LMSP Initial Direction for Event 382 . . . . .	71
6.21	Matched Filter Response for Event 382 . . . . .	72
6.22	Amplitude Response for Event 382 . . . . .	73
6.23	Frequency Response for Event 382 . . . . .	74
6.24	LMSP Matched Filter Direction for Event 382 . .	75
6.25	LMSP Multiple Target Direction Summary for Event 382 . . . . .	76
6.26	LMSP Initial Direction for Event 372 . . . . .	77
6.27	Matched Filter Response for Event 372 . . . . .	78
6.28	Amplitude Response for Event 372 . . . . .	79
6.29	Amplitude Response of Malfunctioning Sensor for Event 372 . . . . .	80
6.30	Frequency Response for Event 372 . . . . .	81
6.31	LMSP Matched Filter Direction for Event 372 . .	82
6.32	LMSP Multiple Target Direction Summary for Event 372 . . . . .	83
6.33	LMSP Initial Direction for Event 375 . . . . .	84
6.34	Matched Filter Response for Event 375 . . . . .	85
6.35	Amplitude Response for Event 375 . . . . .	86
6.36	Amplitude Response of Malfunctioning Sensor for Event 375 . . . . .	87





6.37	Frequency Response for Event 375 . . . . .	88
6.38	LMSP Matched Filter Direction for Event 375 . .	89
6.39	LMSP Multiple Target Direction Summary for Event 375 . . . . .	90
6.40	LMSP Initial Direction for Event 374 . . . . .	91
6.41	Matched Filter Response for Event 374 . . . . .	92
6.42	Amplitude Response for Event 374 . . . . .	93
6.43	Amplitude Response of Malfunctioning Sensor for Event 374 . . . . .	94
6.44	Frequency Response for Event 374 . . . . .	95
6.45	LMSP Matched Filter Direction for Event 374 . .	96
6.46	LMSP Multiple Target Direction Summary for Event 374 . . . . .	97
6.47	LMSP Initial Direction for Event 302 . . . . .	98
6.48	Matched Filter Response for Event 302 . . . . .	99
6.49	Amplitude Response for Event 302 . . . . .	100
6.50	Frequency Response for Event 302 . . . . .	101
6.51	LMSP Matched Filter Direction for Event 302 .	102
6.52	LMSP Multiple Target Direction Summary for Event 302 . . . . .	103
6.53	LMSP Initial Direction for Event 354 (2 - 6sec) . . . . .	104
6.54	Matched Filter Response for Event 354 (2 - 6sec) . . . . .	105
6.55	Amplitude Response for Event 354 (2 - 6sec) .	106
6.56	Frequency Response for Event 354 (2 - 6sec) .	107
6.57	LMSP Matched Filter Direction for Event 354 (2 - 6sec) . . . . .	108
6.58	LMSP Multiple Target Direction Summary Event 354 (2 - 6sec) . . . . .	109
6.59	LMSP Initial Direction for Event 354 (7 - 11sec) . . . . .	110
6.60	Matched Filter Response for Event 354 (7 - 11sec) . . . . .	111



6.61	Amplitude Response for Event 354 (7 - 11sec) .	112
6.62	Frequency Response for Event 354 (7 - 11sec) .	113
6.63	LMSP Matched Filter Direction for Event 354 (7 - 11sec) . . . . .	114
6.64	LMSP Multiple Target Summary Event 354 (7 - 11sec) . . . . .	115



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## I. INTRODUCTION

Timely and accurate combat intelligence is a integral part of the modern battlefield. A primary goal of combat intelligence is target acquisition. Hostile targets can be acquired by either passive or active means. An example of passive target acquisition is visual target identification. Radar, on the other hand, is an active target acquisition device. An effective combat intelligence system will include a mix of both active and passive target acquisition methods.

Rapidly advancing technology in the fields of electronic counter-measures and radiation-seeking weapons has enhanced interest in passive target acquisition methods. To be cost effective, as an additional target acquisition system, a passive system must be able to provide swift and accurate target identification, location and tracking information on hostile targets. A variety of seismic sensor systems have been used in this roll with varying degrees of sucess.

Naval Ocean System Command (NOSC) in San Diego has developed a system based on a circular ring of sensors with data collection managed by an array-processor/minicomputer system [Ref. 1]. The observation of enemy movements and activity beyond the Forward Edge of the Battle Area (FEBA) is the design objective of this system. This thesis uses data collected during a test of this system at the Marine Corps Air-Ground Combat Center at Twenty-nine Palms, California. Investigated are various methods of processing the seismic data collected. The objective of this research is to try to provide viable methods of satisfying system design objectives through signal processing techniques.



The following chapter addresses the design objectives and requirements for such a seismic sensor system. Additionally, capabilities and deficiencies of current systems and research are detailed. In order to intelligently address solutions to these requirements and deficiencies, an understanding of seismic theory and sensors is needed. General seismic theory is presented with emphasis on the constraining parameters for the use of the earth's surface as a medium for gathering seismic intelligence. Also highlighted are the similarities of the earth's surface to electro/optical phenomena and the resulting simplifying assumptions.

The sequence of design solutions investigated followed from the analogies and simplifying assumptions addressed in the study of seismic sensor theory. The problem of target identification or classification is approached using digital matched filtering of the time domain amplitude data. Frequency domain matched filtering was not considered, based upon the conclusion by NOSC that there appeared to be no consistent spectral lines for any of the possible target types, except for artillery [Ref. 1]. Matched filtering was used to identify single and multiple target classes occurring during a sample period. The chapter detailing the matched filter procedures and implementation also includes a description of support and validation software used in the analysis of the seismic data.

The validation software is primarily used to check the accuracy of the direction finding routines. These direction finding routines are the time domain phase difference procedure (TDPD) and a least mean squares polynomial (LMSP) curve fitting procedure. The combining of the matched filtering procedure and these direction routines allowed for multiple target direction finding. The theory and derivations of the two direction finding algorithms are presented in the multiple target direction chapter.



Application of these algorithms is performed first on simulated targets for validation of the procedures. The experimental data is then analyzed. A user's manual, which includes procedures for tape and mass storage operations, is provided as an appendix. This appendix describes how to set up and use the software system.



## II. THEORY OF SEISMIC SENSORS

Elastic waves result from the stressing of an elastic media. The elastic media for seismic theory is the earth. Seismic theory is the study of the earth as a wave propagating media. Elastic waves propagate away from the source of seismic stress, e.g. an explosion [Ref. 2]. The energy, which propagates through the earth, travels via particle deformations. The elastic properties and densities of the earth media determine the velocities of these seismic waves. [Ref. 3]. Seismic wave sources of interest may be impulsive or continuous. Impulsive or short duration sources are artillery recoil or shell blasts. The time-limited nature of this type of seismic signal produces a broad range of frequencies. Continuous wave signals may be produced by tanks, trucks and low flying aircraft. These continuous wave signals may be described by narrow band frequency characteristics. The spectral power of a seismic source is a function of several parameters. A non-inclusive list of these parameters includes:

1. The vehicle's velocity and mass
2. The size of the explosive charge associated with the artillery or shell blast
3. The degree of coupling into the earth's surface
4. The geological structure over the wave's path

Information about the seismic source is contained in the waves which it generates. For example, in an array of seismic sensors, directional information is contained in the relative received signal phases. In otherwords, the relative phase differences between the signals received by the individual array elements can be used to compute the direction to the seismic source [Ref. 4]. These relative phase





differences represent the time delays of the waves as they pass the array's elements. The response of the array's elements is proportional to the amplitude and velocity of the earth's motion, relative to the geophone's sensing axis for the waves. [Ref. 3]

Assumptions about the propagation of seismic waves must be made to assist with their analysis. The earth is assumed to be made up of horizontal, homogeneous, and isotropic layers of material. These layers are assumed to be discontinuous in their elastic properties at their borders. This variance in the elasticity between the layers leads to an optical analogy for the wave propagation. Propagation paths may now be viewed as being direct, refracted, or reflected versions of the source's seismic waves. [Ref. 3]

There are four basic types of seismic waves. These types are compressional, shear, Love, and Rayleigh waves. Compressional waves are generated by impulsive sources such as shell blasts. Particle motion is along the direction of travel. Shear waves are characterized by particle motion orthogonal to the direction of motion. The Love wave is a surface wave which may occur as a result of the layering of the earth's surface. This layering effect acts as a wave guide for this type of wave. Particle motion is orthogonal to the direction of wave propagation. The Rayleigh wave is generally the strongest of the seismic waves. The Rayleigh wave travels along the free surface of the earth. Its particle motion direction is always in the vertical direction. It is the strongest wave generated by a compressional source. Its amplitude attenuates at a rate only inversely proportional to the square root of the distance. [Ref. 3]

The waves of primary interest for a seismic system are the Rayleigh and Love waves. This is due to the long-range propagation of these waves. Since these two wave types are orthogonal to each other, they must be sensed by different



geophones. Rayleigh waves may be sensed by vertical geophones and the Love waves by horizontal geophones. Since the Rayleigh wave is normally the strongest, and in order to reduce computational complexity, only verticle sensor data is used.

Rayleigh waves experience absorbtion losses, particularly at higher frequencies. This phenomenon occurs because of the lowpass filter effect of the earth. This filtering effect is further compounded due to the fact that the cutoff frequency of the earth diminishes with range. Further complications arise due to the dependence of wave velocity on frequency. The result being that the wave train may change with distance, reducing the correlation of the wave shape between its source and distant points. Other sources of error occur because of the weathering of the surface layer, irregularities in the sub-surface composition, variances in the earth's layers and surface geometry. [Ref. 3]



### III. DEVELOPMENTAL REQUIREMENTS AND PROBLEM DEFINITION

#### **A. PASSIVE TARGET ACQUISITION AND SURVEILLANCE**

A battlefield commander possesses a definite requirement for real time combat intelligence. A significant tactical advantage is held by the commander who is able to integrate his available combat intelligence sources with his supporting arms, i.e., target acquisition and engagement. It follows that to be part of the target acquisition process, any real time, seismic sensing system must provide swift and accurate information on detected enemy targets. The specific requirements for such a system are the ability to detect, identify, and locate these targets [Ref. 5]. Additionally, the target's rate and direction of movement should be provided or made easily discernible.

Any seismic sensing system must be designed around the target acquisition cycle. The target acquisition cycle, as given by Dublin [Ref. 5], is as follows:

1. Search Time
2. Target Sensing
3. Information Processing
4. Display of Target Information
5. Analysis of Target Information
6. Time required to make a Decision
7. Time Required for Supporting Weapons to Respond

For a seismic system, a prioritized list of possible targets are as follows:

1. Artillery
2. Helicopters and Aircraft
3. Tracked and Wheeled Vehicles
4. Personnel





As may be expected, the relative amplitudes of these seismic targets vary widely. A seismic targeting system is therefore constrained as to the targets it can or can not be expected to effectively engage.

The variance in the relative amplitudes of seismic targets suggests a range of specifications for detection of these targets. As summarized by Dublin [Ref. 5], possible detection radii may be as shown in Table I. Radii are given for both short and long targeting systems.

**TABLE I**  
**Target Detection Radii**

<u>Target</u>	<u>Short Range System</u>	<u>Long Range System</u>
Personnel	100 M	None
Vehicles	1KM	10-20KM
Low Flying Aircraft	1KM	10-20KM
Hostile Weapons	1KM	15-20KM

The timeliness requirement is ancillary to the radii of detection specifications. Timeliness, as used here, refers to the total time commencing when the seismic sensor system first detects and processes the seismic target data and ending with the dissemination of the targeting information to command elements for disposition. This timeliness requirement ranges between five to fifteen minutes, depending upon the mobility of the target [Ref. 5].

The parameters having a direct effect on the timeliness of a system are the probabilities of false alarm and detection. These parameters directly relate to a system's value. Increased probability of detection with reasonable false alarm performance, combined with the ability to disregard



friendly targets, are practical design objectives for any targeting system. The ability to incorporate such design features into a seismic sensor system will reduce both the time wasted on invalid targets and the danger of undetected targets.

Once a valid target has been detected, target location information must be obtained. Stringent specifications for target locations allow for the system to support or enhance the effectiveness of; fire support systems, blind bombing, Harassing and Interdiction fire (H and I), and observerless artillery engagement.

## B. CURRENT CAPABILITIES AND DEFICIENCIES

To date, numerous successful algorithms have been developed to determine direction to single targets. These algorithms include both time and frequency domain methods. Target identification of long range targets via seismic sensing has not yet met with equal success.

The modern battlefield is seldom a single target type environment. The complicated, real world problems of multiple target identification and multiple target engagement require solution before practical seismic sensor systems can be integrated into the target acquisition process.



#### IV. MATCHED FILTER CONCEPT AND DISCRETE ALGORITHM

##### A. MATCHED FILTER THEORY

As previously addressed, there exists a requirement for battlefield target identification/classification. The recovery and classification of target signals suggests a filtering requirement. Previous works and implementations have used frequency domain techniques [Ref. 4]. The Air Force's SKEET system and the U.S Army's Remote Battlefield Surveillance System (REMBASS) both have successfully implemented a spectral power approach for classification of seismic data. These systems, however, are for short range applications. Time domain approaches to target identification have been for the most part left unexplored.

The discrete matched filtering technique is an attempt to classify targets by their time domain amplitude pattern i.e., their seismic amplitude signature. The heuristic basis for this method evolved from the observation of visual differences between the amplitude versus time signals for the various classes of targets. The matched filter, being the optimum filter for detecting known signals, was selected [Ref. 6].

The discrete matched filter is described by equation 4.1, where  $h(t)$  is the impulse response of a filter whose output signal to noise ratio at time  $t_0$  is maximized. The unit step  $u(t)$  has been added to assure causality for the system. The matched filter is [Ref. 7].

$$h(t) = s(t_0 - t)u(t) \quad (4.1)$$



The output signal is given by

$$s_{out} = \int_{-\infty}^{\infty} h(v) s(t - v) dv \quad (4.2)$$

The maximum signal to noise ratio is given by

$$(s_{out}^2/M^2)_{maxoutput} = E(t_0)/N_0 \quad (4.3)$$

Where  $M$  is the noise level at the filter output,  $N$  is the input noise level, and  $E(t_0)$  is the energy in  $s(t)$  up to time  $t_0$ . In equation 4.2, the replica of the original known signal is reversed and translated in time to be convolved with the signal input to the filter, producing the optimum output signal to noise ratio.

For discrete realization of the matched filter as implemented, equation 4.2 becomes equation 4.4, where  $h(k)$  is the reflected and translated known signal.

$$s_{out}(j) = \sum_{k=1}^N h(k) s(j - k) \quad (4.4)$$

Where  $N$  is the number of data points per sample period.

## B. MATCHED FILTER ALGORITHM

Samples of known signals are stored in a data file and read into a 5120 array at the start of program execution. Five sample, or known filter signals, are recorded in this array. Each sample signal comprises 1024 of the 5120





elements of the matched filter array. To perform the matched filtering, the 1024 seismic data samples (unknown signal) are copied over five times on an array of 11264 size. These copies of the experimental data are separated by 1024 zeros on either side. Additionally, the leading and trailing elements of the experimental data are set to zero to eliminate switching spikes present in the data. Hence forth, this 11264 element array will be referred to as the working array for brevity. This working array will contain the results of the matched filtering. For M, given as the number of input signal and filter signal array elements and also the number of zeros, the requirement set forth in [Ref. 8] for nonoverlapping convolution of length L is satisfied. Equation 4.5 establishes the minimum length for nonoverlapping convolution of one matched filter segment.

$$L = 2M - 1 \quad (4.5)$$

Figure 4.1 depicts the working array layout. Notice that the first filter signal, "Tracked Vehicle" is loaded into the h(t) array and is convoluted with the working array elements one through 2048. Once the leading data point of h(t) reaches the working array's element 2048, a new known signal is loaded into h(t), "Wheeled Vehicle", and the convolution is continued for working array elements 2048 to 4096. This process continues until the last of the five h(t) filter signals has been read in and the convolution has been performed on all copies of the data. Notice that working data array elements 10240 to 11264 are for array length over-run protection.

Prior to convolution, each filter sample signal and the input signal are equalized to the same power level through



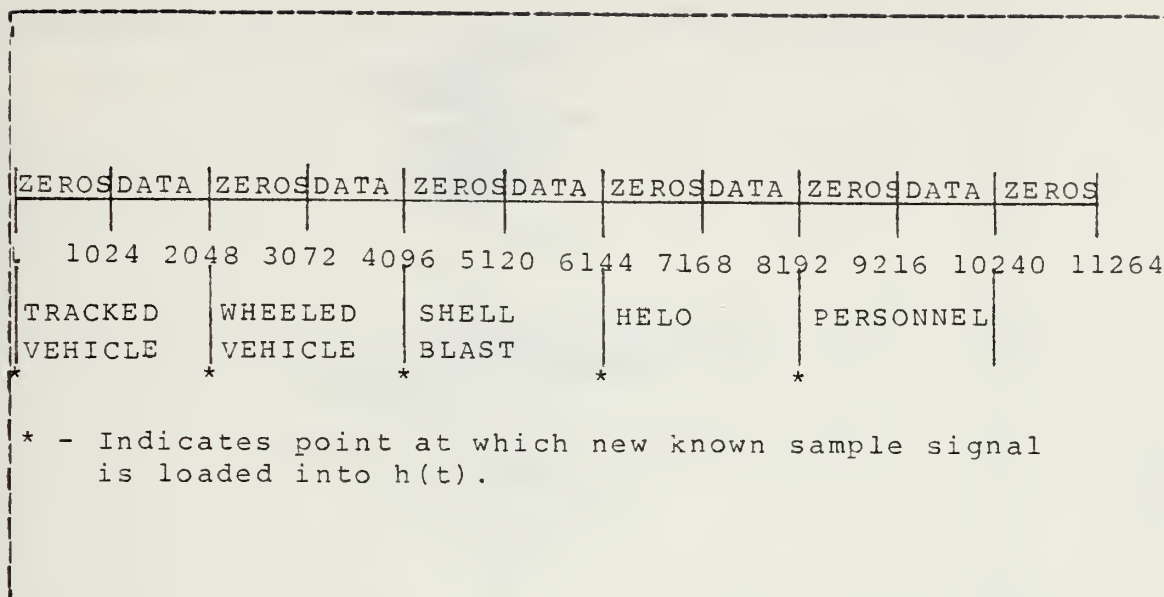


Figure 4.1 Working Array Configuration

division by their respective root mean square values. Additionally, after the convolution, the entire working array is normalized with respect to its maximum amplitude element. The maximum value in each target classification section is then compared with the interactively selected matched filter threshold. If the section's peak value is above the threshold value, that class of target is declared to be present. This method allows for the simultaneous detection and classification of multiple targets. It should be noted that this equalization forces both high and low amplitude signals to an equivalent average power level. This is felt to be justified in that signal amplification is not the goal, rather target detection and classification is. In the case of a single target, the known signal that most closely matches the unknown signal is anticipated to have the greatest amplitude matched filter spike. Figure 4.2 is a sample output.



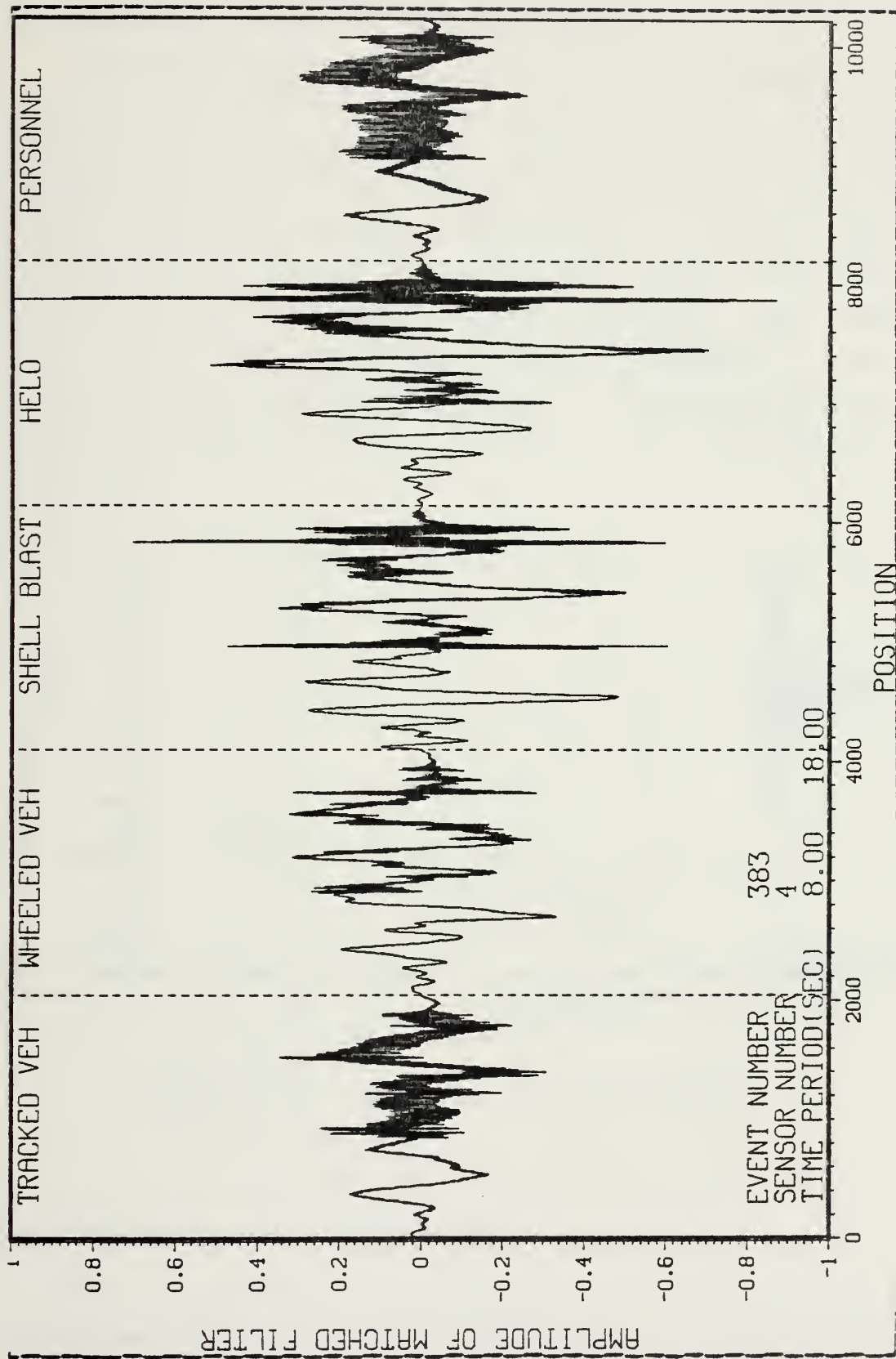


Figure 4.2 Sample Matched Filter Output



### C. MULTIPLE TARGET MATCHED FILTERING

The upper limit of equation 4.4 may be selected to be from one to 1024 when called by the multiple target direction routine. This allows for the selection of reduced program execution times. Target identification, however, is always made by the full 1024 element buffer. When the matched filter target identification routine is used by the multiple target direction finding routine, data windows of less than 1024 are formed from a segment of the 1024 elements by extracting the segment size required around the maximum signal value. Figure 4.3 illustrates this procedure.

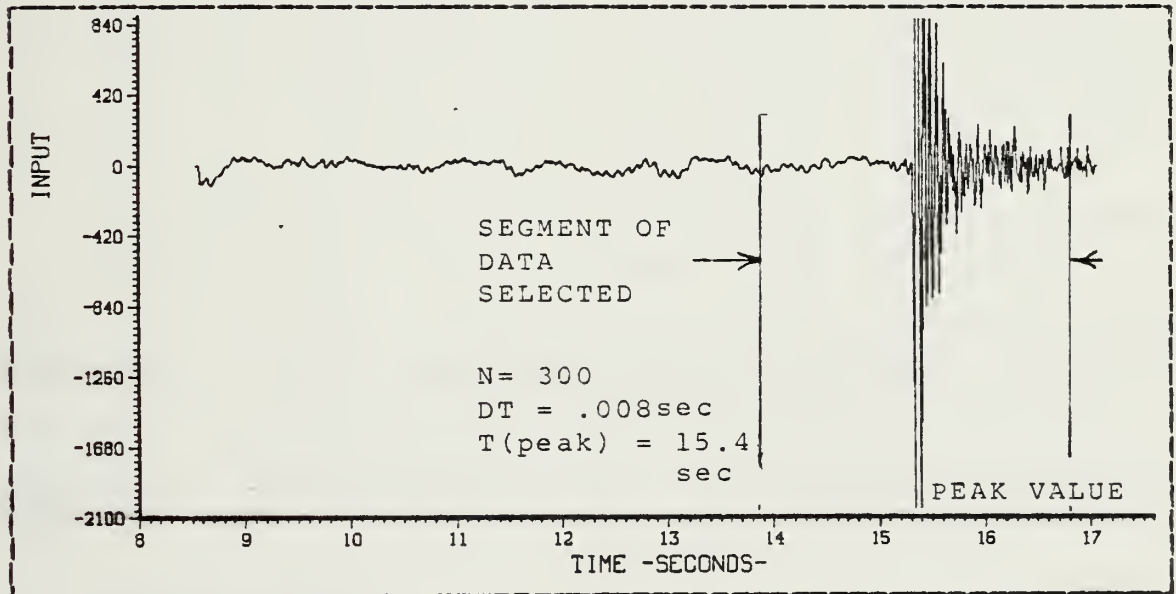


Figure 4.3 Windowing of Experimental Data

### D. COMPUTATIONAL REQUIREMENTS

The computational requirements for this procedure are described by equation 4.6, where  $N_0$  is the total number of operations required by the matched filter routine.





$$NO = (Ndf^2)(Nc) + (Ndf - 1)(Ndf)(Nc) \quad (4.6)$$

Ndf is the number of data elements and also the number of filter elements. Nc is the total number of target classes. The term  $Ndf^2Nc$  is the total number of multiplications required, while  $(Ndf - 1)NdfNc$  is the total number of additions.

When used for target identification, Ndf equals 1024 and Nc equals five. Equation 4.6 gives a total of 10,480,640 operations for these array sizes. When the matched filter routine is initiated by the multiple target direction routine, the value of Ndf can be selected to range from one to 1024. Figure 4.4 is a plot of equation 4.6 and shows the computational consequence for selection of large values for Ndf. Note that equation 4.6 must be multiplied by the number of sensors in the ring when computing the number of operations for the multiple direction routine.

Window sizes of 100 and 200 were found to provide acceptable accuracy with greatly reduced computation times. As shown by figure 4.4, a window size of 200 requires 399,000 operations, while a window size of 100 requires only 99,500 operations. The number of operations required was found, as expected, to be proportional to the execution time of this routine.

## E. SUPPORT SOFTWARE

### 1. Amplitude Analysis ( Timeout )

A graphical output is provided by this amplitude routine which displays the relative amplitude versus time for a selected sensor. The initial target direction and target classifications found are also displayed. This routine allows for the interactive selection of the



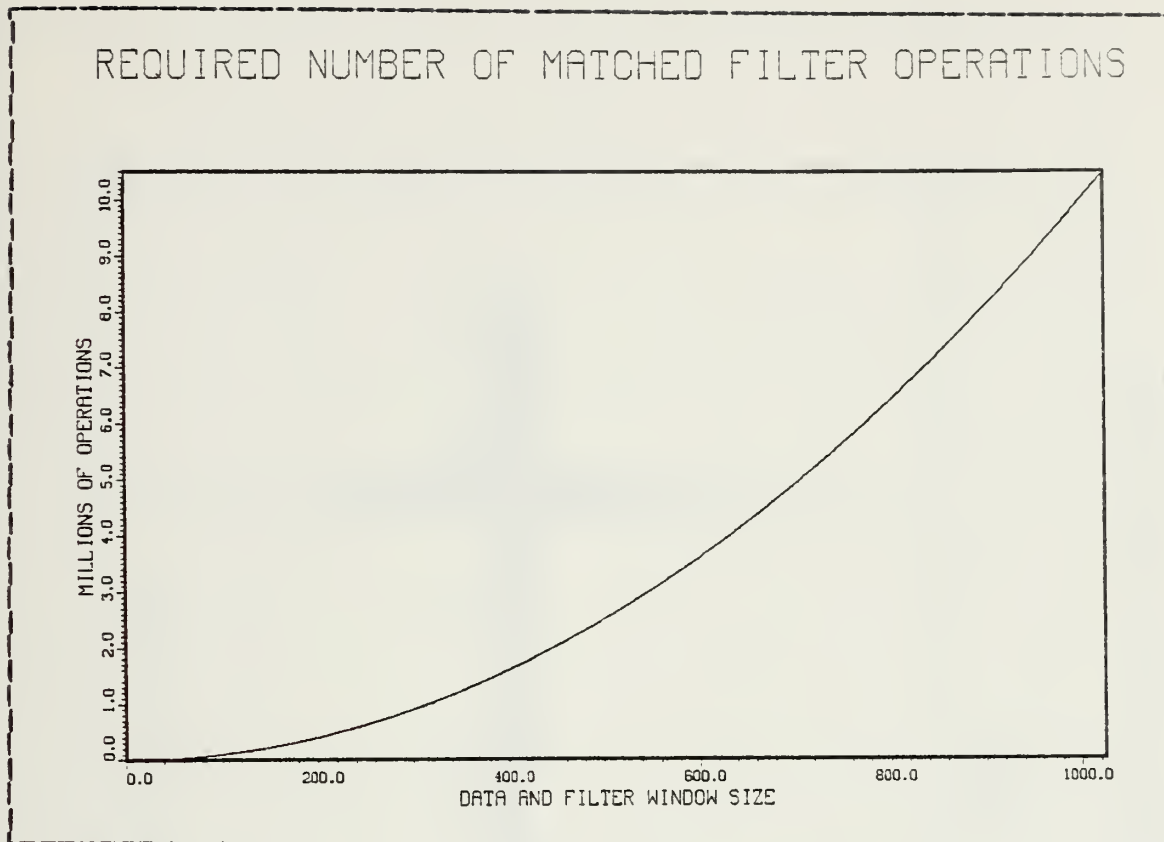


Figure 4.4 Data Window Size vs Number of Operations

amplitude response of any sensor as a sample target for later use in the matched filter analysis. In this way sample, signals can be catalogued and evaluated as filter signals. The axes of the graphical output adapts to the data's maximum amplitude and to the time period involved. Figure 4.5 is an example of amplitude analysis output.

## 2. Frequency Analysis ( Freqot )

The frequency routine, as in the amplitude analysis routine, allows for initial primary target direction, target classifications, and for the time period of the experimental data to be displayed. Normalized spectral power versus frequency is graphically displayed as shown in figure 4.6.



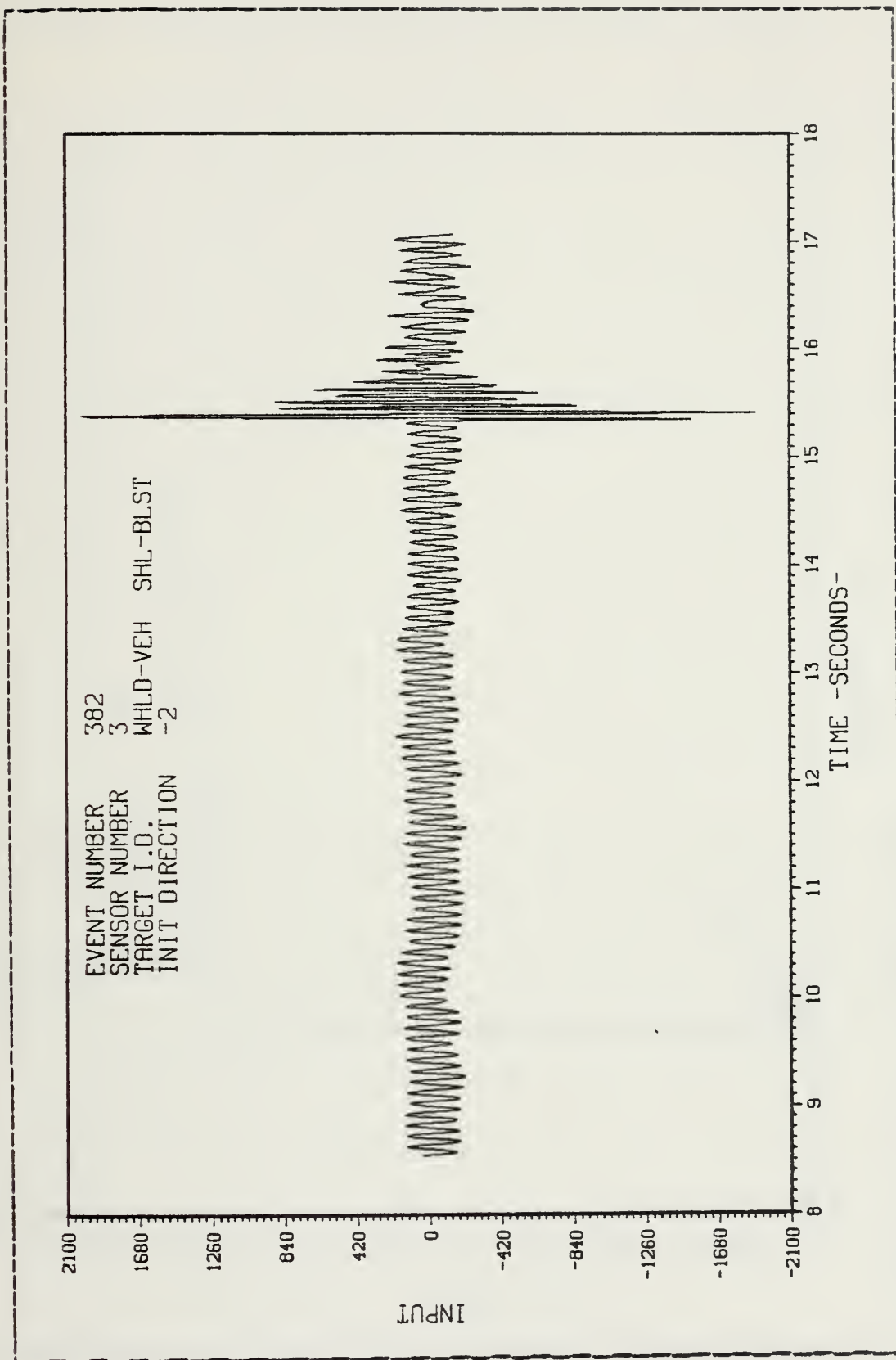


Figure 4.5 Sample Amplitude versus Time Output



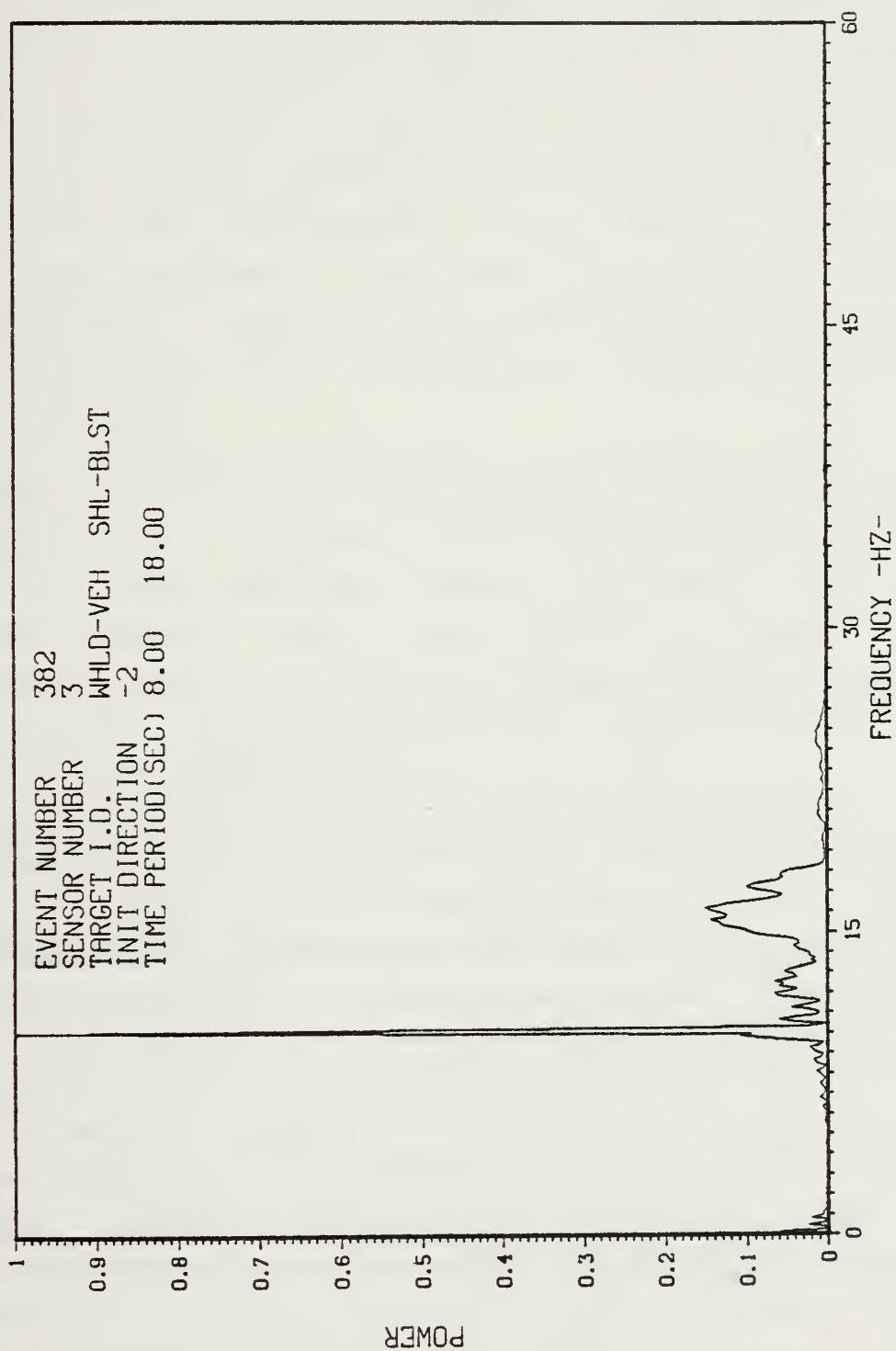


Figure 4.6 Sample Frequency versus Power Output





### 3. Simulation and Validation Software (SIMULT)

In order to validate the various algorithms and their implementation in software, a testing procedure was required. The specific algorithms which the simulation routine was designed to validate are the initial angle, phase difference and least mean square target direction routines. These routines, as previously described, use the relative time differences of the seismic signal's peak amplitude response or the peak matched filter response respectively. Validation of these routines is performed by allowing the creation of simulated targets with selected arrival angles.

Simulated targets can be created in the routine SIMULT. Up to four sine wave targets of selected frequency, amplitude, and direction can be input during each sample period. These simulated targets are added to the experimental seismic signal data for the sample period. Correspondingly, zero direction filter data must have been written into the matched filter data file at these selected sample target frequencies.

The directions for the simulated targets are created by introducing relative phase delays between the sine waves that are added to each sensor's seismic data. This is implemented by introducing a zero phase to the sensor in the desired direction of the simulated target. The phases of the other sensors are increased proportionally by their distance on the circular array away from the zero phase shift sensor. Figure 4.7 illustrates the case of a zero degree simulated target direction.

A summary of the target directions found by the multiple target direction routine and the simulated targets entered is provided by the multiple direction plotting routine. Figure 4.8 is a sample output.



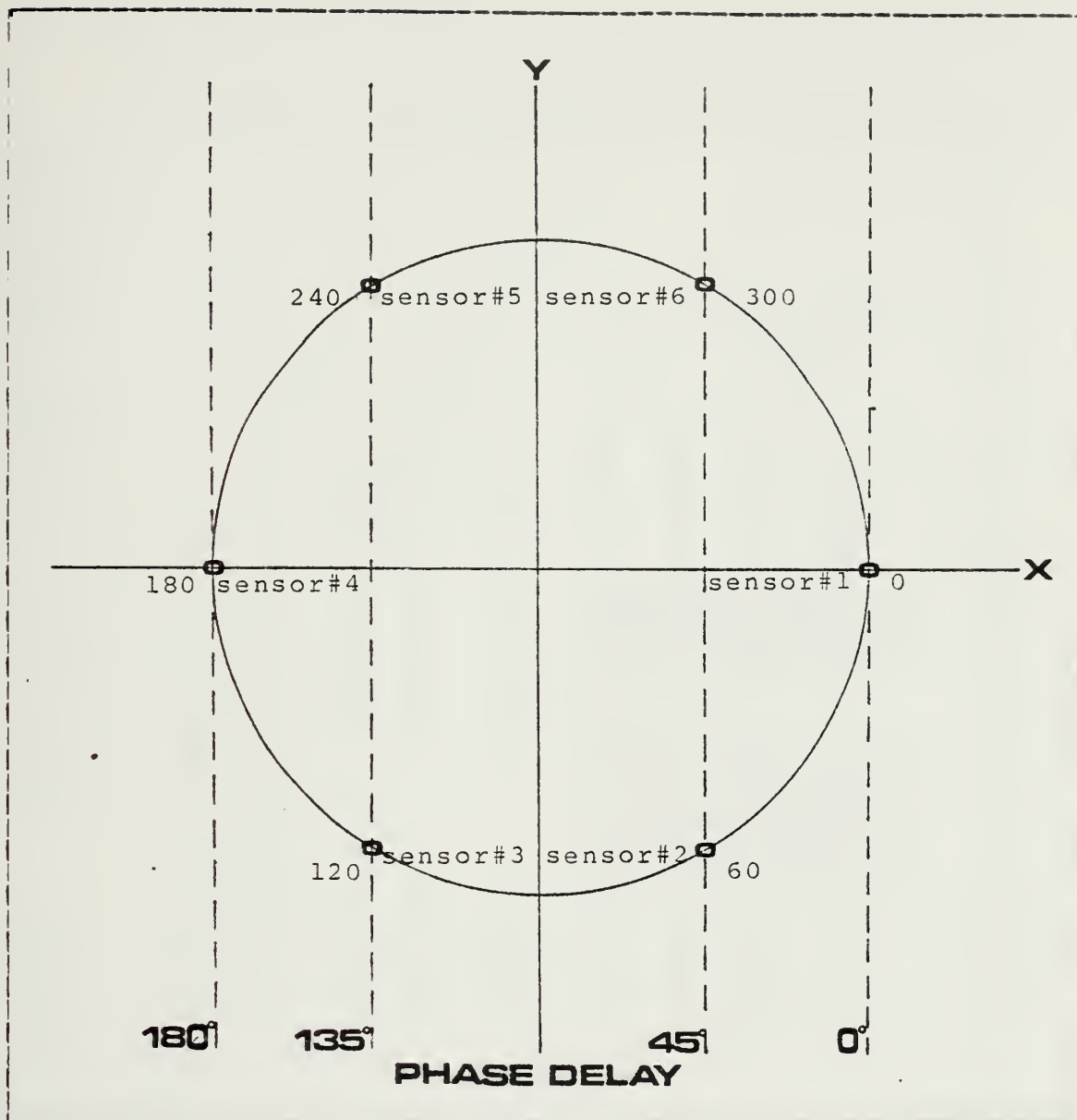


Figure 4.7 Simulation of a Zero Degree Target



# MULTIPLE TARGET - MATCHED FILTER OUTPUT

EVENT NUMBER	375
TIME PERIOD(SEC)	25.00 35.00
WHEELED VEHICLE	DIRECTION --59.00
SHELL BLAST	DIRECTION - 315.00
PERSONNEL	DIRECTION --59.00
SIMULATED TRKD VEHICLE	TARGET FREQUENCY 0.00
AMPLITUDE	0.0000
DIRECTION	0.0000
SIMULATED WILD VEHICLE	TARGET FREQUENCY 0.00
AMPLITUDE	0.0000
DIRECTION	0.0000
SIMULATED HELICOPTER	TARGET FREQUENCY 0.00
AMPLITUDE	0.0000
DIRECTION	0.0000
SIMULATED PERSONNEL	TARGET FREQUENCY 0.00
AMPLITUDE	0.0000
DIRECTION	0.0000

Figure 4.8 Sample Multiple Target and Simulated Target Output



## V. MULTIPLE TARGET DIRECTION

### A. THEORY AND DESIGN CRITERION

The modern battlefield is comprised of many classes and quantities of seismic signals. Using these signals for target identification and acquisition is the purpose of battlefield seismic sensors. As presented in the last chapter, matched filters can be used for target identification. In this chapter, it will be shown that matched filter information may also be used to obtain target bearing.

Multiple target acquisition requires the concurrent separation of the target classes and the computation of direction for each of the target classes found. The output of the matched filter is a spike at  $t_0$ , the time of peak signal detection. If matched filtering is performed for each of the sensors in the ring, the value of their respective  $t_0$ , for each filter output, would be different. Since the seismic waves impinge upon each sensor at different times, dependent upon the target direction, the values for  $t_0$  for each sensor may be expected to be directly related to the arrival angle of the seismic wave. The  $t_0$  spike of the matched filter output may be thought of as a signal compression for both the continuous (tank, truck etc.) and the time limited (shell blast, artillery recoil etc.) seismic signals [Ref. 6].

Time domain methods [Ref. 1] use the positional differences of known wave points to geometrically estimate direction. The times associated with a sensor ring's peak amplitude responses may be explained by way of an illustrative example of a shell blast. A rough direction to the origin of this shell blast can be computed using the





relative time differences associated with the peak amplitudes of all of the ring's sensors [Ref. 9].

The enhanced time positional information, which is a by-product of the matched filtering, can be used to perform just such a time domain approach. The motivation for the method is that, unlike other time and frequency domain methods, which are very susceptible to noise corruption inaccuracies, matched filtering pulls the signal out of the noise and optimally detects the signal at time  $t_0$ . Two time domain methods are evaluated for finding arrival angles of the seismic signal. The first being the time domain phase difference (TDPD) method. The second being a least mean squares polynomial (LMSP) curve fitting approach.

#### B. MULTIPLE TARGET FILTERING ALGORITHM (MULTI)

The routine MULTI calls the matched filter routine for each sensor's amplitude signal. Returned are the target classes found with their relative peak filter response positions. Figure 5.1 illustrates a two target case. The matched filter response and the relative time position for the two classes of targets can be seen. The figure shows that a shell blast target is present. The relative time for this target class is 5800. The relative time returned for the simulated wheeled vehicle target is 3000. These times or positions are relative since each sensor's filter response peaks are offset in time with respect to the peaks of the other sensors. This allows for simultaneous direction finding for each class of target. This algorithm allows selection of either a time domain phase difference or a least means square polynomial algorithm for finding the direction to the targets. The time domain phase difference algorithm is derived first [Ref. 1]. The least mean squares polynomial direction algorithm then follows and is believed to be an original application to this field [Ref. 10].



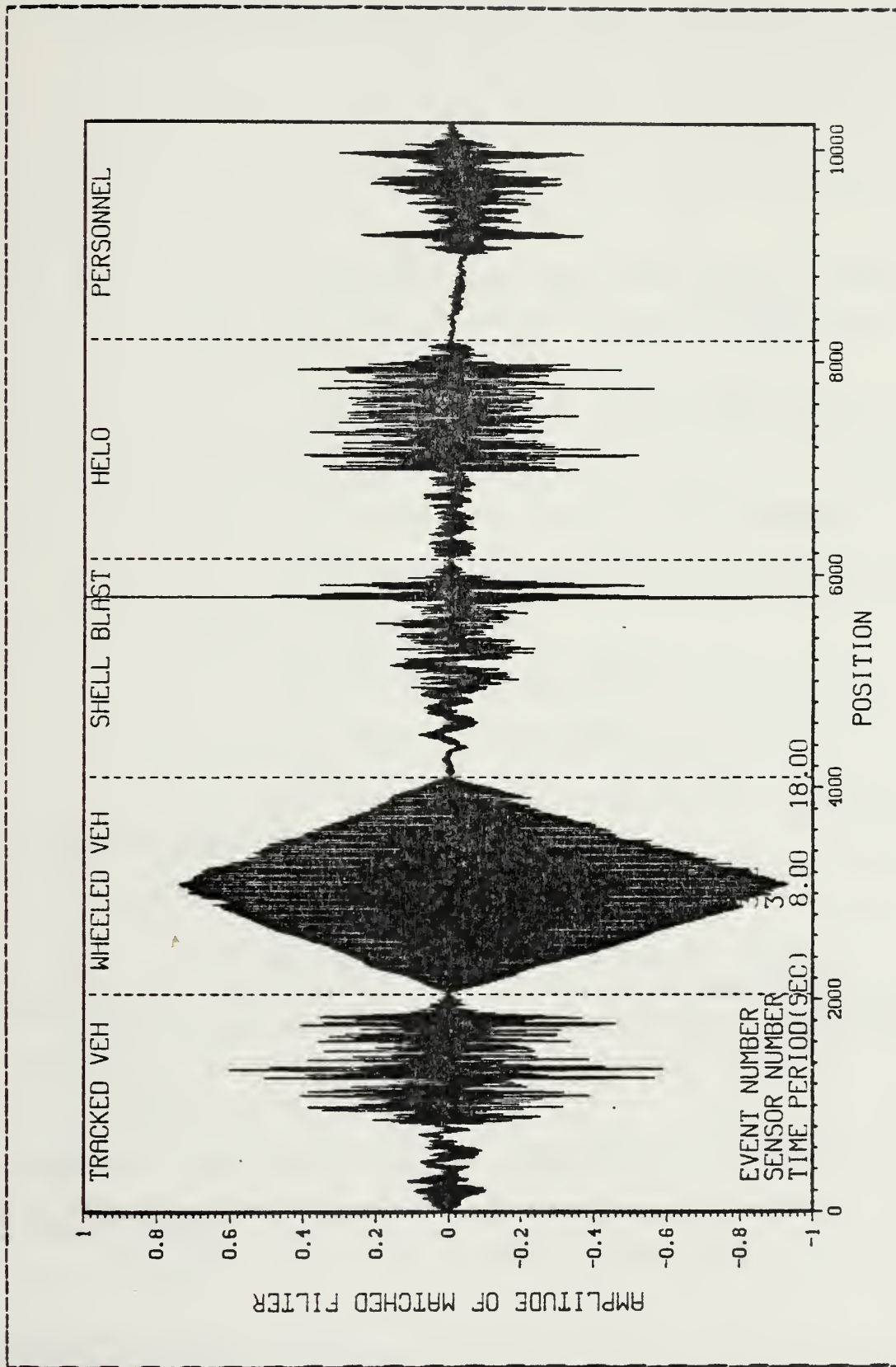


Figure 5.1 Two Target Matched Filter Response



# 1. Multiple Target Direction Phase Difference Algorithm

$T_{ij}$  - the arrival time of the seismic signal at the I-th sensor for the J-th target class

$\theta_i$  - the angle of the I-th sensor to the x - axis

$D_{ji}$  - the distance from the origin to where the wave front of the J-th target passes the I-th sensor

$T_{cj}$  - the time when the J-th target class passes the origin

$X_i, Y_i$  - the position of the I-th sensor

$B_j$  - the arrival angle of the seismic wave for the J-th target class

$V$  - the seismic wave velocity

$R$  - the radius of the sensor ring

$I$  - the sensor number where  $I$  has integer values from one to nine

$J$  - the J-th target class

$N$  - the number of sensors in the ring

Figure 5.2 illustrates these parameters and their interdependence. The derivation of the algorithm follows:

$$\theta_i = 2 (I - 1) / N$$

where zero degrees is set parrallel to the x - axis

$$X_i = R \cos \theta_i$$

$$Y_i = R \sin \theta_i$$

$$D_{ji} = R \cos (\theta_i - B_j)$$



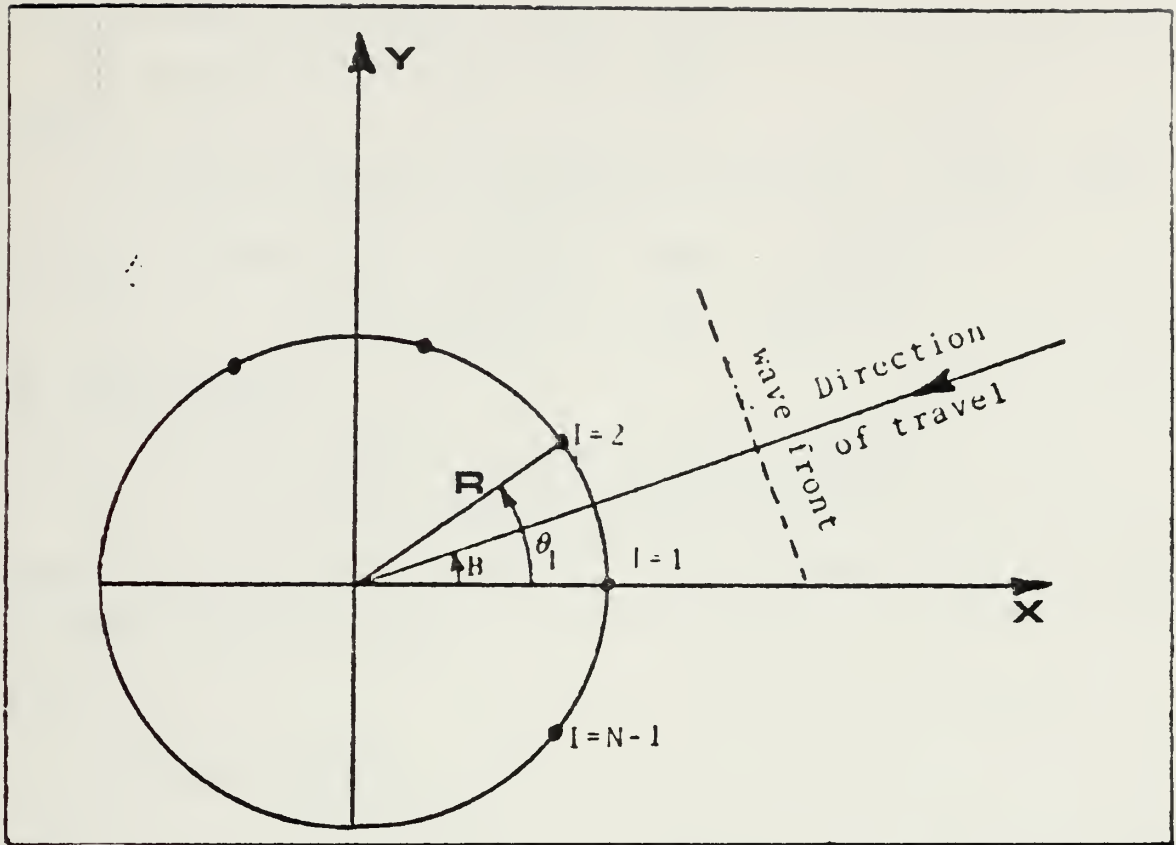


Figure 5.2 Circular Sensor Array Geometry

or equivalently  $D_{ji} = (X_i) \cos B_j + (Y_i) \sin B_j$

$$Tc_j = (1/N) \sum_{i=1}^N T_{ji}$$

$$\tau_{ji} = Tc_j - T_{ji}$$

$$V = D_{ji} / \tau_{ji}$$

$$V = ((X_i) \cos B_j + (Y_i) \sin B_j) / (Tc_j - T_{ji}) \quad (5.1)$$

Since the wave velocity can be assumed to be constant when passing all sensors, then for any sensor I and K where  $I \neq K$ , equation 5.1 leads to





$$\begin{aligned} ((X_i) \cos B_j + (Y_i) \sin B_j) / (T_{c_j} - T_{ji}) = \\ ((X_i) \cos B_j + (Y_i) \sin B_j) / (T_{c_j} - T_{jk}) \end{aligned}$$

Where  $I \neq K$

Now solving for the arrival angle  $B_{jik}$  of the wave

$$B_{jik} = \arctan \left( \frac{((T_{c_j} - T_{jk}) X_i - (T_{c_j} - T_{ji}) X_k) /}{((T_{c_j} - T_{ji}) Y_k - (T_{c_j} - T_{jk}) Y_i)} \right)$$

or equivalently;

$$B_{jik} = \arctan \left( \frac{((T_{c_j} - T_{jk}) \cos \theta_i - (T_{c_j} - T_{ji}) \cos \theta_k) /}{((T_{c_j} - T_{ji}) \sin \theta_k - (T_{c_j} - T_{jk}) \sin \theta_i)} \right)$$

Where the values of  $T_{ji}$  and  $T_{jk}$  are returned values from the matched filter routine.

Now;

$$B_j = (1/(N)^2) \sum_{i=1}^N \sum_{k=1}^N B_{jik}$$

Where  $B_j$  is the direction in radians to the J-th class target. For the multiple direction routine as implemented, 'j' has values from one to five.

## 2. Least Mean Square Polynomial Direction Finding

The least mean square direction finding algorithm was developed in response to problems encountered with the phase difference direction finding algorithm. This new method is based on a least mean squares polynomial curve fit of the sensor data. This approach was selected since the least mean squares polynomial provides for best fit or a maximum likelihood curve fit for noisy data.

The least mean squares direction finding algorithm, as with the phase difference algorithm, assumes the seismic wave to be planar. Figure 5.2 illustrates the parameters for this model. Once the assumption of a planar seismic wave is made, the expected relation between the arrival



angle, relative delay times and sensor position in the circular array, can be made. Figure 5.3 illustrates these relations for a nine sensor circular array with a seismic wave arriving at zero degrees. Notice that the relative delay times have been scaled to be from zero to one.

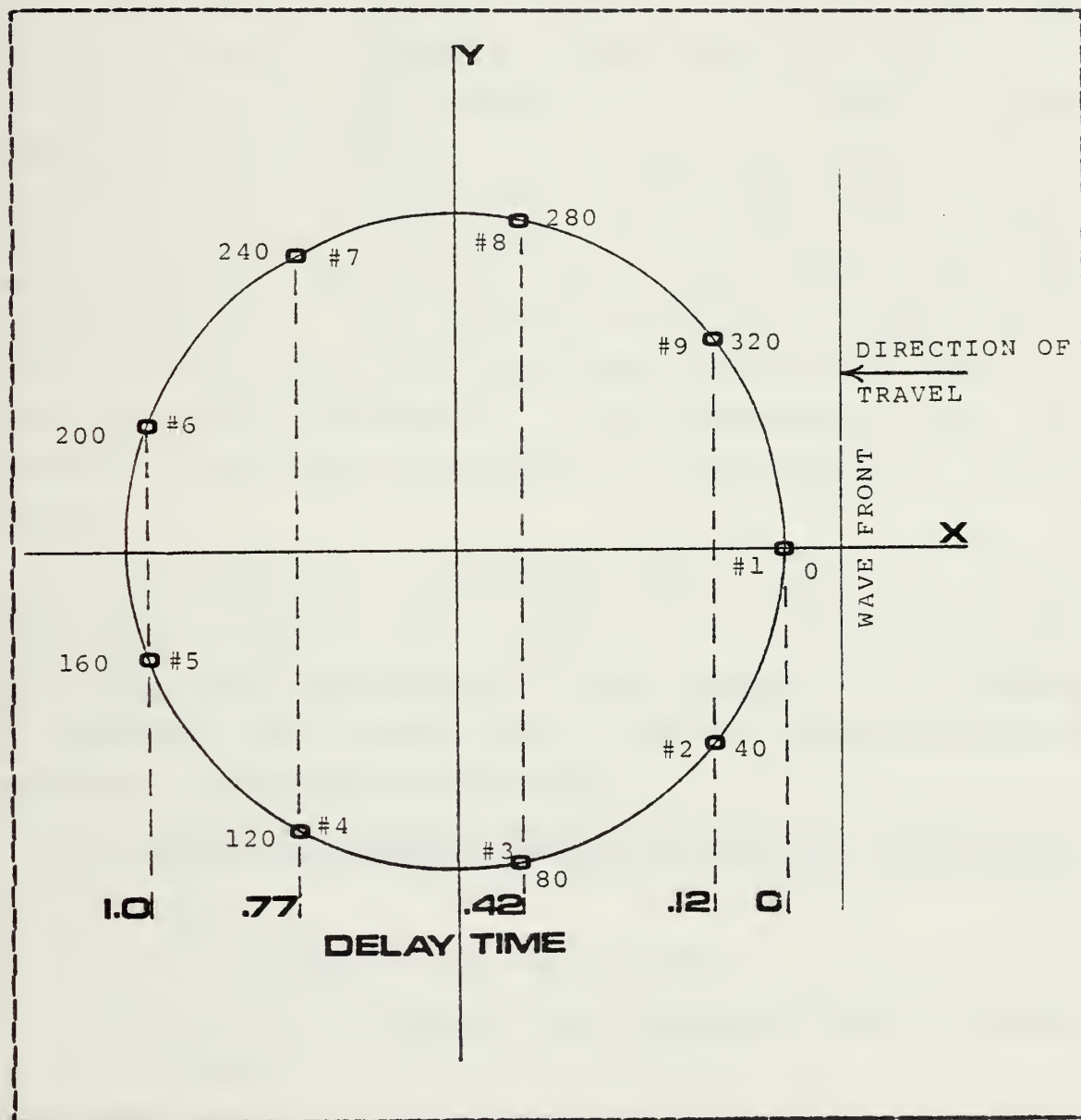


Figure 5.3 Relative Delay Times in a Nine Sensor Ring



Since the sensors in a nine sensor ring are at increments of forty degrees relative to the x-axis, a correlation can be seen between the relative time delays at each sensor and the arrival angle of the seismic wave. A plot can now be made to illustrate the relationship of sensor angles versus relative time delays. Figure 5.3 is a plot for a nine sensor ring with a planar seismic wave arriving at zero degrees. Figure 5.4 shows that for a wave at an arrival angle of 160 degrees, the delay time at sensor number five will be zero. It can be seen that the fitting of these ideal data points with a least mean squares polynomial will produce an equation for a curve whose minimum value is also at the arrival angle of the seismic wave. The minimum degree of the polynomial to fit this ideal data is four. This results from noting that the curve in figure 5.4 has three curve inflections. For experimental data, this minimum curve point corresponds to the predicted arrival angle.

Polynomials of degrees higher than four may be expected to enhance arrival angle errors since the polynomial would distort to fit noisy data. Least means squares polynomials of degree two and three however, may be useful in reducing curve sensitivity to one or two malfunctioning sensors or excessively noisy data.

### 3. Least Mean Squares Polynomial Algorithm Derivation

Let:

$N$  - number of data point pairs

$Y_i$  - the observed or experimental data position values

$X_i$  - independent degree values with a range of 0 to 360 degrees



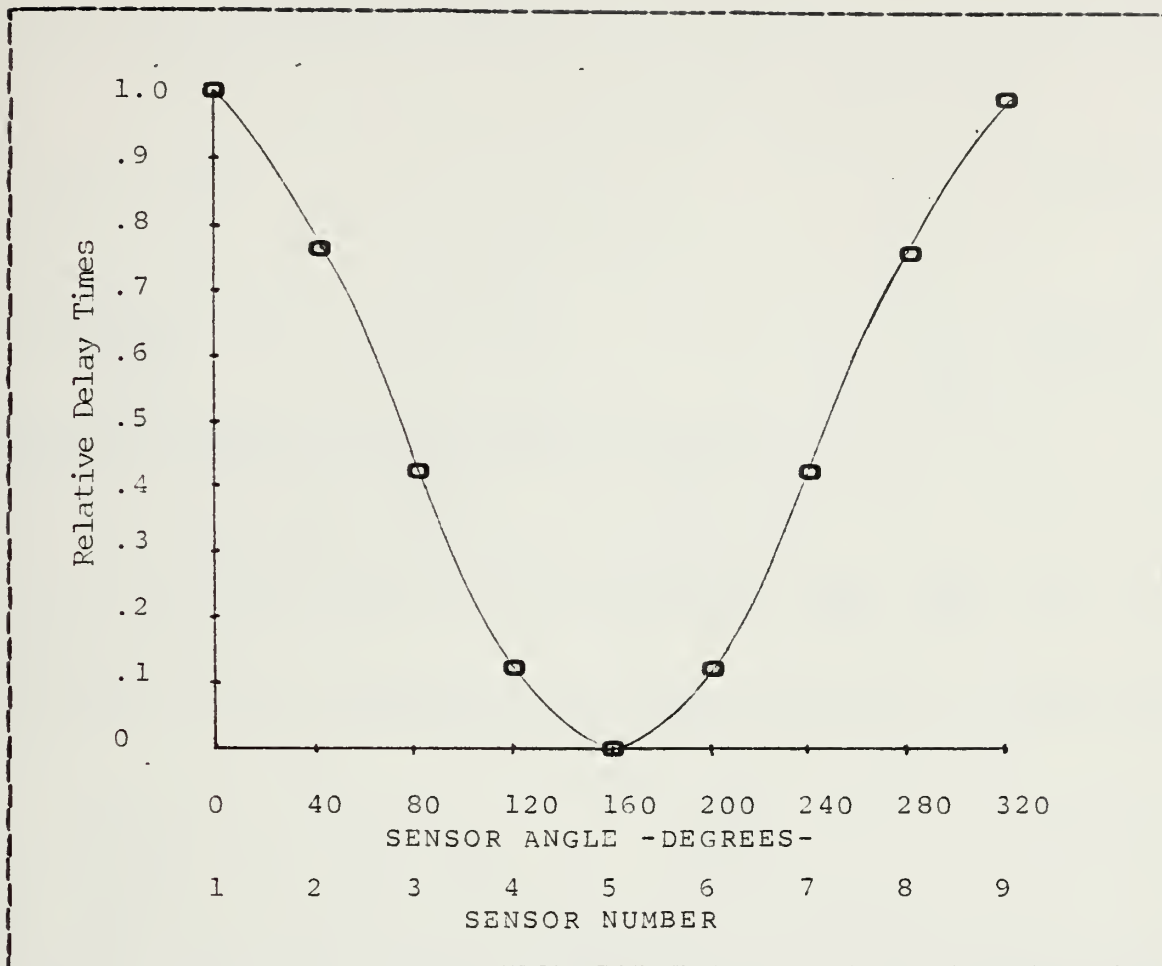


Figure 5.4 Relative Time Delay versus Sensor Angle

$P_i$  - dependent predicted delay time values found by the least mean squares polynomial

$A_i, B_i$  - coefficient values for the system of simultaneous equations

$E_i$  - error between the experimental data values and predicted values of time delays

$S$  - sum of the square errors between each data and predicted points

The derivation of the least mean squares polynomial follows:

$$S = E_1^2 + E_2^2 + E_3^2 + \dots + E_N^2$$





$$P_i = A_0 + A_1 X_i + A_2 X_i^2 + A_3 X_i^3 + \dots + A_n X_i^n \quad (5.2)$$

$$E_i = Y_i - P_i \quad (5.3)$$

$$S = \sum_{i=1}^N E_i^2 \quad (5.4)$$

Combining equations 5.2 and 5.3 yields

$$E_i = Y_i - A_0 - A_1 X_i - A_2 X_i^2 - \dots - A_n X_i^n$$

where  $n$  is the degree of the polynomial such that  $N > n + 1$  and  $1 < i < N$

Equation 5.4 now becomes, after substituting for  $E$ , equation 5.5

$$S = \sum_{i=1}^N (Y_i - A_0 - A_1 X_i - A_2 X_i^2 - \dots - A_n X_i^n)^2 \quad (5.5)$$

To find the minimum of the sum of the squares expressed by equation 5.5, the partial derivatives of  $S$  with respect to all of the coefficients are taken. At the minimum, these partial derivatives all vanish.

$$\begin{aligned} \partial S / \partial A_0 &= 0 = \sum_{i=1}^N 2 (Y_i - A_0 - A_1 X_i - \dots - A_n X_i^n) (-1) \\ \partial S / \partial A_1 &= 0 = \sum_{i=1}^N 2 (Y_i - A_0 - A_1 X_i - \dots - A_n X_i^n) (-X_i) \\ &\quad \cdot \quad \cdot \quad \cdot \\ &\quad \cdot \quad \cdot \quad \cdot \\ \partial S / \partial A_n &= 0 = \sum_{i=1}^N 2 (Y_i - A_0 - A_1 X_i - \dots - A_n X_i^n) (-X_i^n) \end{aligned}$$

Dividing by two and rearranging gives  $n + 1$  normal simultaneous equations. Expressed in matrix notation these equations become



$$\begin{bmatrix} N & \sum X_i & \sum X_i^2 & \dots & \sum X_i \\ \sum X_i & \sum X_i^2 & \sum X_i^3 & \dots & \sum X_i \\ \sum X_i^2 & \sum X_i^3 & \sum X_i^4 & \dots & \sum X_i \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ \sum X_i^n & \sum X_i^{n+1} & \sum X_i^{n+2} & \dots & \sum X_i^{2n} \end{bmatrix} \begin{bmatrix} A_0 \\ A_1 \\ A_2 \\ \vdots \\ A_n \end{bmatrix} = \begin{bmatrix} \sum Y_i \\ \sum X_i Y_i \\ \sum X_i^2 Y_i \\ \vdots \\ \sum X_i^n Y_i \end{bmatrix}$$

The coefficient matrix in the above system of equations can be solved for. The minimum value for  $P_i$  can then be found. The  $X$  corresponding to this minimum value is declared to be the predicted arrival angle of the seismic wave. [Ref. 10]

#### 4. Adaptive Target Direction Finding

An adaptive method is used to improve the directions found for all single target cases. To enhance the resolution accuracy of the peak filter output position, the single target seismic data is copied into the filter data section for its class of target. Subsequently, when the matched filter routine is called for each sensor, filtering is performed with sensor data from that time period.

#### 5. Software features of the Multiple Target Direction Routine

As first addressed in the previous chapter, the multiple direction routine allows for the selection of the number of data points to be used from the 1024 size buffer of sensor data. This was included to investigate the algorithm's performance for various data/filter window sizes and to allow an option for reduced CPU time utilization for interactive program runs. Tabular output from this routine includes the event number, the time period for the data, identification and directions for up to five target classes, and up to four simulated target specifications. Also, notice that the routine adapts to the number of sensors



specified for the ring. This was necessary since the experimental data included sensor rings of six and nine vertical sensors.

### C. MULTIPLE TARGETS OF THE SAME TARGET CLASS

A limitation on the system, as presented up to this point, is its inability to engage multiple targets of the same class. Discrete targets may appear as separate entities since the seismic signals generated by the two same class targets are not likely to be incident at the same time. This situation is greatly complicated for continuous time signals, such as tracked or wheeled vehicles. For such continuous time targets, mutual distortion would be the likely result.

An algorithm is needed to identify these multiple peaks without erroneously declaring elements in the same peak as targets. By using only the positive half of the matched filter output and performing data smoothing on the remaining points, a curve with its number of peaks equalling the number of targets present could be generated. Numerical methods for curve fitting or interpolation are available [Ref. 11.]. Polynomial curve fitting, Sterling's method and variations of Newton's method are only a few of the possible approaches applicable for equally spaced data. By differentiating the smoothed data, the peaks and valleys of the filter output can be found. The height of the curve corresponding to the points where the derivative is zero can now be compared to the selected matched filter threshold. This excludes the valley points and leaves the points remaining which correspond to the relative times of the same class targets.

This method is constrained by resolution of close proximity, time limited targets and near phase synchronization



of continuous targets. The variables to be optimized through experimentation may be the degree of the smoothing of the curve data and the exclusion of erroneous valleys associated with the same target's data.





## VI. ANALYSIS OF SEISMIC DATA

Analysis of the simulated and experimental seismic data will be conducted as detailed in Table II. Table III lists the matched filter contents for the simulated data. Table IV is the test plan for the experimental data. Table V lists the matched filter signals used for the experimental data analysis.

Table VI summarizes the results of the simulated and experimental data runs for direction finding. The window size, used for all multiple target direction finding results, was 300. Table VII lists the events in which targets were missed or incorrectly identified.

The time domain phase difference directions found, are not presented for the reasons noted earlier. Errors of up to eighty degrees were not uncommon with this method.

Each event run will be accompanied by the following graphic output:

1. Least Mean Square Initial Direction
2. Matched Filter Response
3. Amplitude Response
4. Amplitude Response of any Malfunctioning Sensor
5. Frequency Response
6. Least Mean Squares Polynomial Curve Fitting (LMSP)  
Using Matched Filter Outputs
7. Multiple Target Direction Summary Resulting from  
Least Mean Squares Curve Fitting



TABLE II  
Test Plan for Simulated Data

<u>Event</u>	<u>#Sen</u>	<u>#Tgts</u>	<u>Frequency</u>	<u>Amplitude</u>	<u>Direction</u>
001	9	1	10	3000	0
001	9	1	10	3000	40
001	9	1	10	3000	120
001	9	1	10	3000	240

TABLE III  
Matched Filter for Simulated Targets

<u>Filter</u>	<u>Frequency</u>	<u>Amplitude</u>	<u>Direction</u>
Tracked Veh	30	2000	0
Wheeled Veh	10	2000	0
Shell blast data from event #383			0
Helicopter	15	2000	0
Personnel	20	2000	0



**TABLE IV**  
**Test Plan for Experimental Data**

<u>Event</u>	<u>#Sen</u>	<u>#Tgts</u>	<u>Dir</u>	<u>Target</u>	<u>Distance</u>
383	9	1	0	Shot	5KM
382	9	1	0	Shot	5Km
372	6	1	315	Helicopter	5 - 15KM
375	6	1	0	Tank	5 - 0Km
374	6	1	315	Helicopter	15 - 5KM
302	6	1	0	Mortar	1KM
314	6	1	315	LVT	4 - 5KM
354	6	5	0	105mm How	5Km
			225	175mm Gun	4KM
			315	LVT	4 - 5KM
			0	M-60 Tank	4 - 5KM

**TABLE V**  
**Matched Filter for Experimental Data**

<u>Target</u>	<u>Event Used as Filter</u>
Tracked Vehicle	375
Wheeled Vehicle	none (background noise)
Blast/Recoil	383
Helicopter	372
Personnel	none (background noise)



**TABLE VI**  
**Summary of Direction Finding Results**

<u>Event</u>	<u>#Sen</u>	<u>#Tgts</u>	<u>Distance</u>	<u>Dir</u>	<u>Initial</u> <u>Dir</u>	<u>Zerror</u>	<u>LMSP</u> <u>Dir</u>	<u>Zerror</u>
001	9	1	N/A	0	N/A		0	0
001	9	1	N/A	40	N/A		40	0
001	9	1	N/A	120	N/A		120	0
001	9	1	N/A	240	N/A		240	0
383	9	1	5KM	0	4 (3)	1.1	28 (4) -5	7.8 1.4
382	9	1	5KM	0	-14 (4)	3.9	-6	1.67
372	6	1	5 - 15KM	315	-32	3.6	-59	3.9
375	6	1	5 - 0KM	0	312	13.3	FAILED	
374	6	1	15 - 5KM	315	-59	4.0	FAILED	
302	6	1	1KM	0	4	1.1	6	1.7
354	6	5	5KM	0	-3	.8	3	.8
			4 KM	225	291	18.0	FAILED	
			4 - 5KM	315	FAILED			
			4 - 5KM	0	FAILED			

\*Note: The matched filter threshold was set at .9 for all single targets and .6 for all multiple target events. Brackets indicate the use of other than a second degree polynomial.





TABLE VII  
Missed or Incorrectly Identified Targets

<u>Event</u>	<u>#Targets</u>	<u>Target</u>	<u>Nature of Errors</u>
375	1	Tank	1. Matched filter was not based on a high S/N sample signal
374	1	Helo	2. Small seismic signal amplitudes
354	1	LVT	3. Malfunctioning sensor(s)
	1	Tank	
	1	175mm Gun	Sever clipping distortion of input signal

Note: The numbered error sources apply to all events listed.



# LEAST MEAN SQUARES POLYNOMIAL

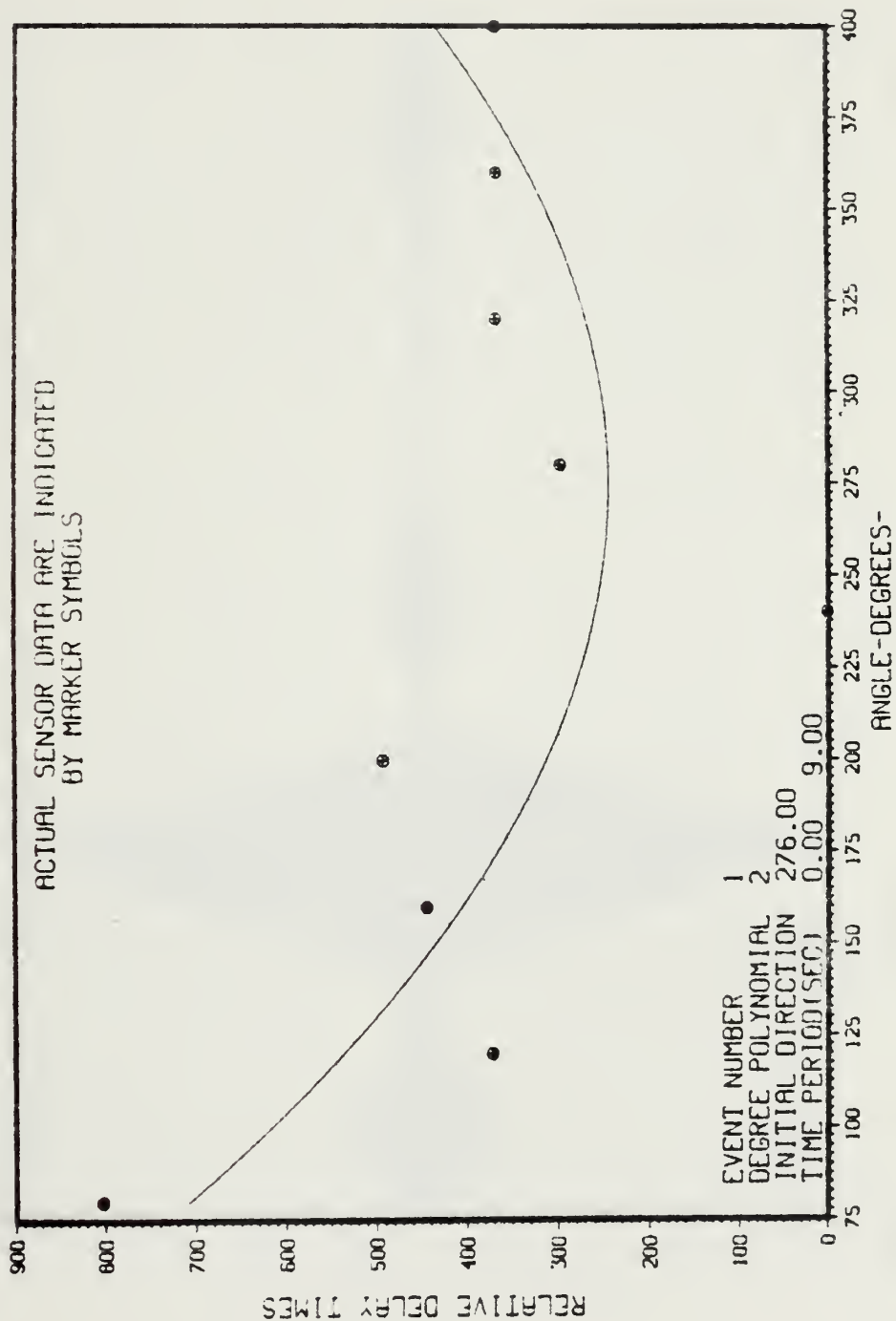


Figure 6.1 Sample Least Mean Squares Initial Direction for Event 001



# MATCHED FILTER RESPONSE

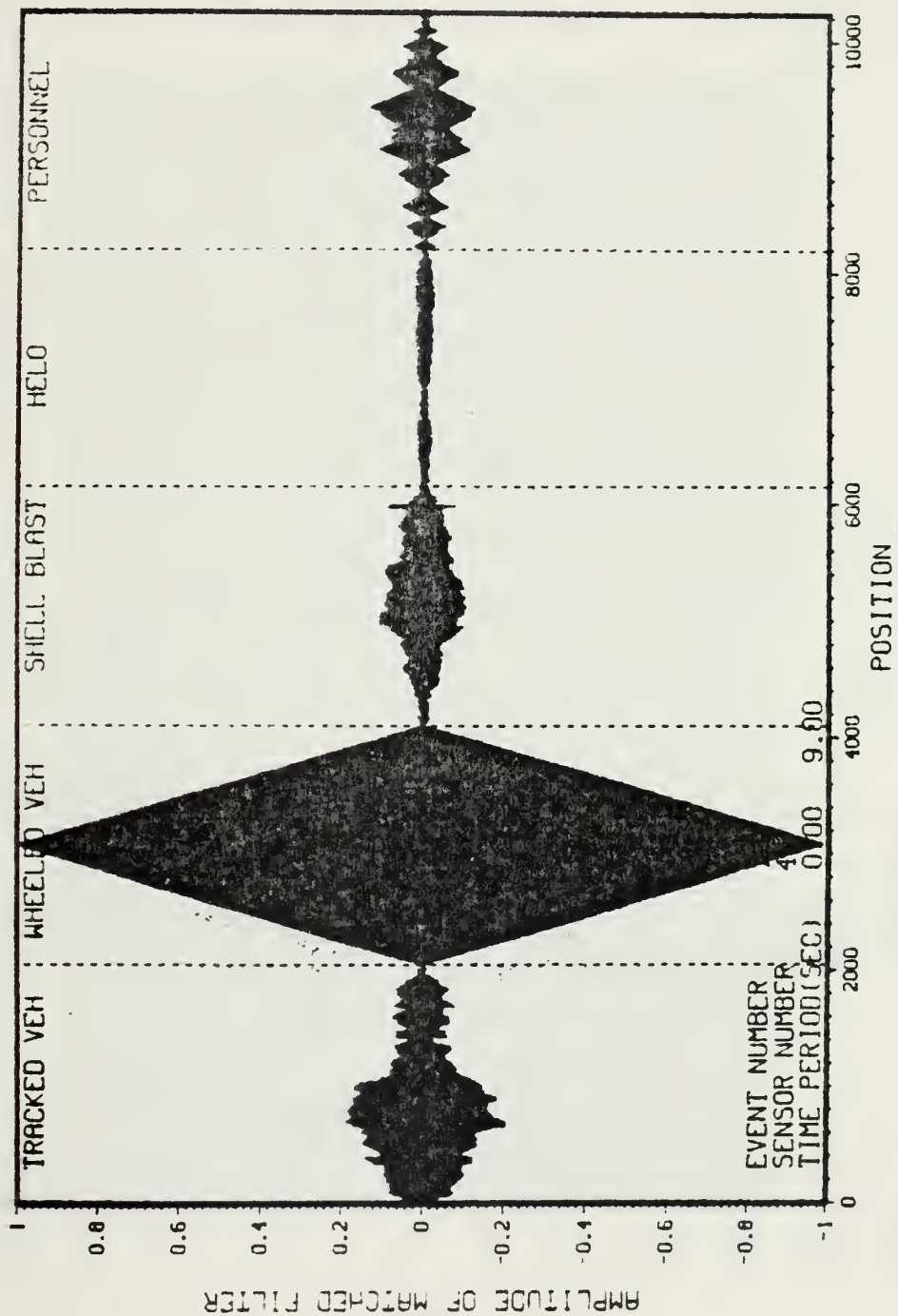


Figure 6.2 Sample Matched Filter Response for Event 001



SENSOR INPUT - VS - TIME

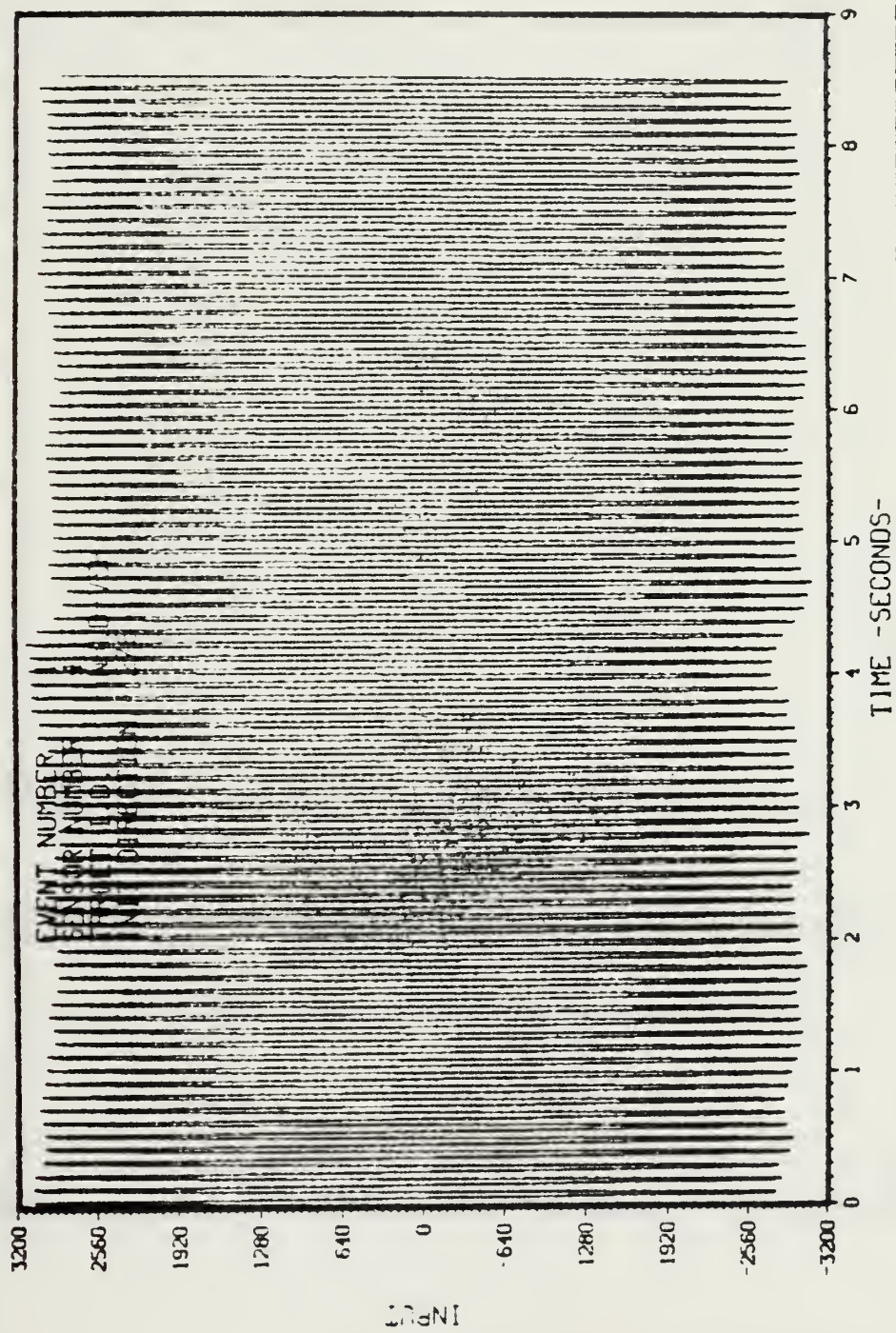


Figure 6.3 Sample Amplitude Response for Event 001





# SENSOR POWER -VS- FREQUENCY

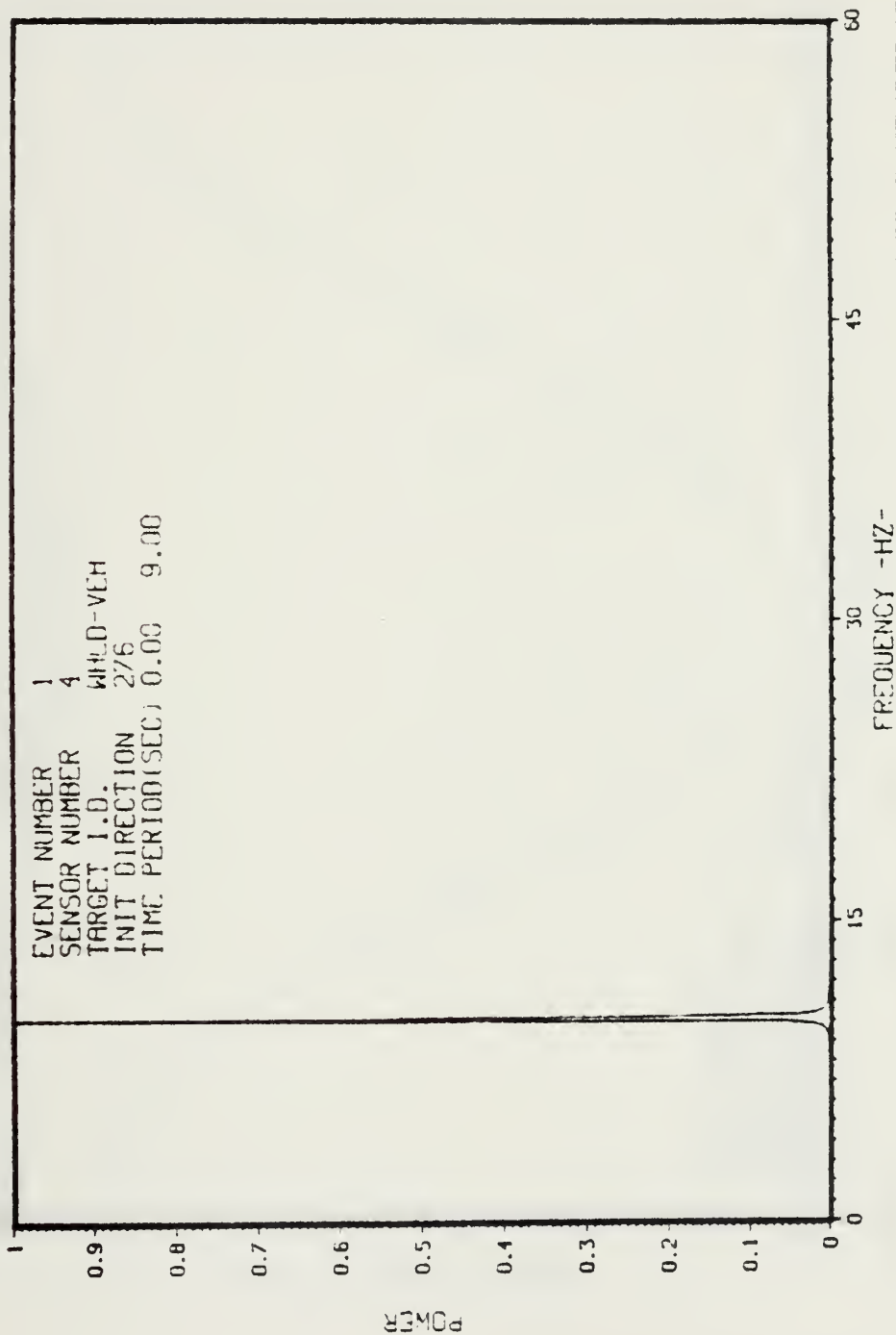


Figure 6.4 Sample Frequency Response for Event 001



# LEAST MEAN SQUARES POLYNOMIAL

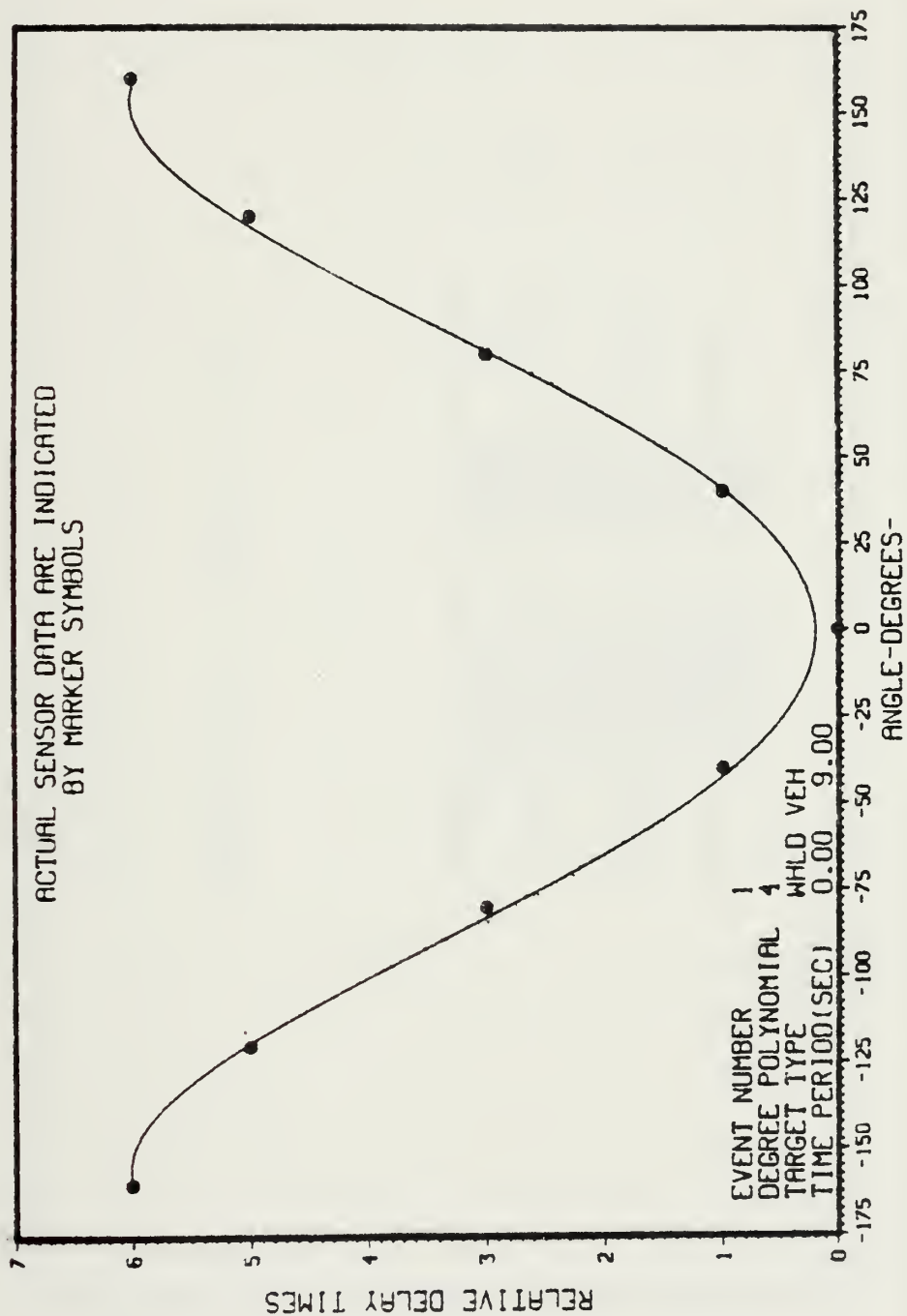


Figure 6.5 LMSP Matched Filter Direction for Event 001



# MULTIPLE TARGET - MATCHED FILTER OUTPUT

EVENT NUMBER 1

TIME PERIOD(SEC) 0.00 9.00

WHEELED VEHICLE DIRECTION - 0.00

SIMULATED TRKD VEHICLE	TARGET FREQUENCY	0.00
AMPLITUDE	0.0000	
DIRECTION	0.0000	
SIMULATED WHLD VEHICLE	TARGET FREQUENCY	10.00
AMPLITUDE	3000.0000	
DIRECTION	0.0000	
SIMULATED HELICOPTER	TARGET FREQUENCY	0.00
AMPLITUDE	0.0000	
DIRECTION	0.0000	
SIMULATED PERSONNEL	TARGET FREQUENCY	0.00
AMPLITUDE	0.0000	
DIRECTION	0.0000	

Figure 6.6 LMSP Multiple Target Direction Summary for Event 001



# LEAST MEAN SQUARES POLYNOMIAL

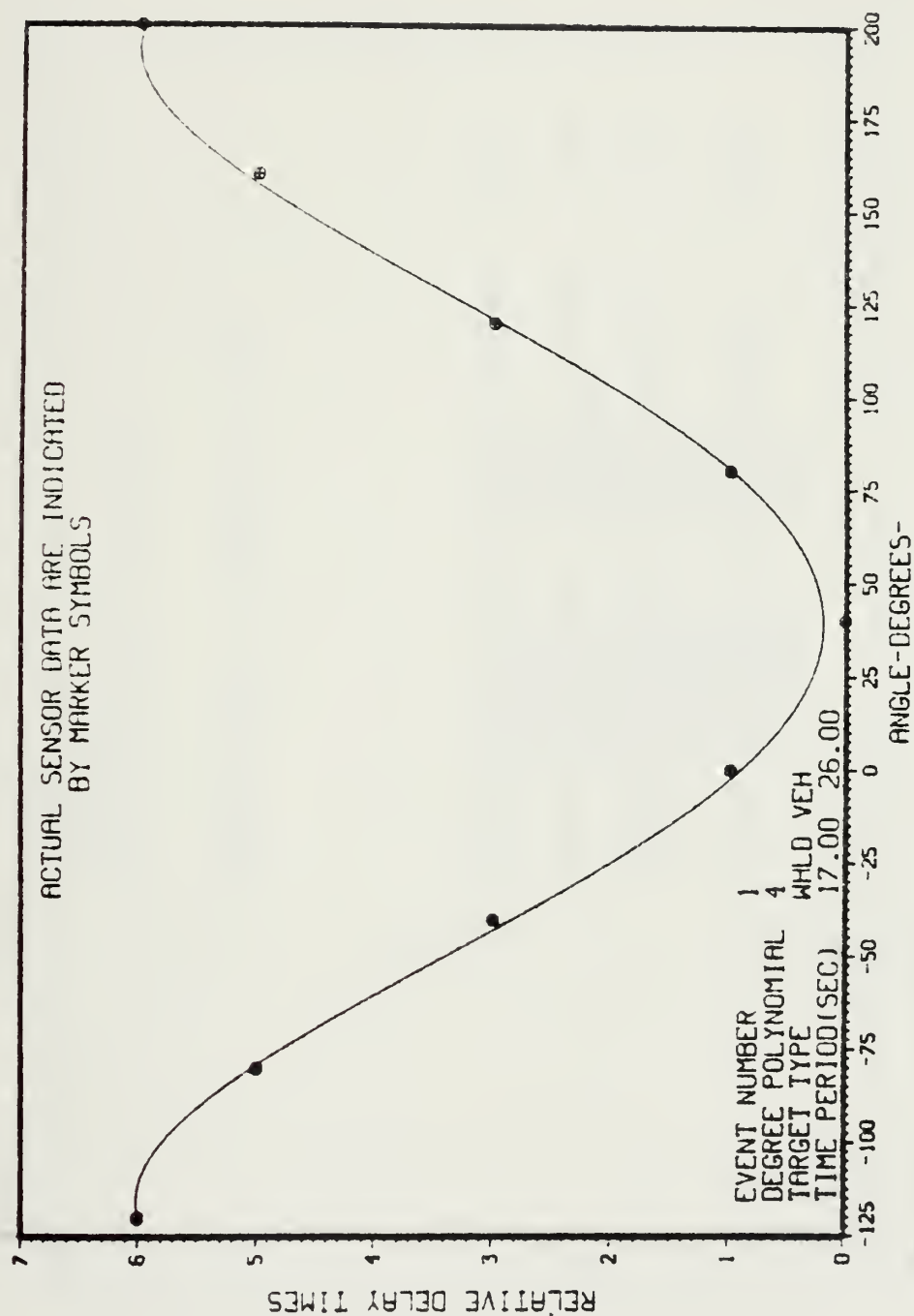


Figure 6.7 LMSP Matched Filter Direction for Event 001





# MULTIPLE TARGET - MATCHED FILTER OUTPUT

EVENT NUMBER 1

TIME PERIOD(SEC) 17.00 26.00

WHEELED VEHICLE DIRECTION - 40.00

SIMULATED TRKD VEHICLE	TARGET FREQUENCY	0.00
AMPLITUDE	0.0000	
DIRECTION	0.0000	
SIMULATED WMLD VEHICLE	TARGET FREQUENCY	10.00
AMPLITUDE	3000.0000	
DIRECTION	40.0000	
SIMULATED HELICOPTER	TARGET FREQUENCY	0.00
AMPLITUDE	0.0000	
DIRECTION	40.0000	
SIMULATED PERSONNEL	TARGET FREQUENCY	0.00
AMPLITUDE	0.0000	
DIRECTION	0.0000	

Figure 6.8 LMSP Multiple Target Direction Summary for Event 001



# LEAST MEAN SQUARES POLYNOMIAL

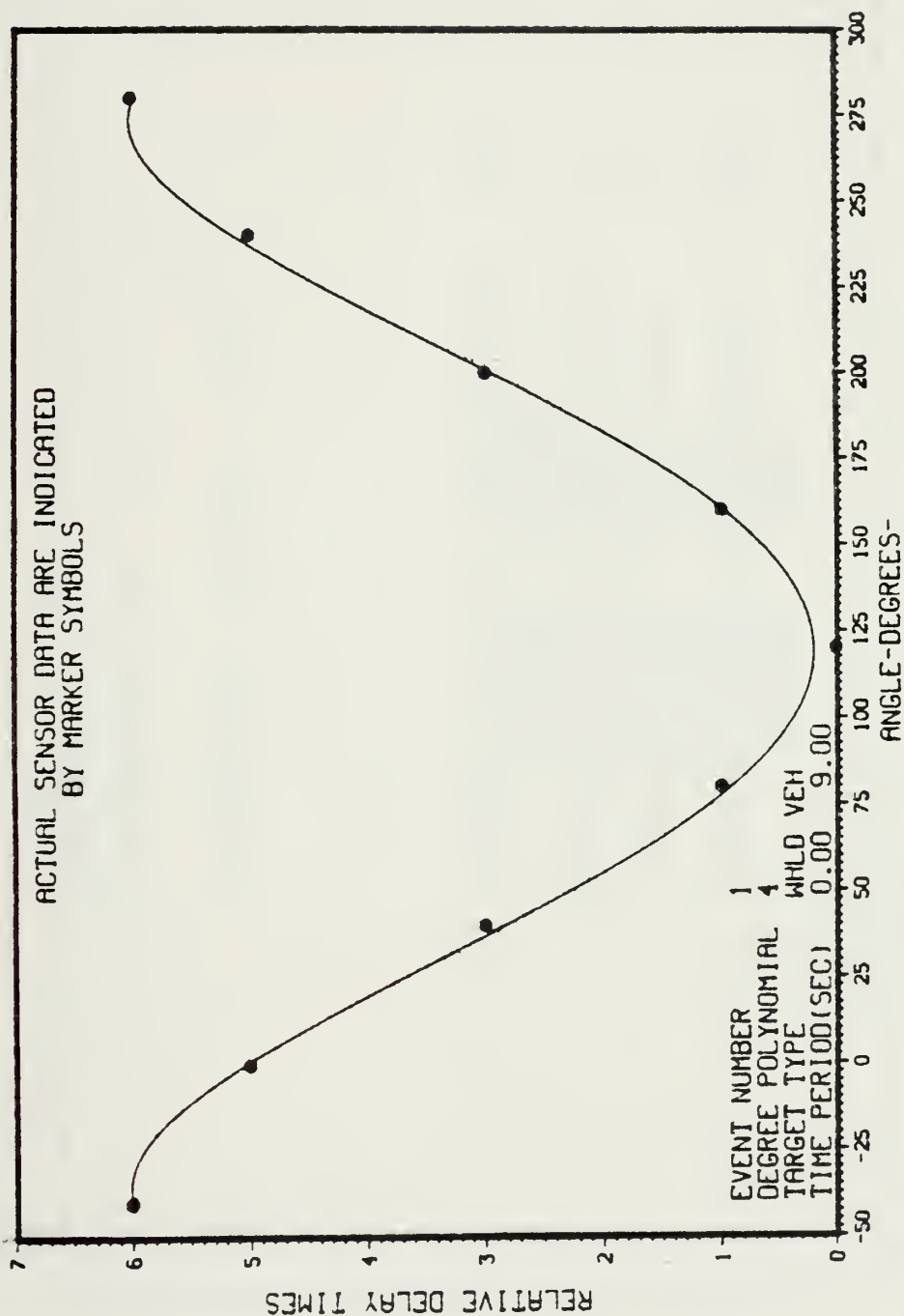


Figure 6.9 LMSP Matched Filter Direction for Event 001



# MULTIPLE TARGET - MATCHED FILTER OUTPUT

EVENT NUMBER	1		
TIME PERIOD(SEC)	0.00	9.00	
WHEELED VEHICLE	DIRECTION - 120.00		
SIMULATED TRKD VEHICLE	TARGET FREQUENCY	10.00	
AMPLITUDE	3000.0000		
DIRECTION	120.0000		
SIMULATED WHLD VEHICLE	TARGET FREQUENCY	0.00	
AMPLITUDE	0.0000		
DIRECTION	0.0000		
SIMULATED HELICOPTER	TARGET FREQUENCY	0.00	
AMPLITUDE	0.0000		
DIRECTION	0.0000		
SIMULATED PERSONNEL	TARGET FREQUENCY	0.00	
AMPLITUDE	0.0000		
DIRECTION	0.0000		

Figure 6.10 LMSP Multiple Target Direction Summary for Event 001



# LEAST MEAN SQUARES POLYNOMIAL

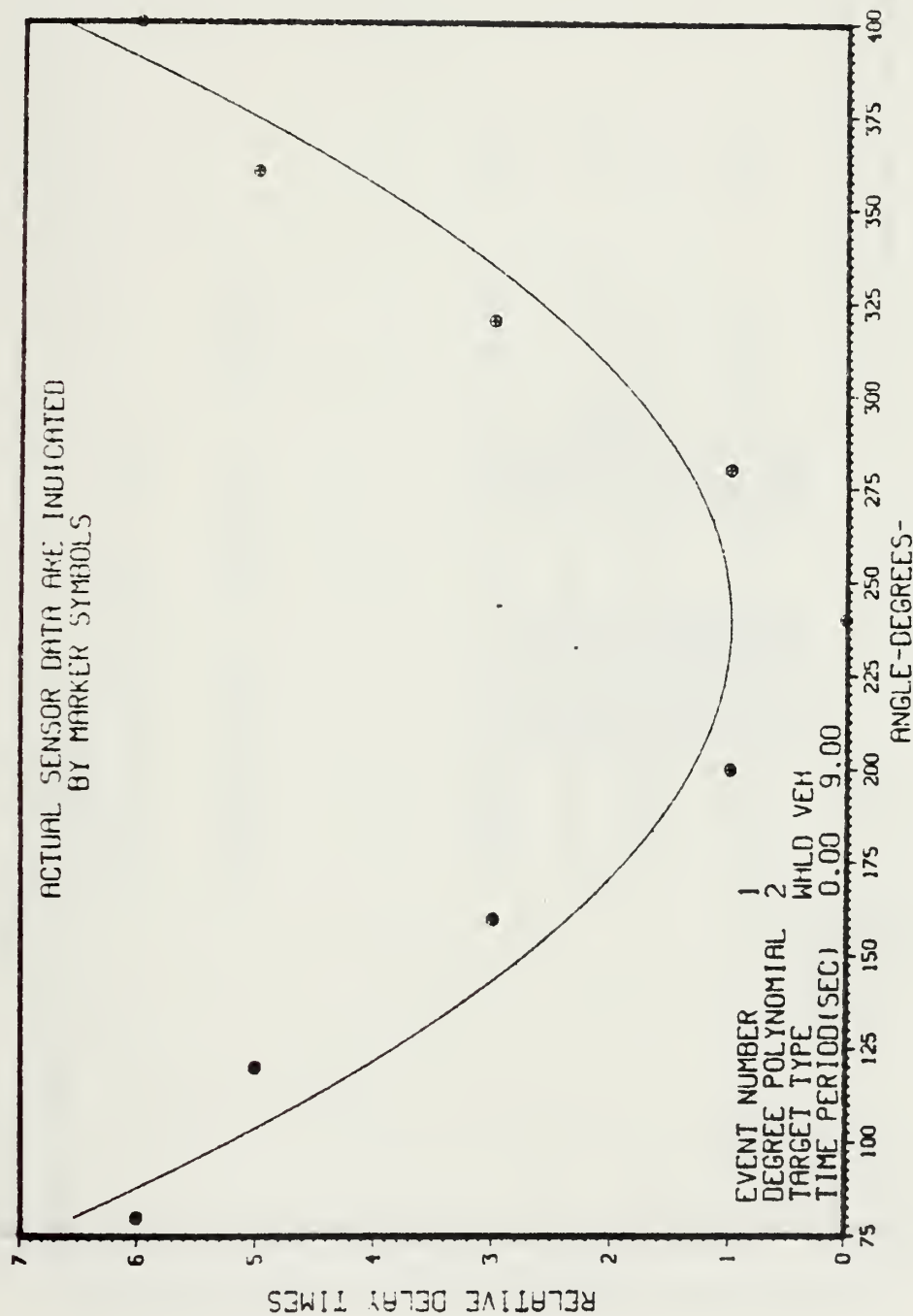


Figure 6.11 LMSP Matched Filter Direction for Event 001





# MULTIPLE TARGET - MATCHED FILTER OUTPUT

```

EVENT NUMBER      1
TIME PERIOD(SEC)  0.00  9.00

WHEELED VEHICLE   DIRECTION - 240.00

SIMULATED TRKO VEHICLE TARGET FREQUENCY      0.00
AMPLITUDE      0.0000
DIRECTION      0.0000
SIMULATED WILD VEHICLE TARGET FREQUENCY      10.00
AMPLITUDE      3000.0000
DIRECTION      240.0000
SIMULATED HELICOPTER TARGET FREQUENCY      0.00
AMPLITUDE      0.0000
DIRECTION      0.0000
SIMULATED PERSONNEL TARGET FREQUENCY      0.00
AMPLITUDE      0.0000
DIRECTION      0.0000
    
```

Figure 6.12 LMSP Multiple Target Direction Summary for Event 001



# LEAST MEAN SQUARES POLYNOMIAL

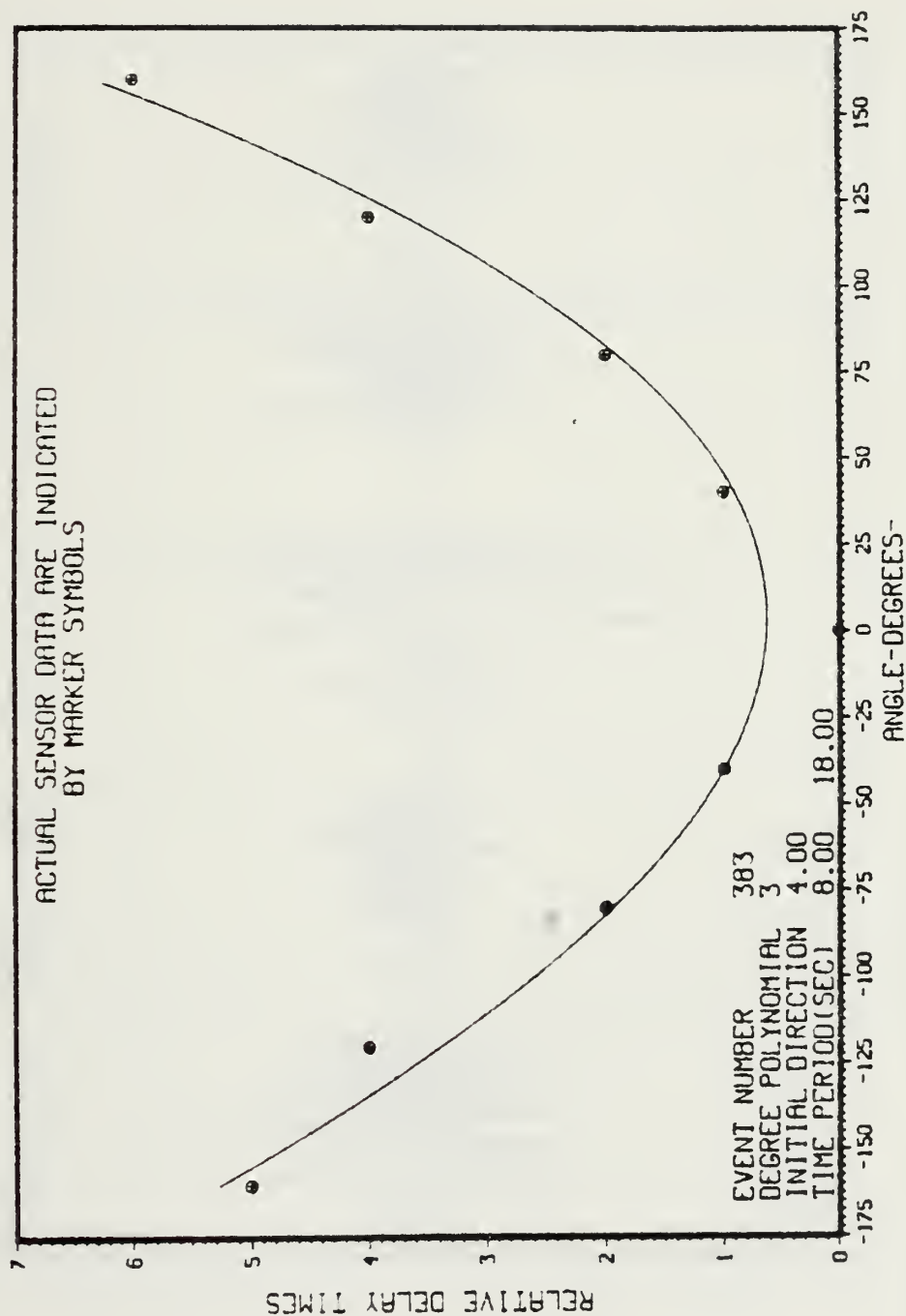


Figure 6.13 LMSP Initial Direction for Event 383



# MATCHED FILTER RESPONSE

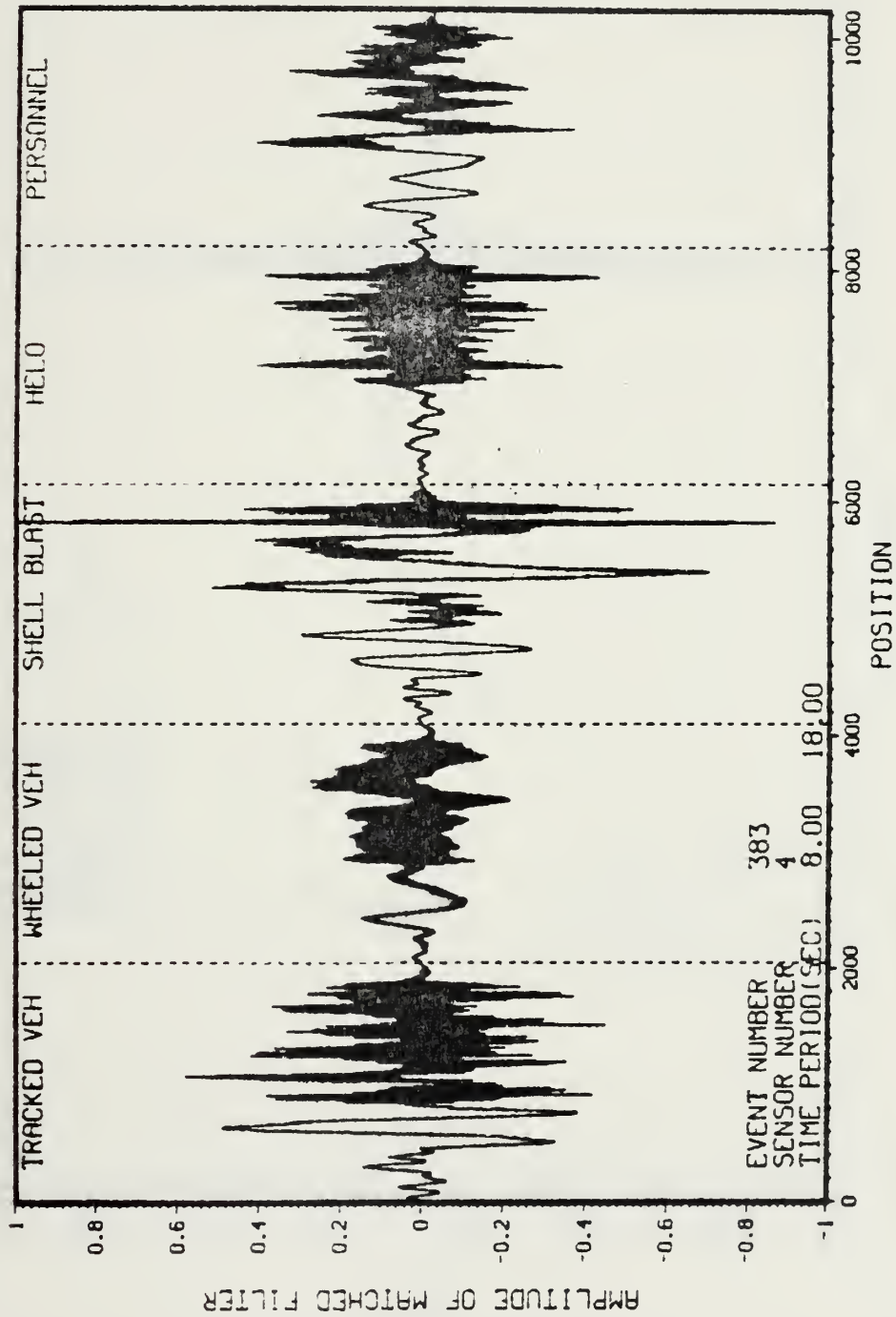


Figure 6.14 Matched Filter Response for Event 383



# SENSOR INPUT - VS - TIME

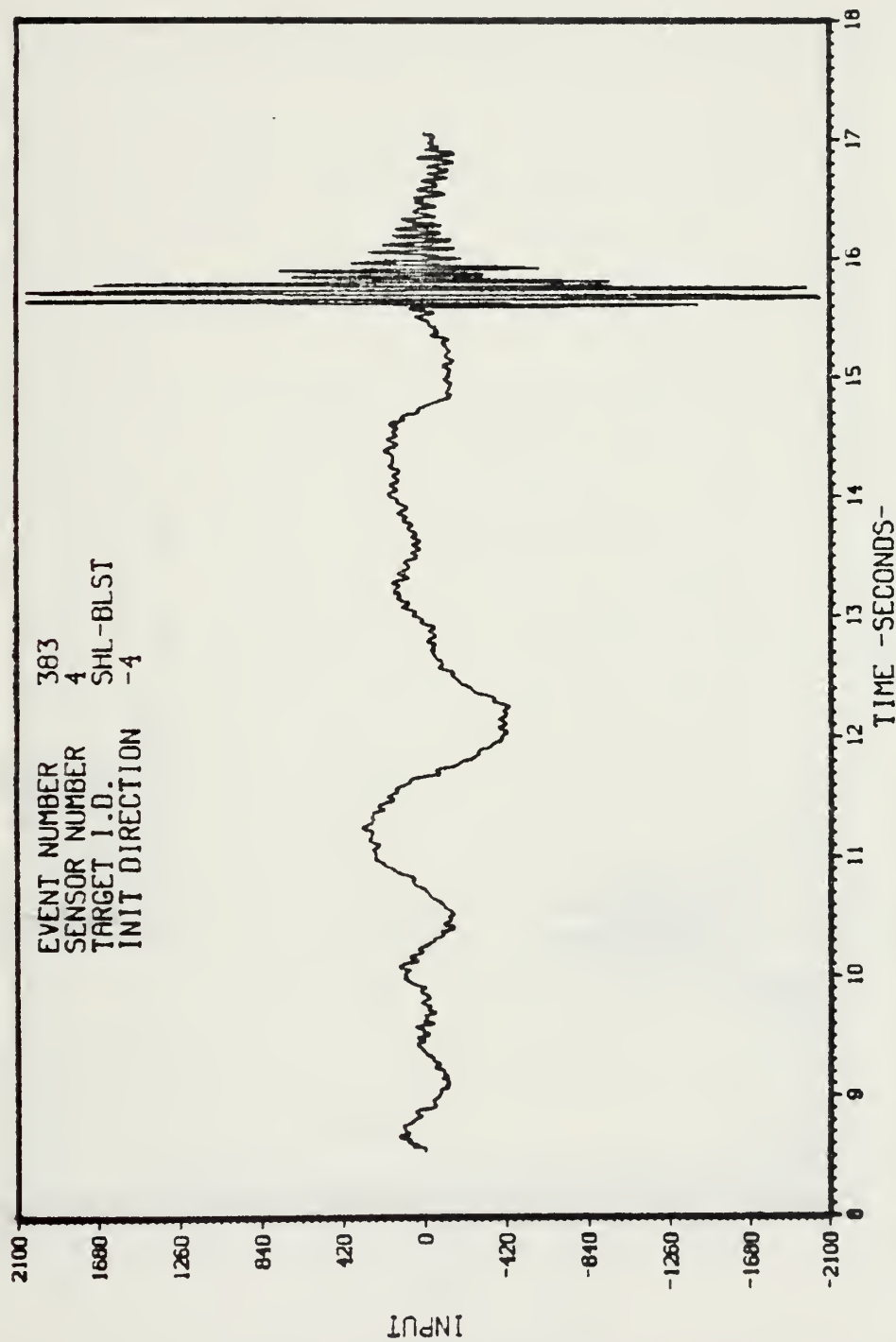


Figure 6.15 Amplitude Response for Event 383





# SENSOR POWER -VS- FREQUENCY

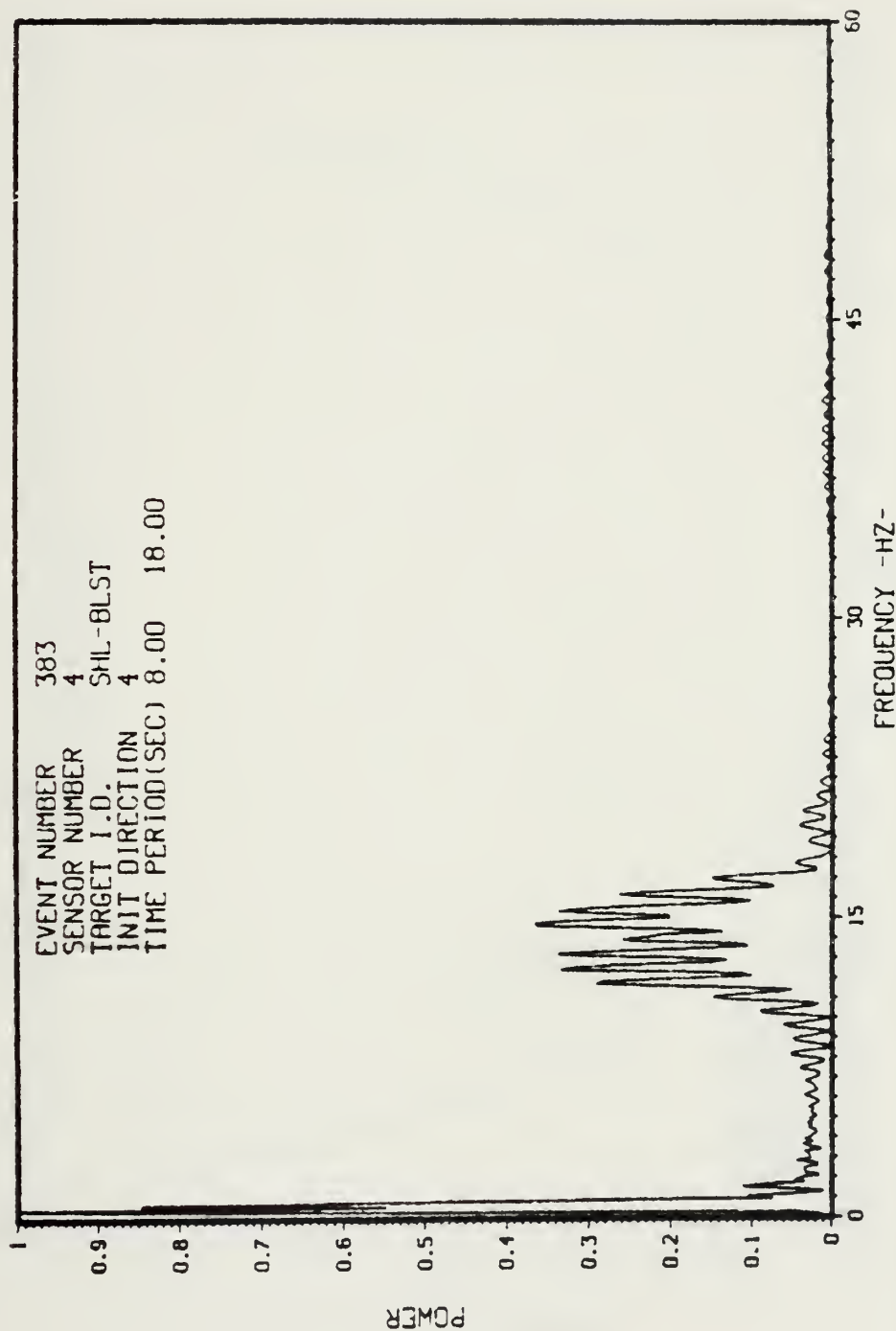


Figure 6.16 Frequency Response for Event 383



# LEAST MEAN SQUARES POLYNOMIAL

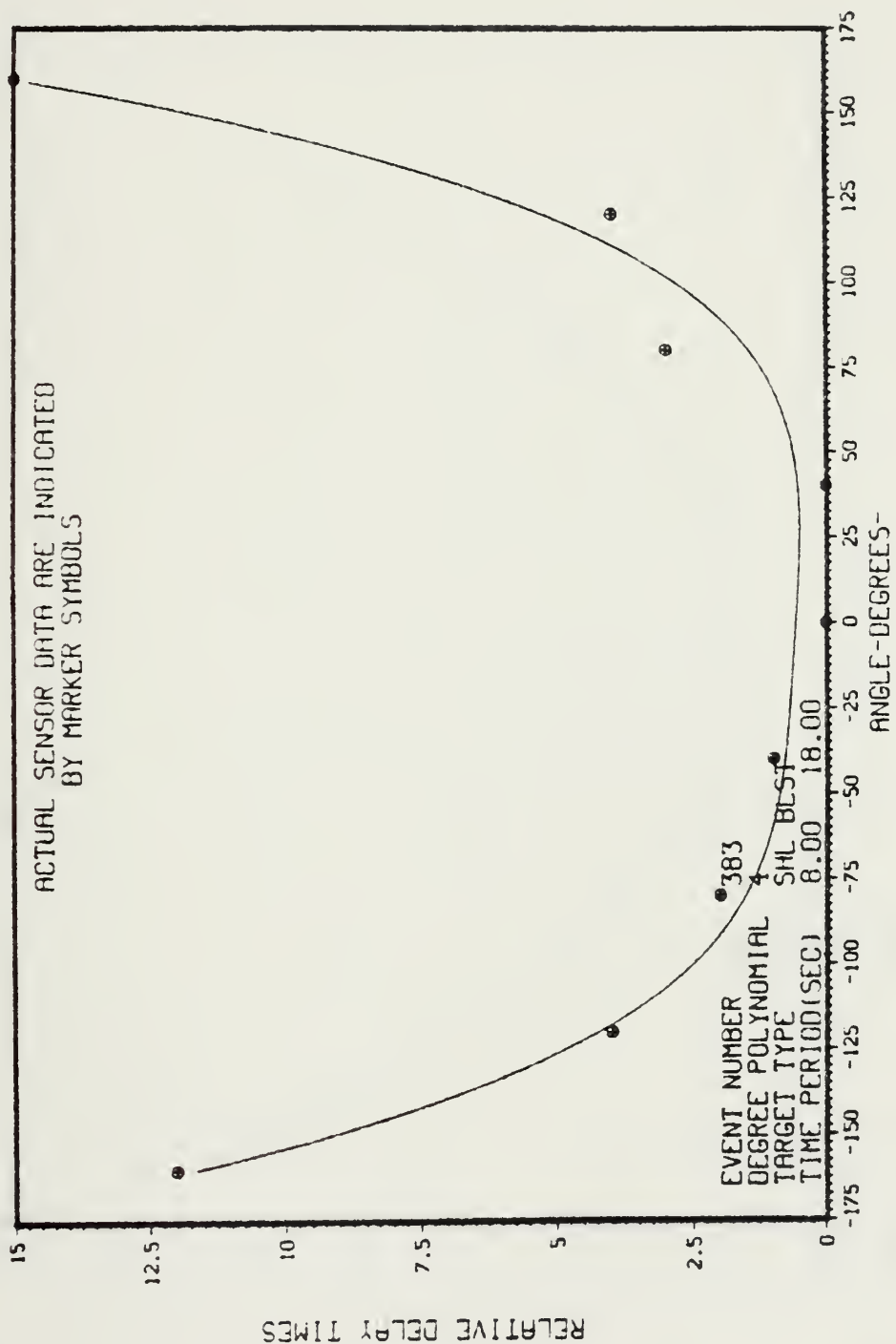


Figure 6.17 Fourth Degree LMSP Matched Filter Direction for Event 383



# LEAST MEAN SQUARES POLYNOMIAL

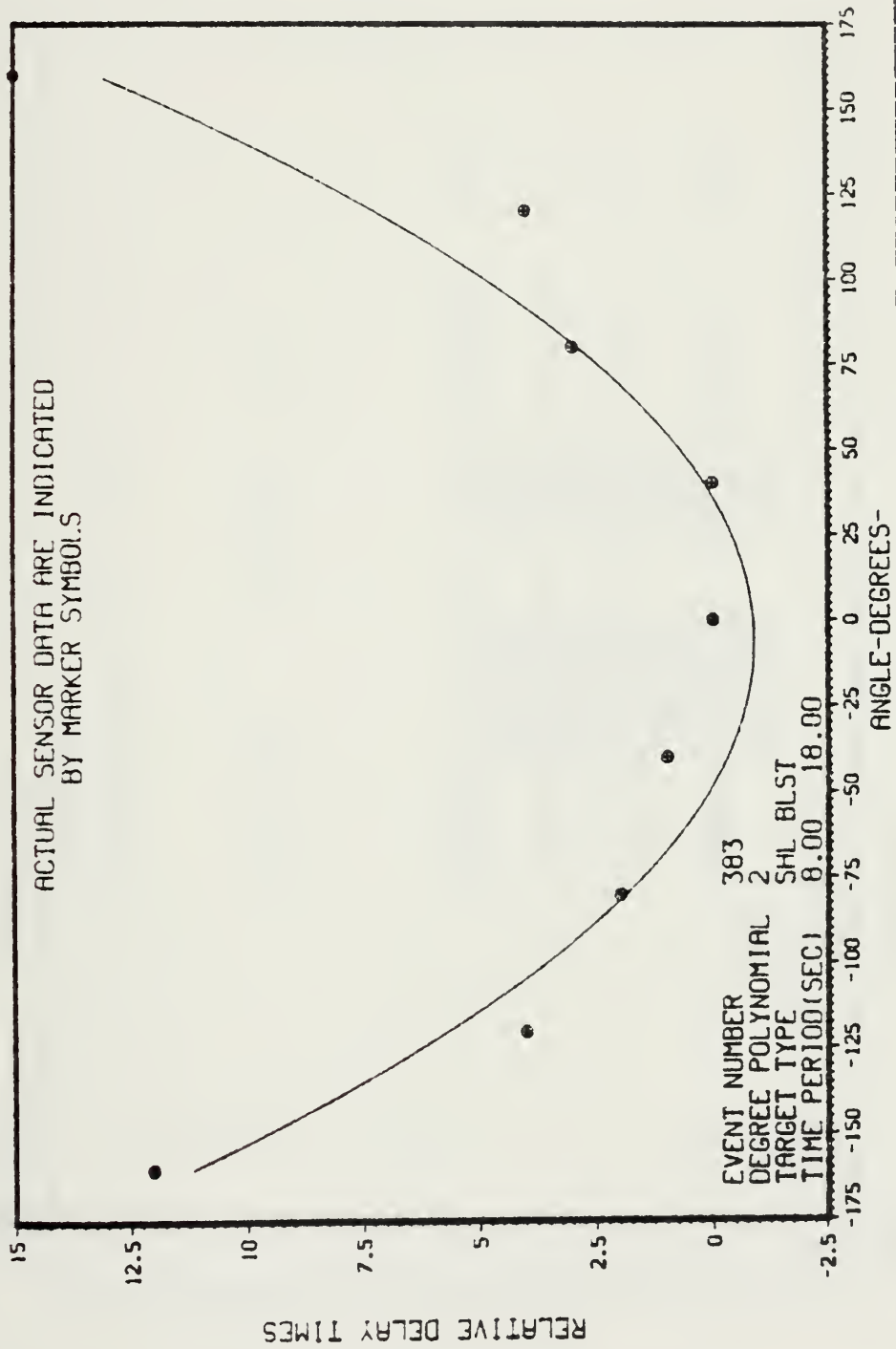


Figure 6.18 Second Degree LMSP Matched Filter Direction for Event 383



# MULTIPLE TARGET - MATCHED FILTER OUTPUT

EVENT NUMBER 383

TIME PERIOD(SEC) 8.00 18.00

SHELL BLAST DIRECTION - 28.00

SIMULATED TRKD VEHICLE TARGET FREQUENCY	0.00
AMPLITUDE 0.0000	
DIRECTION 0.0000	
SIMULATED WHLD VEHICLE TARGET FREQUENCY	0.00
AMPLITUDE 0.0000	
DIRECTION 0.0000	
SIMULATED HELICOPTER TARGET FREQUENCY	0.00
AMPLITUDE 0.0000	
DIRECTION 0.0000	
SIMULATED PERSONNEL TARGET FREQUENCY	0.00
AMPLITUDE 0.0000	
DIRECTION 0.0000	

Figure 6.19 LMSP Multiple Target Direction Summary for Event 383





# LEAST MEAN SQUARES POLYNOMIAL

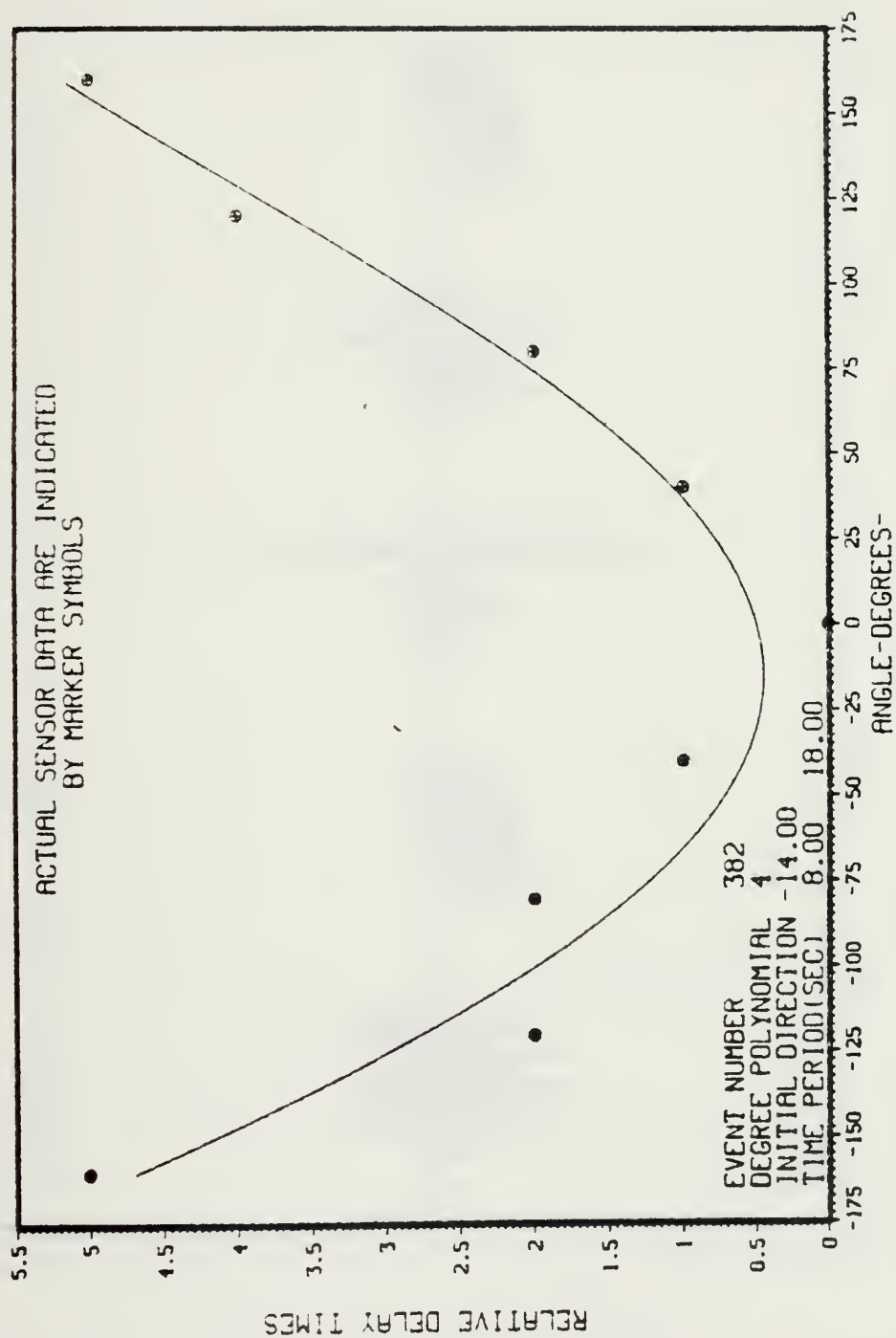


Figure 6.20 LMSP Initial Direction for Event 382



# MATCHED FILTER RESPONSE

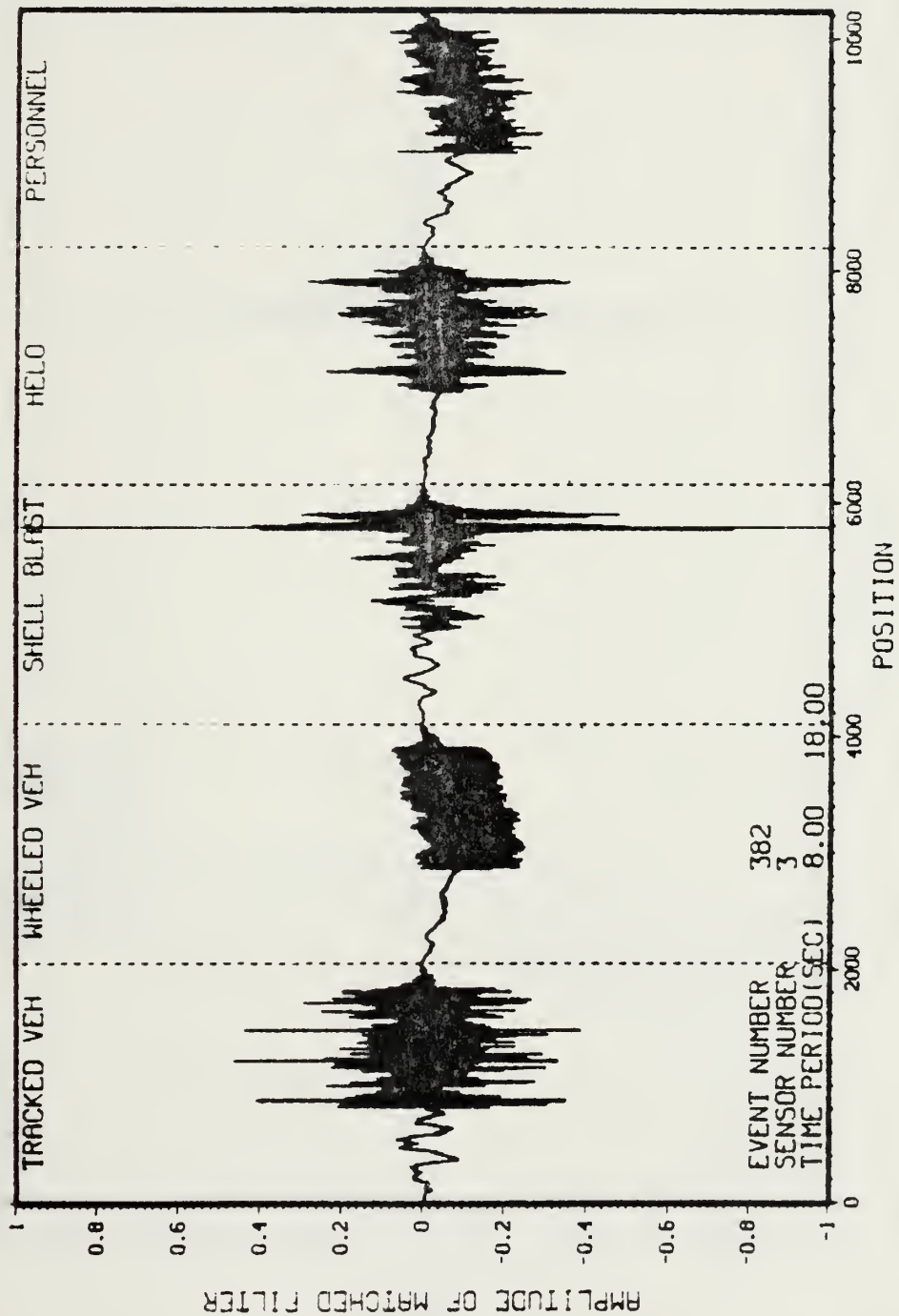


Figure 6.21 Matched Filter Response for Event 382



# SENSOR INPUT - VS - TIME

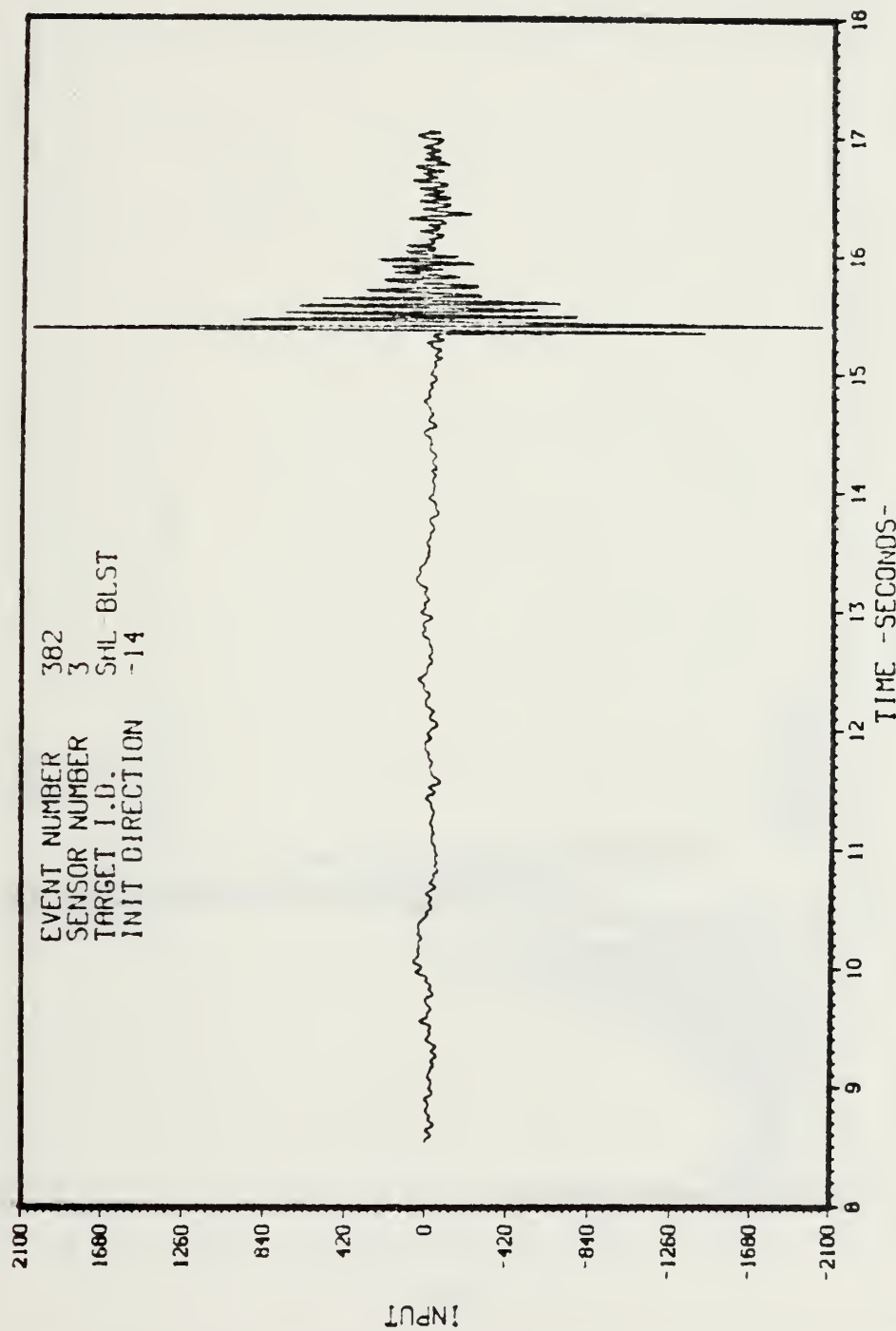


Figure 6.22 Amplitude Response for Event 382



# SENSOR POWER -VS- FREQUENCY

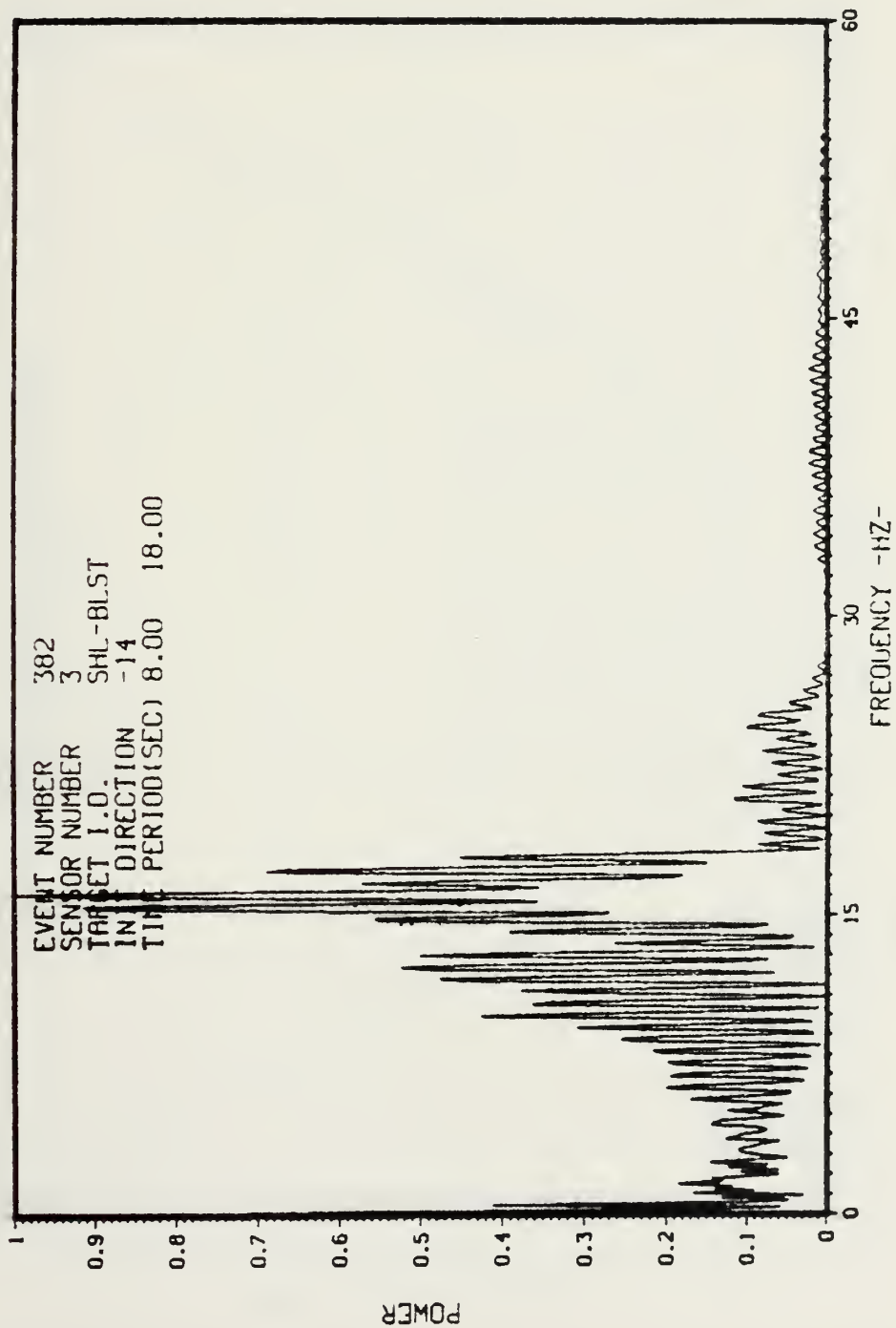


Figure 6.23 Frequency Response for Event 382





# LEAST MEAN SQUARES POLYNOMIAL

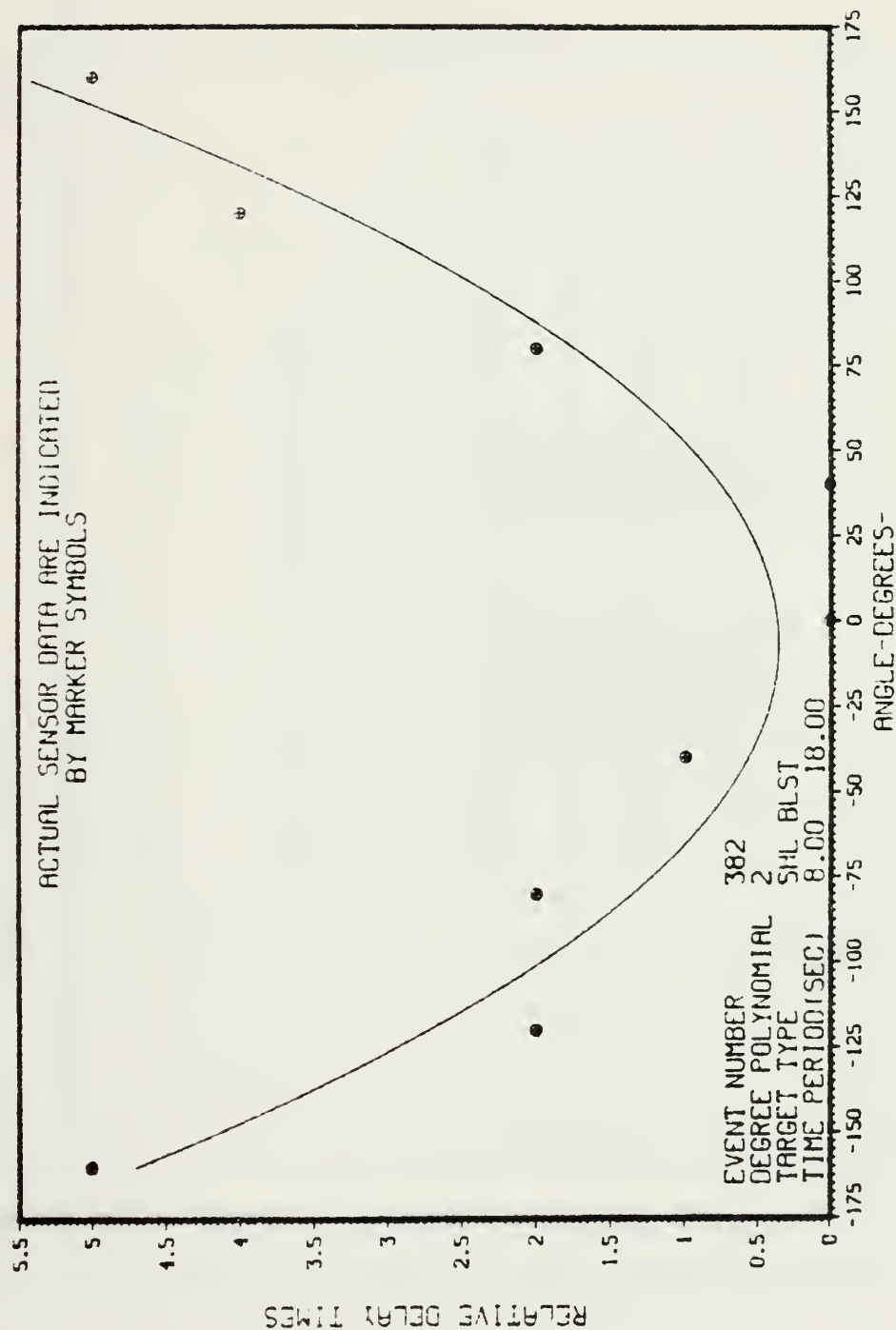


Figure 6.24 LMSP Matched Filter Direction for Event 382



# MULTIPLE TARGET - MATCHED FILTER OUTPUT

EVENT NUMBER 382

TIME PERIOD(SEC) 8.00 18.00

SHELL BLAST DIRECTION - -6.00

.

SIMULATED TRKV VEHICLE TARGET FREQUENCY	0.00
AMPLITUDE 0.0000	
DIRECTION 0.0000	
SIMULATED WHLD VEHICLE TARGET FREQUENCY	0.00
AMPLITUDE 0.0000	
DIRECTION 0.0000	
SIMULATED HELICOPTER TARGET FREQUENCY	0.00
AMPLITUDE 0.0000	
DIRECTION 0.0000	
SIMULATED PERSONNEL TARGET FREQUENCY	0.00
AMPLITUDE 0.0000	
DIRECTION 0.0000	

Figure 6.25 LMSP Multiple Target Direction Summary for Event 382



# LEAST MEAN SQUARES POLYNOMIAL

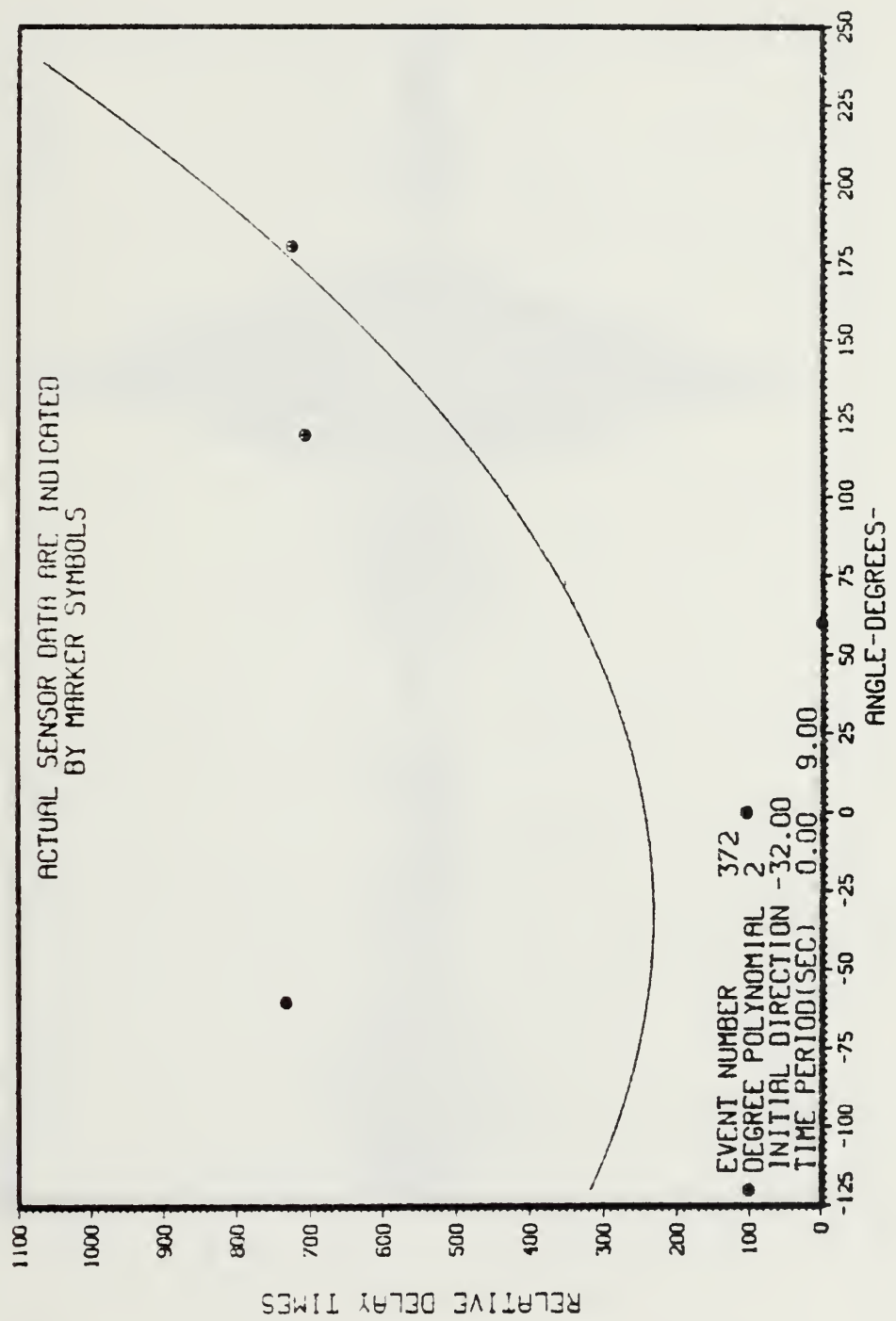


Figure 6.26 LMSP Initial Direction for Event 372



# MATCHED FILTER RESPONSE

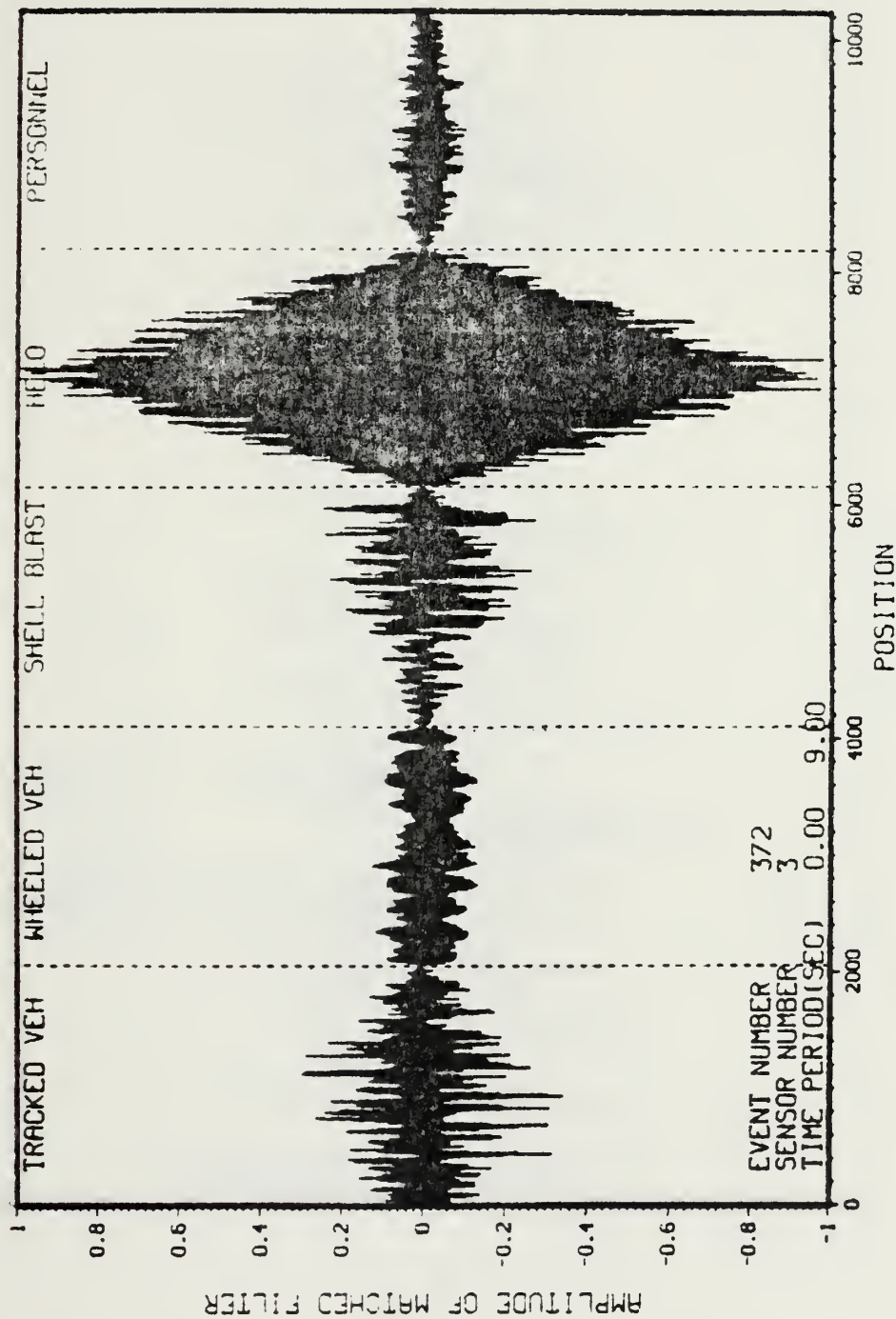


Figure 6.27 Matched Filter Response for Event 372





# SENSOR INPUT - VS - TIME

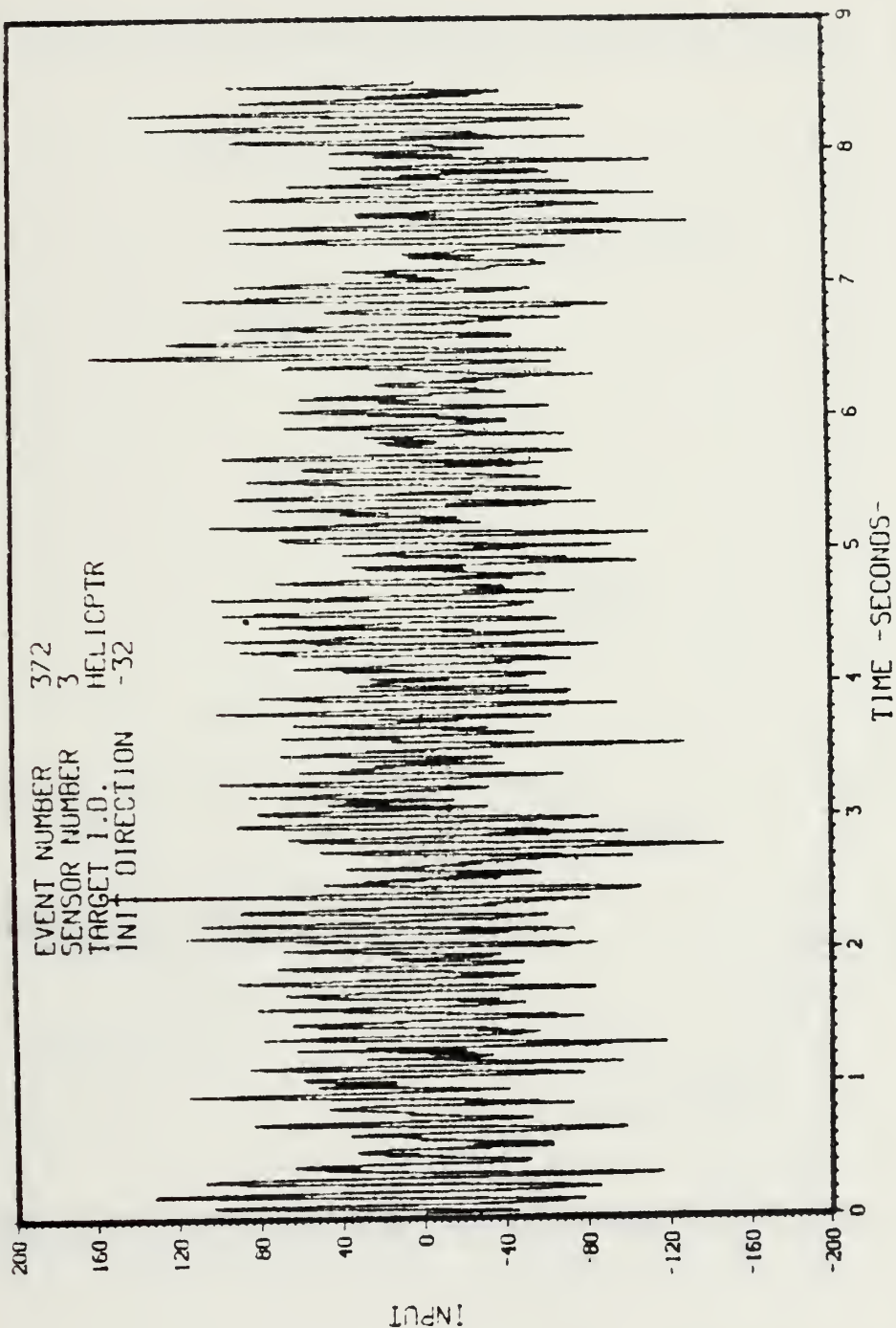


Figure 6.28 Amplitude Response for Event 372



# SENSOR INPUT - VS - TIME

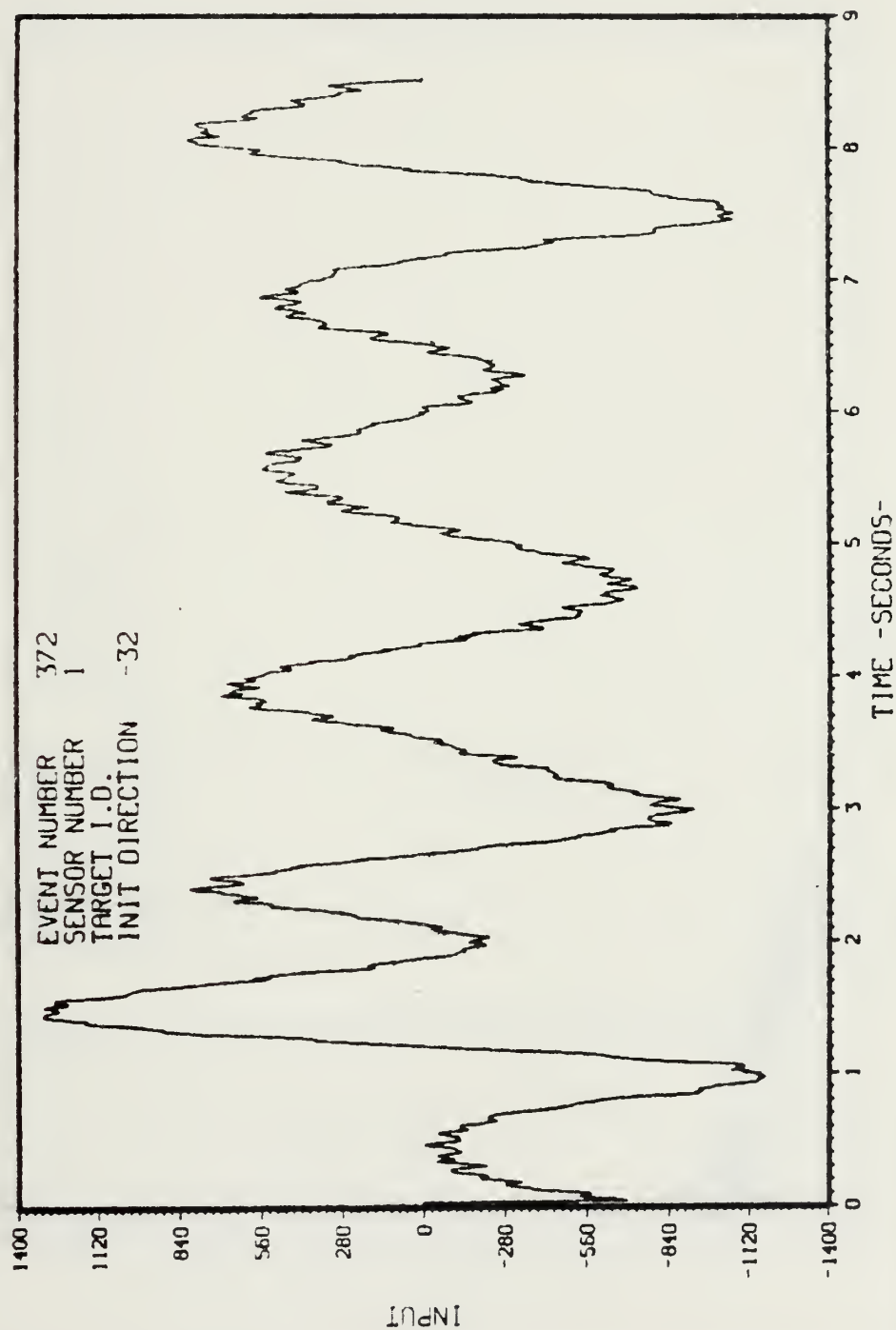


Figure 6.29 Amplitude Response of Malfunctioning Sensor for Event 372



# SENSOR POWER -VS- FREQUENCY

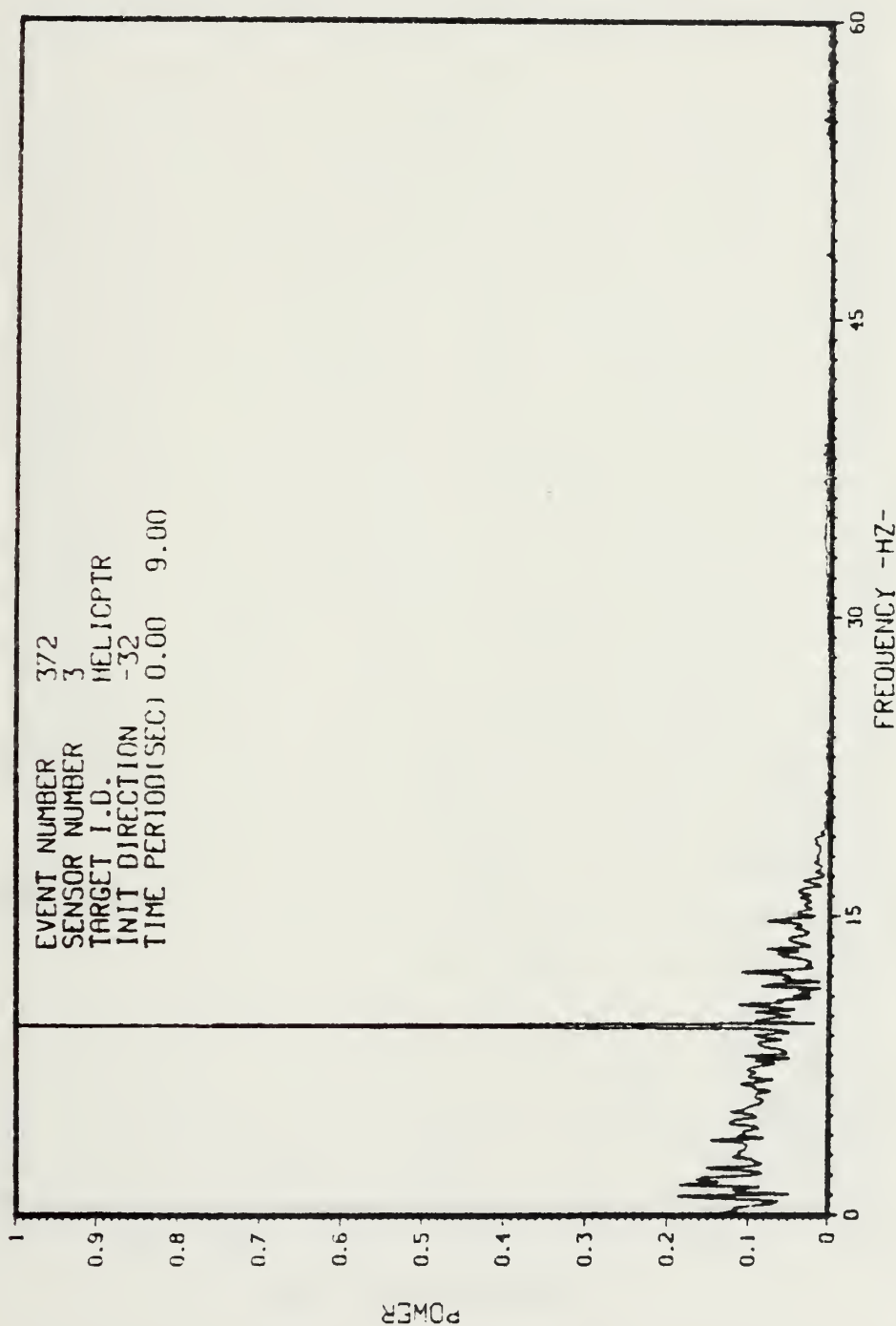


Figure 6.30 Frequency Response for Event 372



# LEAST MEAN SQUARES POLYNOMIAL

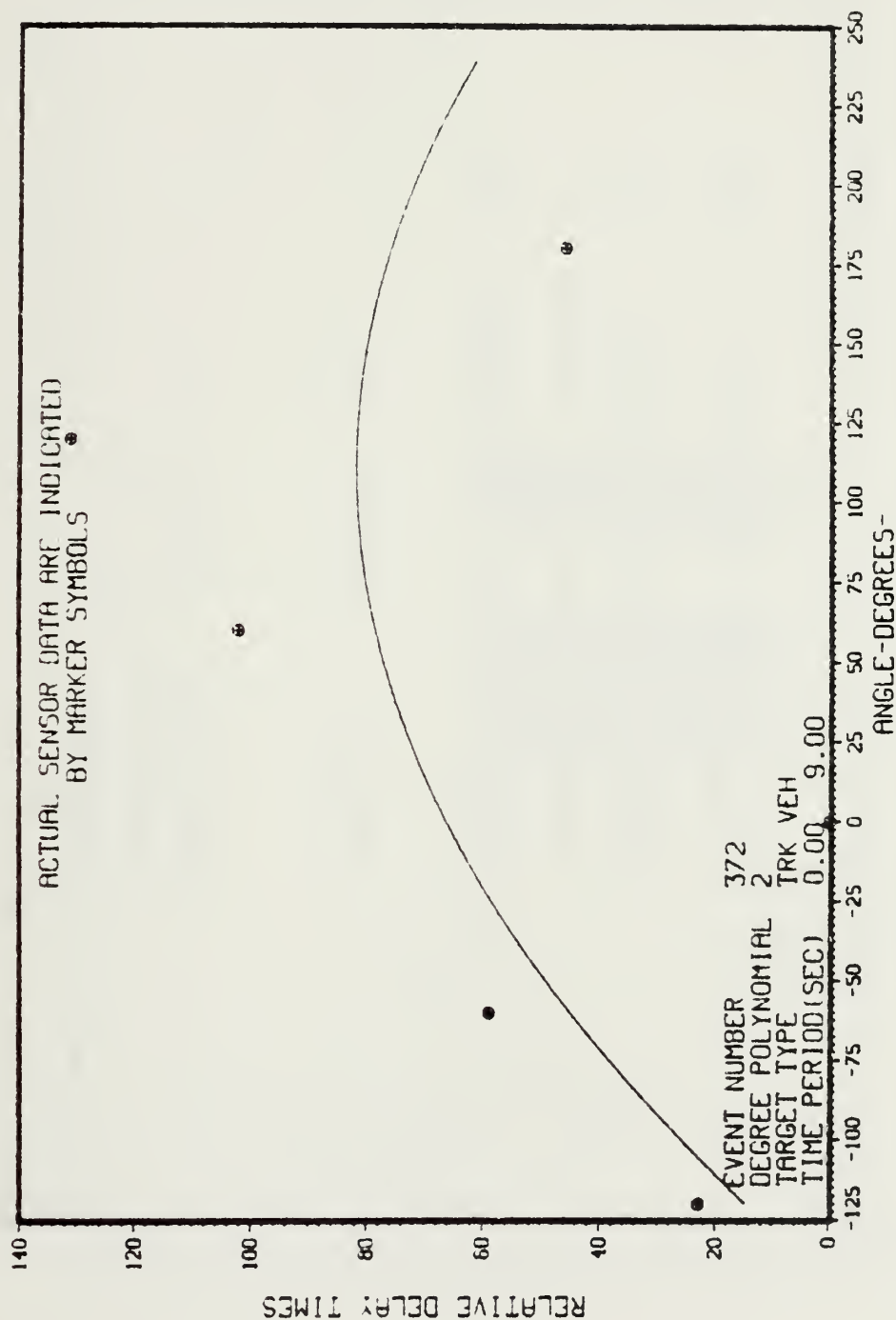


Figure 6.31 LMSP Matched Filter Direction for Event 372





# MULTIPLE TARGET - MATCHED FILTER OUTPUT

EVENT NUMBER	372
TIME PERIOD(SEC)	0.00 9.00
TRACKED VEHICLE	DIRECTION - 0.00
HELICOPTER	DIRECTION - 0.00
SIMULATED TRKD VEHICLE	TARGET FREQUENCY 0.00
AMPLITUDE	0.0000
DIRECTION	0.0000
SIMULATED WILD VEHICLE	TARGET FREQUENCY 0.00
AMPLITUDE	0.0000
DIRECTION	0.0000
SIMULATED HELICOPTER	TARGET FREQUENCY 0.00
AMPLITUDE	0.0000
DIRECTION	0.0000
SIMULATED PERSONNEL	TARGET FREQUENCY 0.00
AMPLITUDE	0.0000
DIRECTION	0.0000

Figure 6.32 LMSP Multiple Target Direction Summary for Event 372



# LEAST MEAN SQUARES POLYNOMIAL

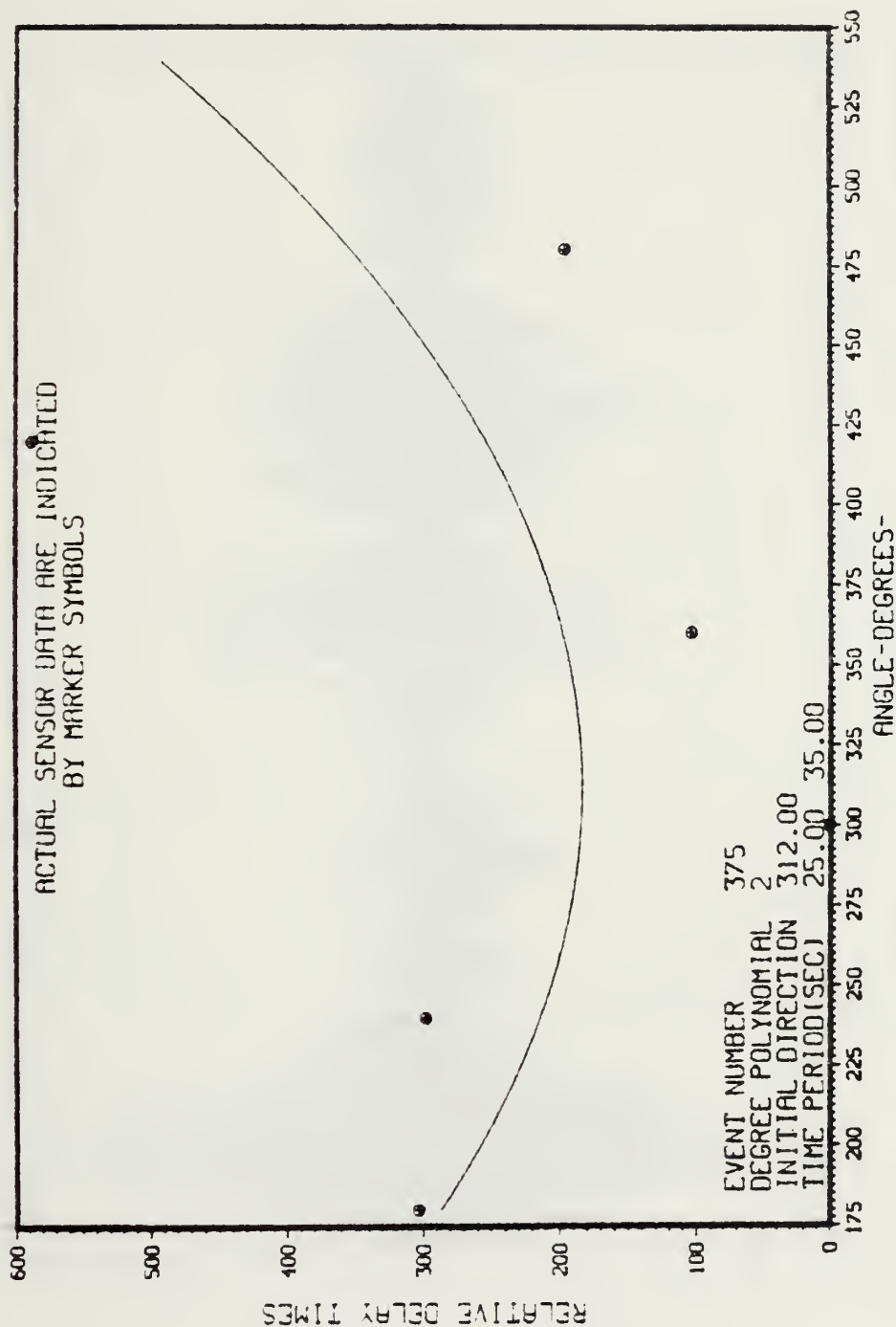


Figure 6.33 LMSP Initial Direction for Event 375



# MATCHED FILTER RESPONSE

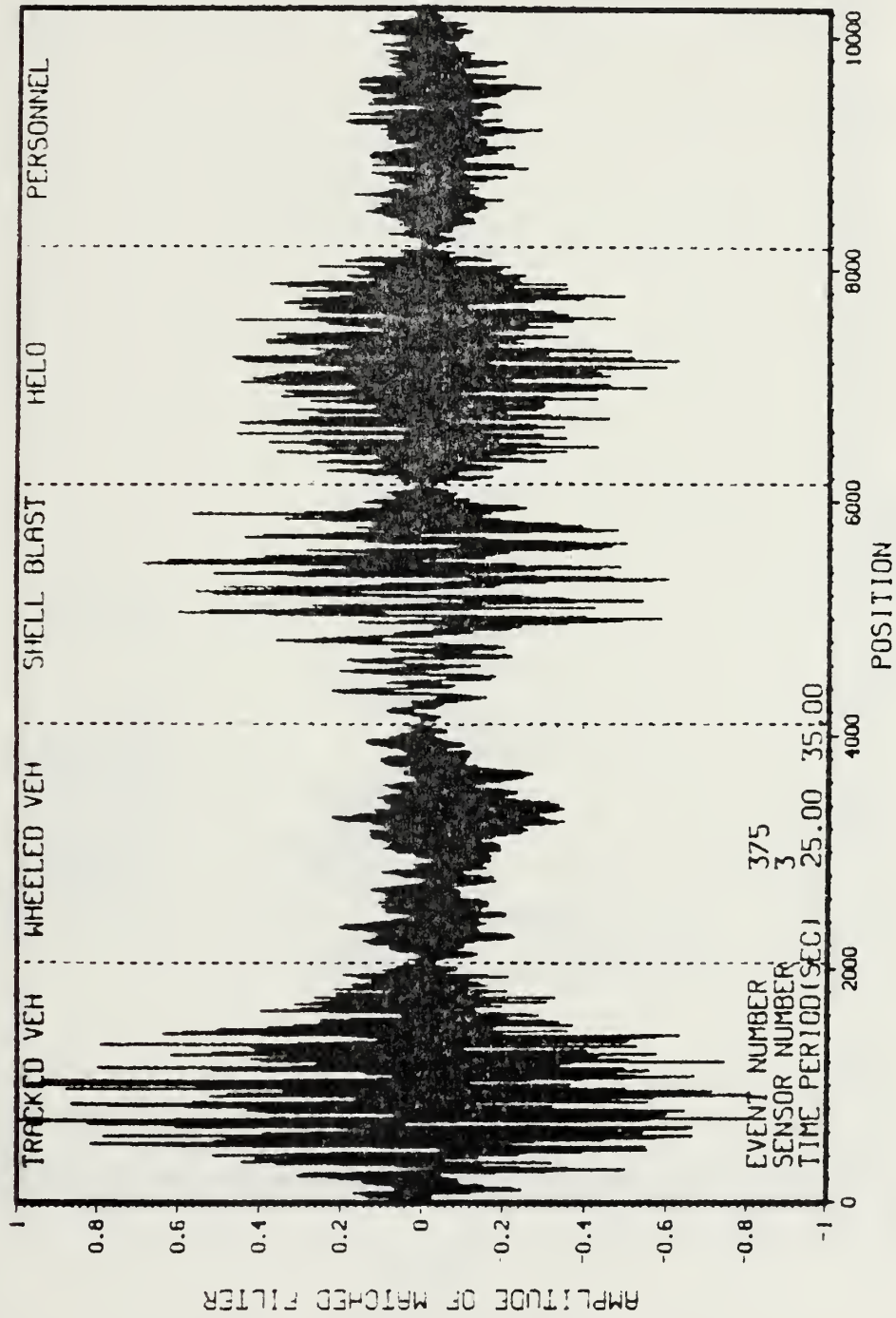


Figure 6.34 Matched Filter Response for Event 375



# SENSOR INPUT - VS - TIME

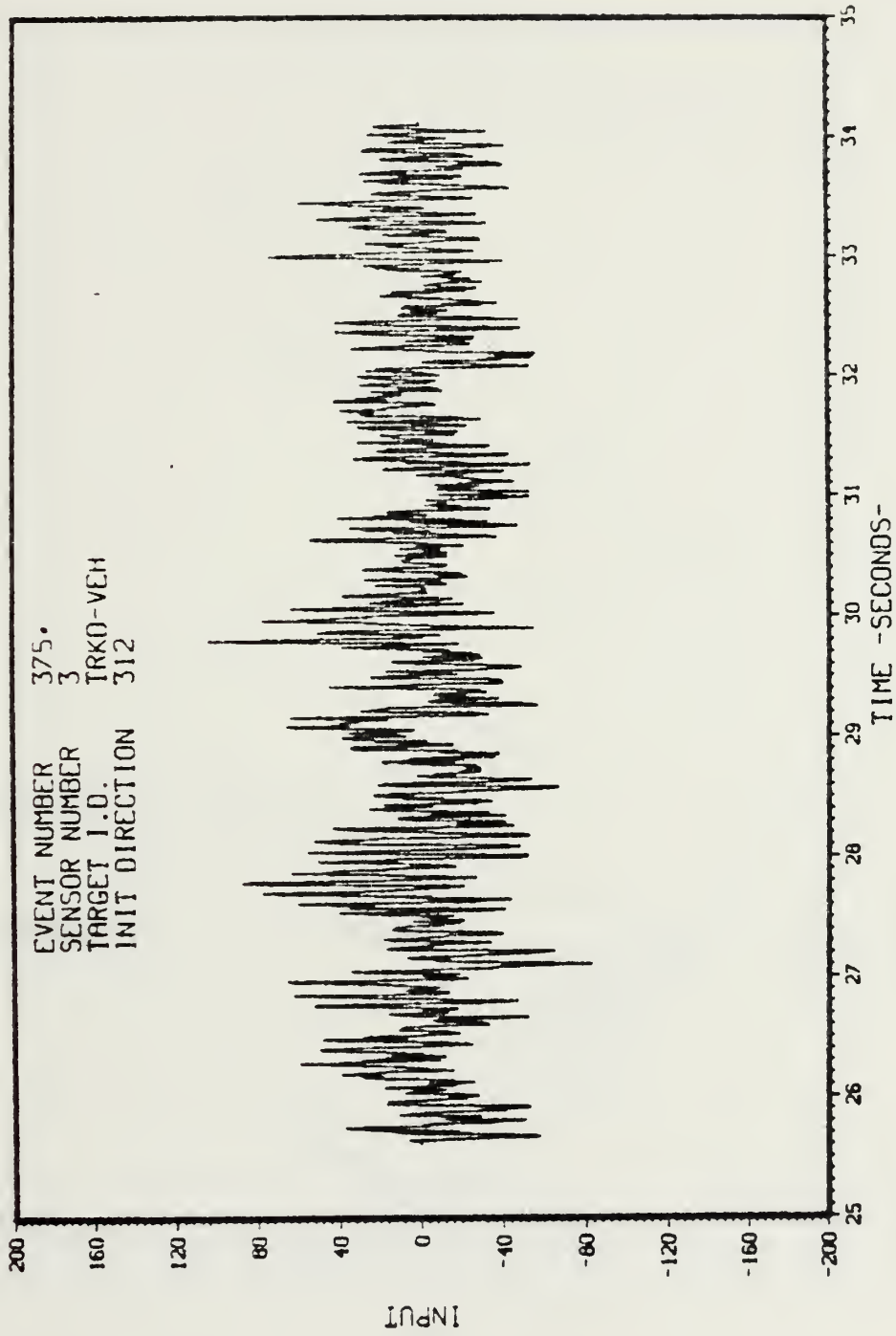


Figure 6.35 Amplitude Response for Event 375





# SENSOR INPUT - VS - TIME

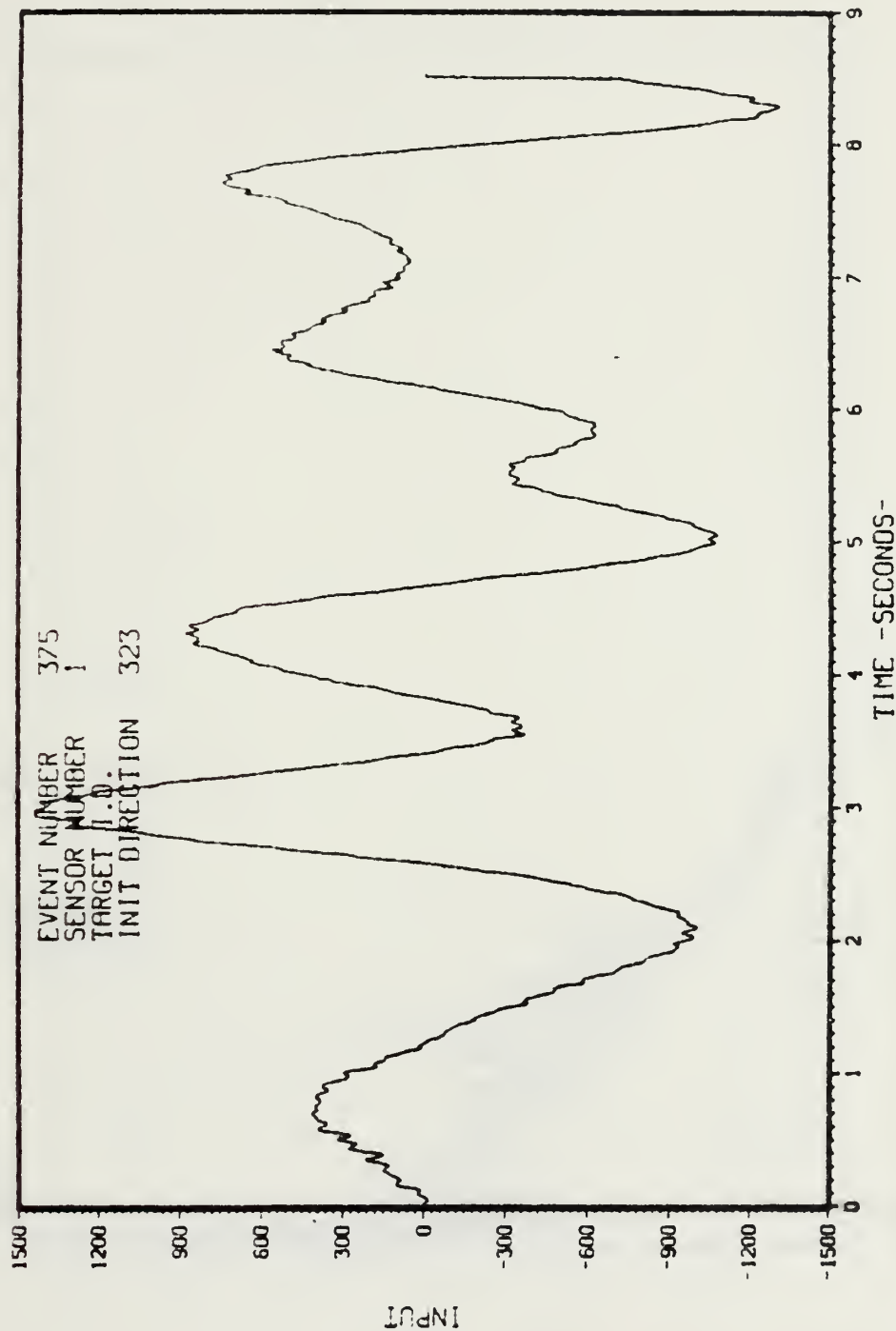


Figure 6.36 Amplitude Response of Malfunctioning Sensor for Event 375



# SENSOR POWER -VS- FREQUENCY

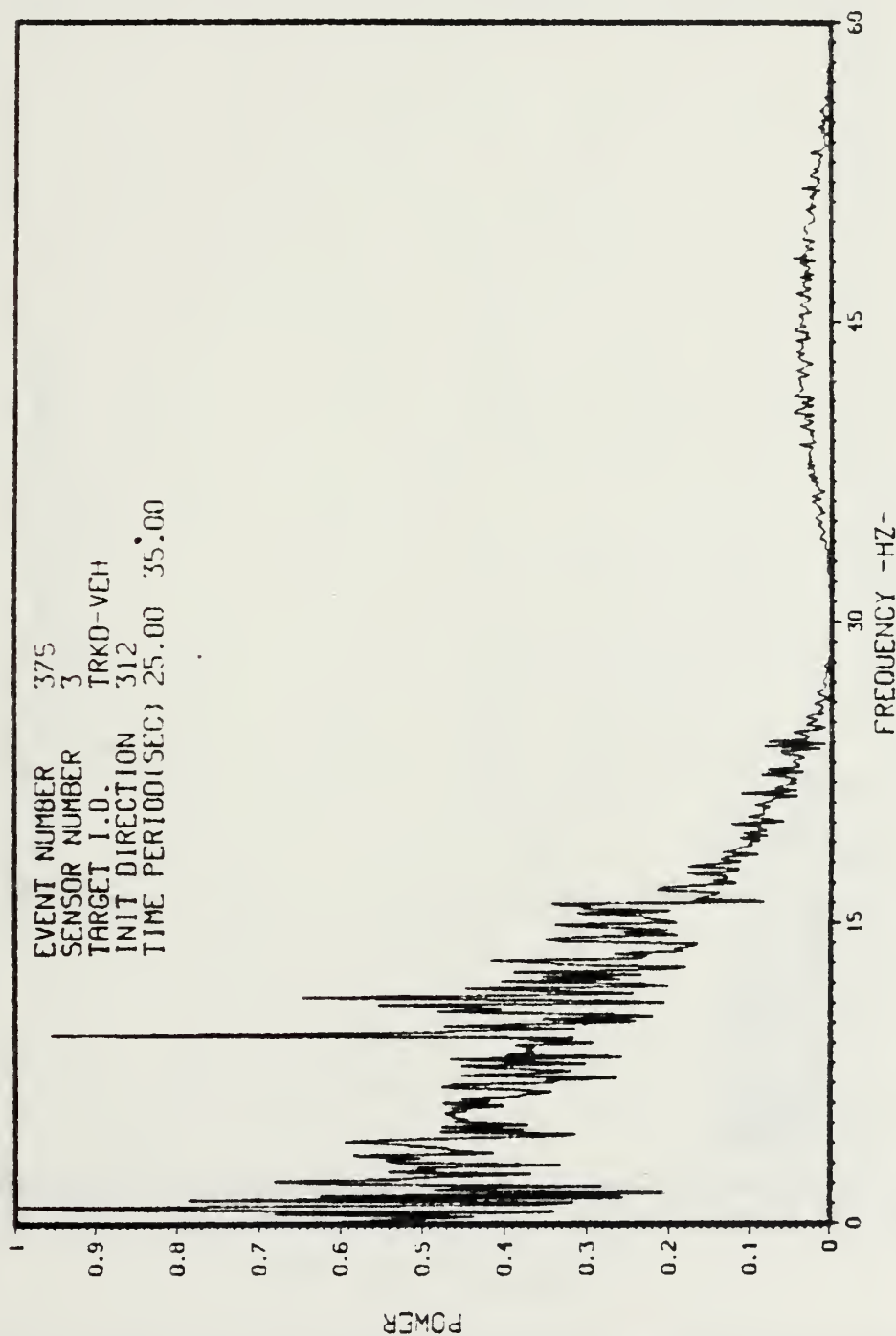


Figure 6.37 Frequency Response for Event 375



# LEAST MEAN SQUARES POLYNOMIAL

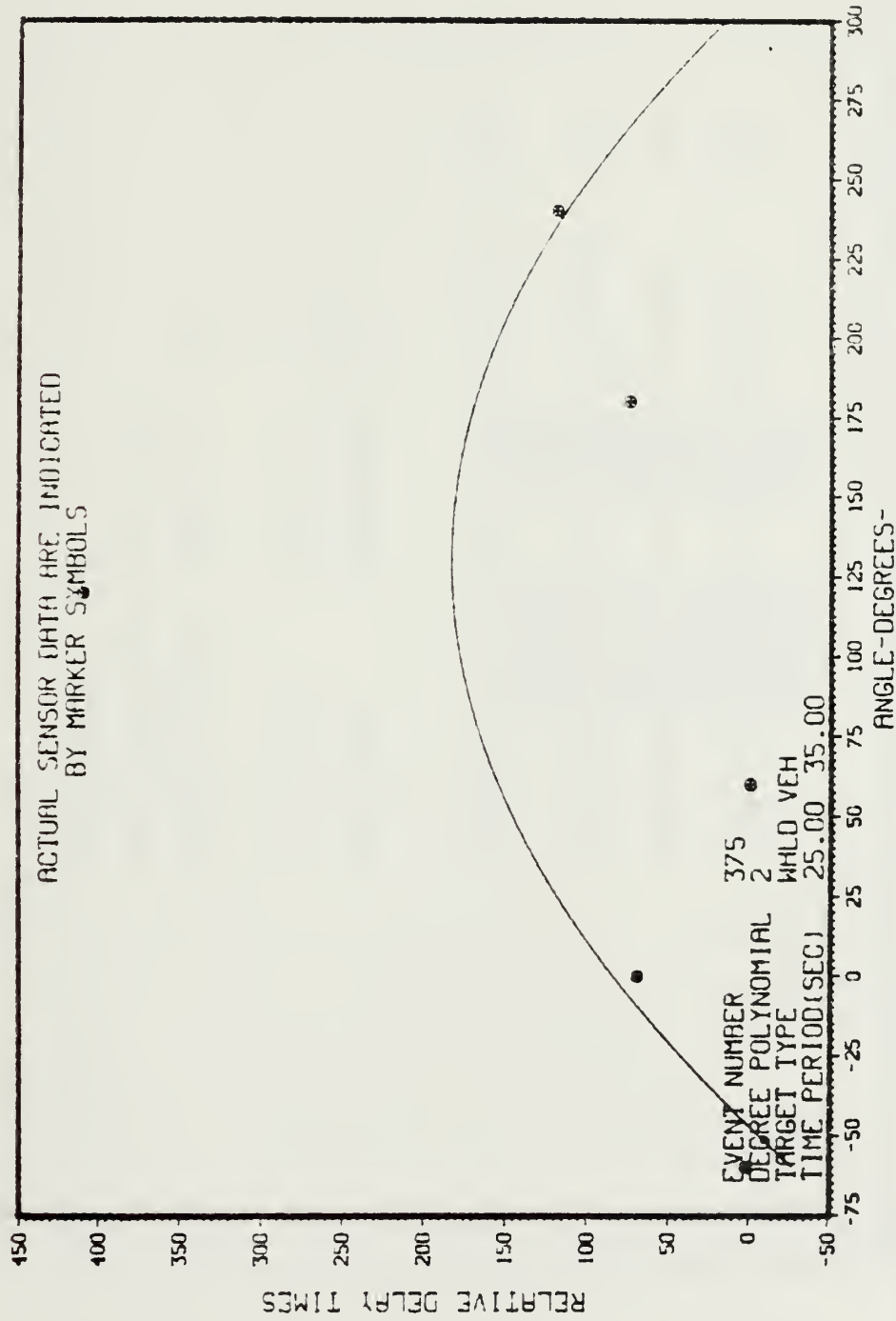


Figure 6.38 LMSP Matched Filter Direction for Event 375



# MULTIPLE TARGET - MATCHED FILTER OUTPUT

EVENT NUMBER	375	
TIME PERIOD(SEC)	25.00 35.00	
TRACKED VEHICLE	DIRECTION - 0.00	
SHELL BLAST	DIRECTION - 312.00	
HELICOPTER	DIRECTION - 0.00	
SIMULATED TRKD VEHICLE	TARGET FREQUENCY	0.00
AMPLITUDE	0.0000	
DIRECTION	0.0000	
SIMULATED WHLD VEHICLE	TARGET FREQUENCY	0.00
AMPLITUDE	0.0000	
DIRECTION	0.0000	
SIMULATED HELICOPTER	TARGET FREQUENCY	0.00
AMPLITUDE	0.0000	
DIRECTION	0.0000	
SIMULATED PERSONNEL	TARGET FREQUENCY	0.00
AMPLITUDE	0.0000	
DIRECTION	0.0000	

Figure 6.39 LMSP Multiple Target Direction Summary for Event 375





# LEAST MEAN SQUARES POLYNOMIAL

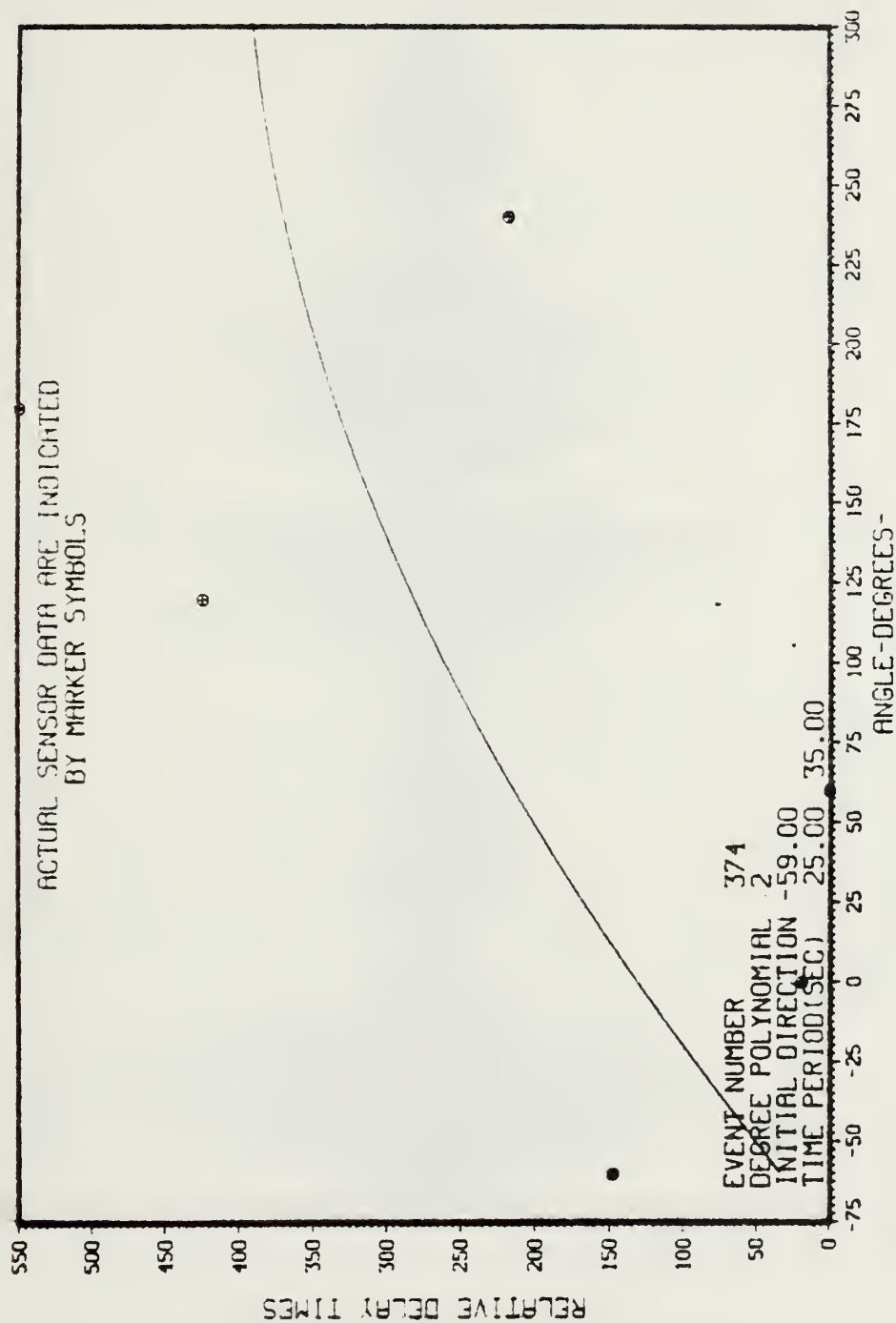


Figure 6.40 LMSP Initial Direction for Event 374



# MATCHED FILTER RESPONSE

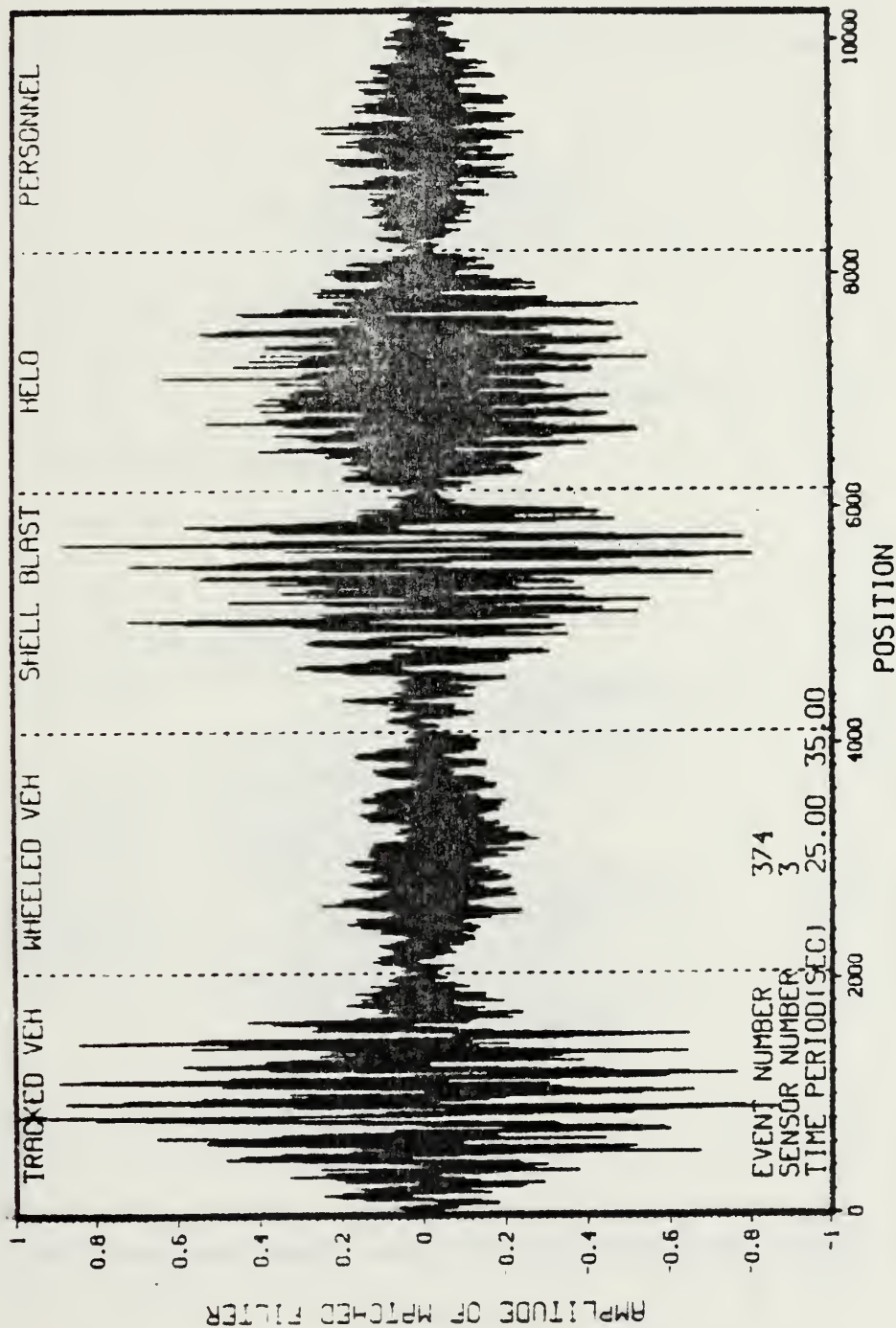


Figure 6.41 Matched Filter Response for Event 374



# SENSOR INPUT - VS - TIME

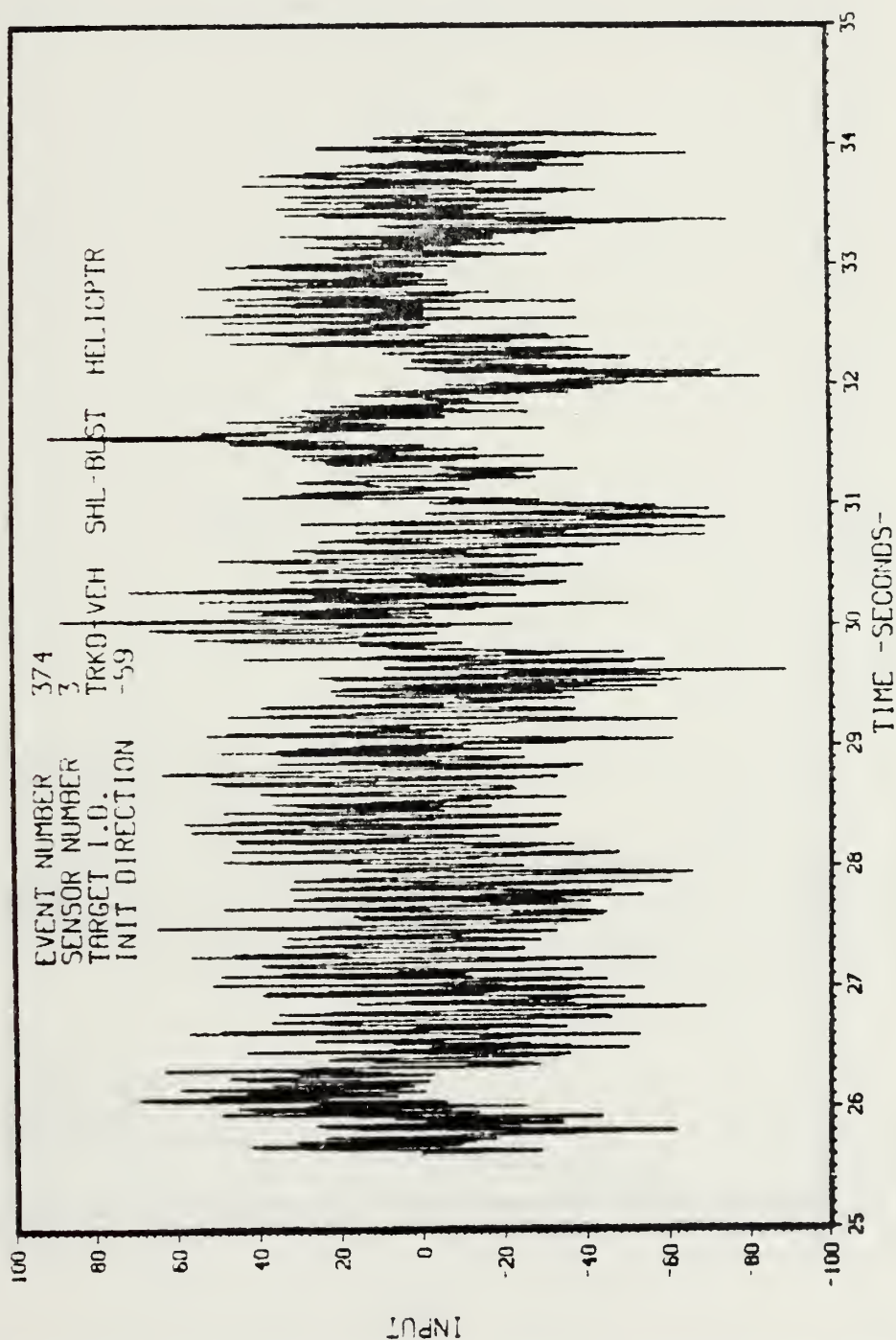


Figure 6.42 Amplitude Response for Event 374



# SENSOR INPUT - VS - TIME

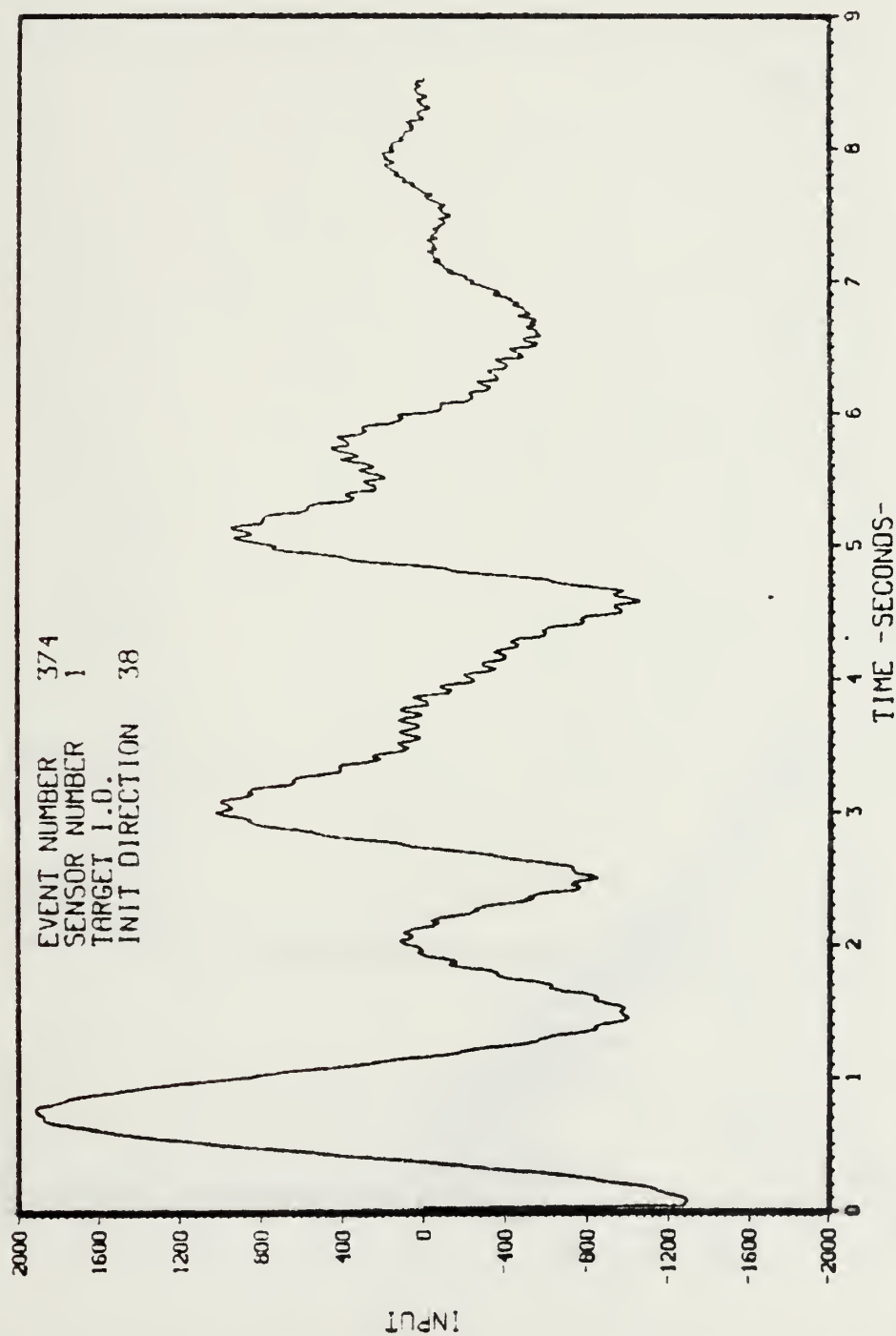


Figure 6.43 Amplitude Response of Malfunctioning Sensor for Event 374





# SENSOR POWER -VS- FREQUENCY

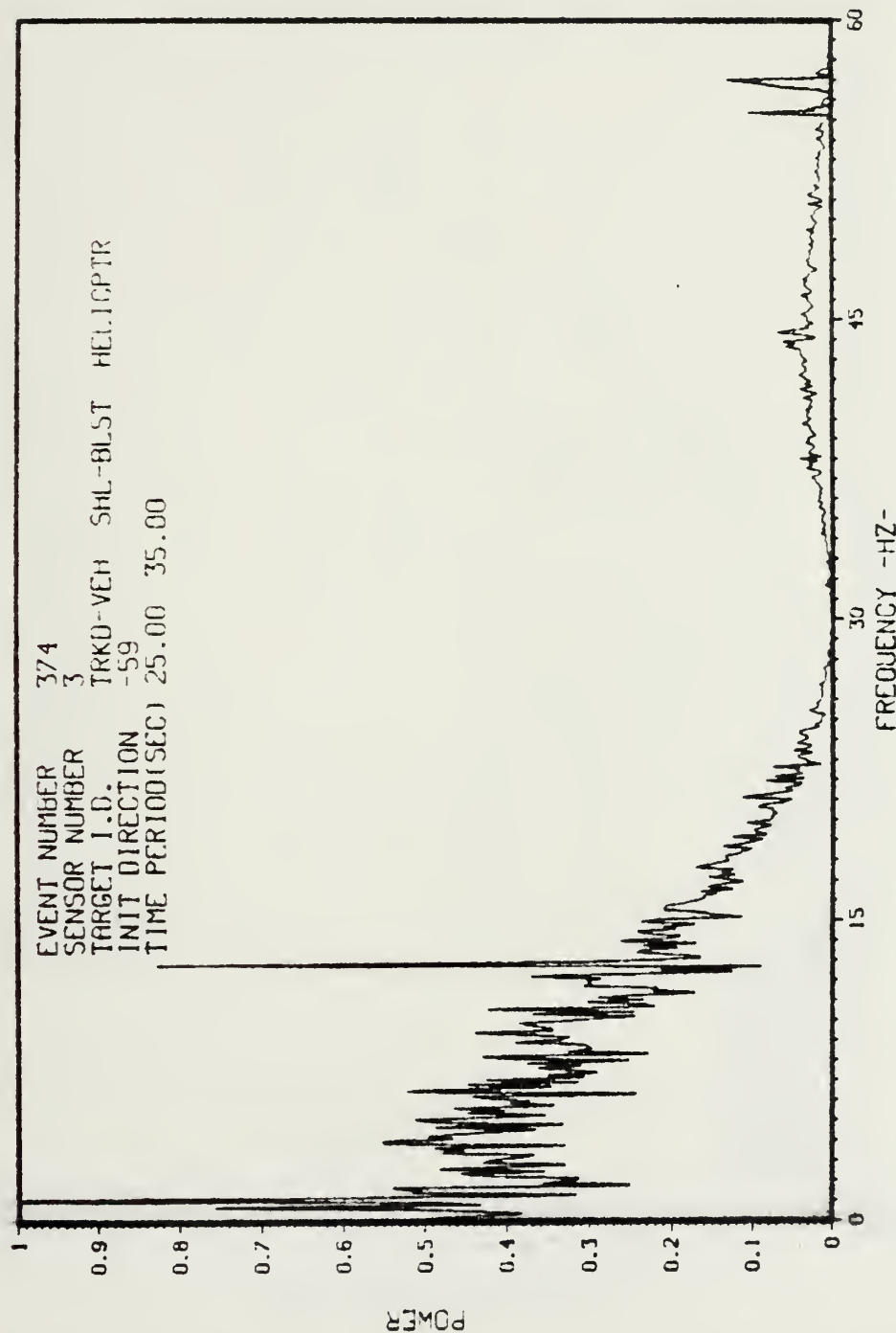


Figure 6.44 Frequency Response for Event 374



# LEAST MEAN SQUARES POLYNOMIAL

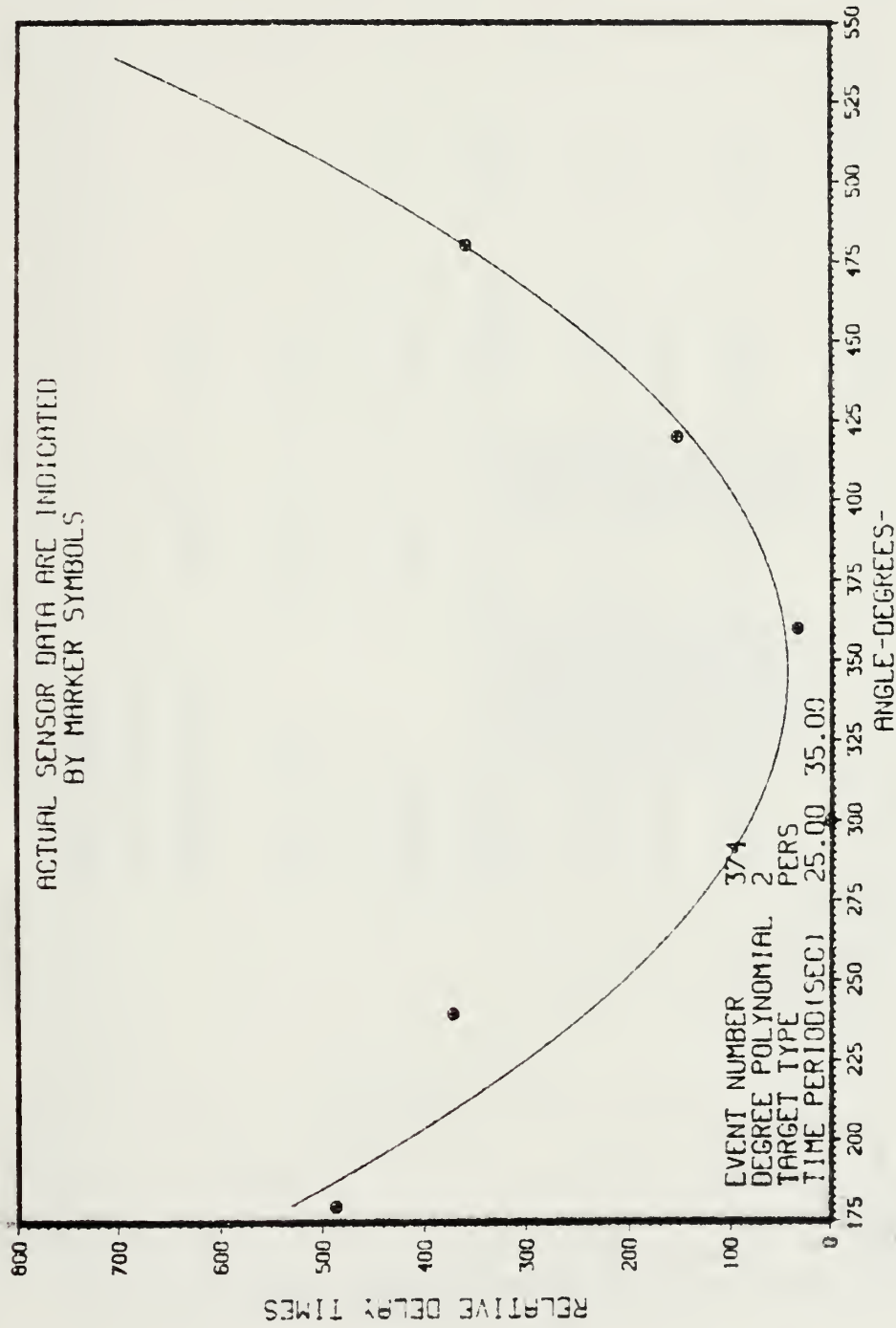


Figure 6.45 LMSP Matched Filter Direction for Event 374



# MULTIPLE TARGET - MATCHED FILTER OUTPUT

EVENT NUMBER	374		
TIME PERIOD(SEC)	25.00	35.00	
TRACKED VEHICLE	DIRECTION	--59.00	
SHELL BLAST	DIRECTION	--59.00	
PERSONNEL	DIRECTION	- 347.00	
SIMULATED TRKD VEHICLE	TARGET FREQUENCY		0.00
AMPLITUDE	0.0000		
DIRECTION	0.0000		
SIMULATED WILD VEHICLE	TARGET FREQUENCY		0.00
AMPLITUDE	0.0000		
DIRECTION	0.0000		
SIMULATED HELICOPTER	TARGET FREQUENCY		0.00
AMPLITUDE	0.0000		
DIRECTION	0.0000		
SIMULATED PERSONNEL	TARGET FREQUENCY		0.00
AMPLITUDE	0.0000		
DIRECTION	0.0000		

Figure 6.46 LMSP Multiple Target Direction Summary for Event 374



# LEAST MEAN SQUARES POLYNOMIAL

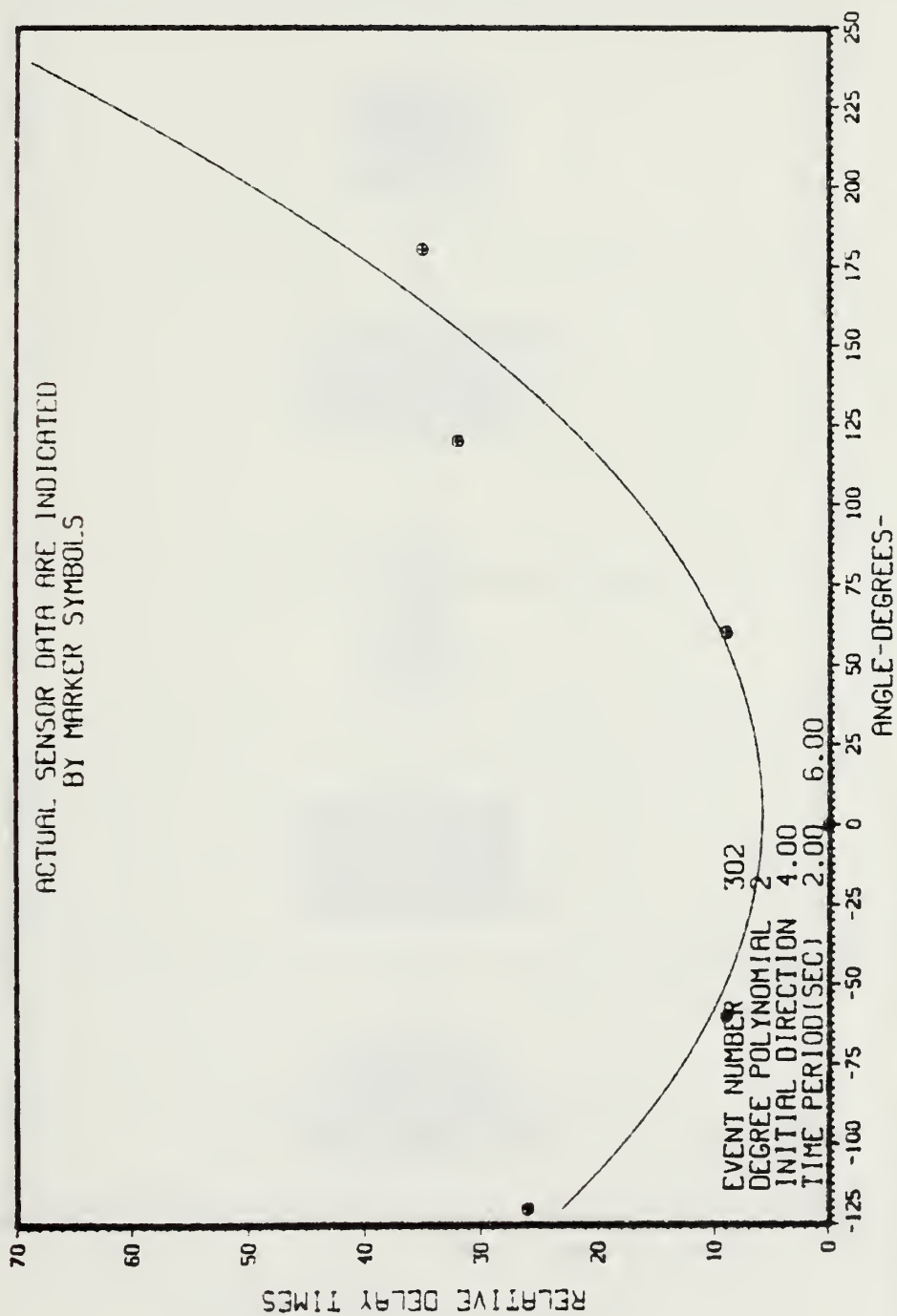


Figure 6.47 LMSP Initial Direction for Event 302





# MATCHED FILTER RESPONSE

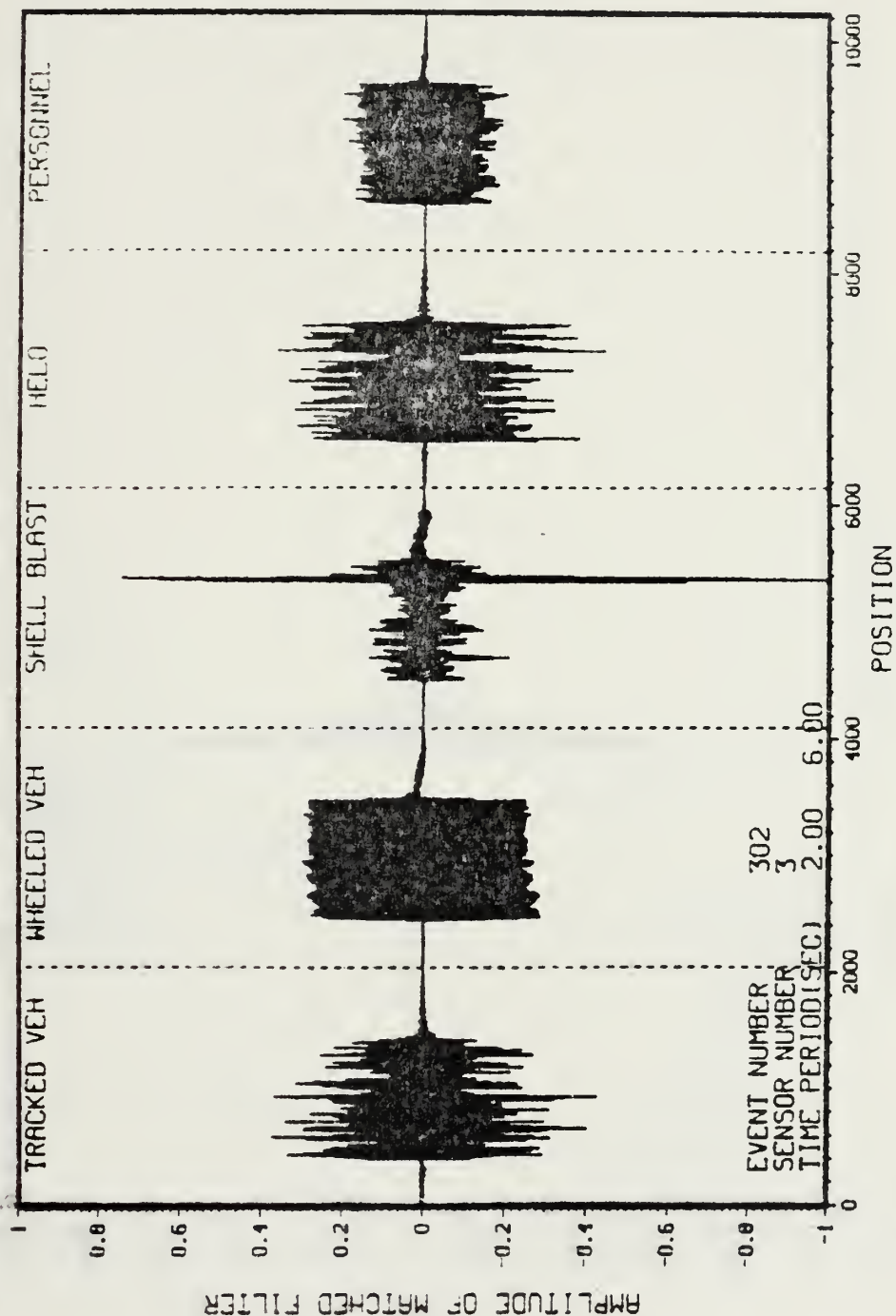


Figure 6.48 Matched Filter Response for Event 302



# SENSOR INPUT - VS - TIME

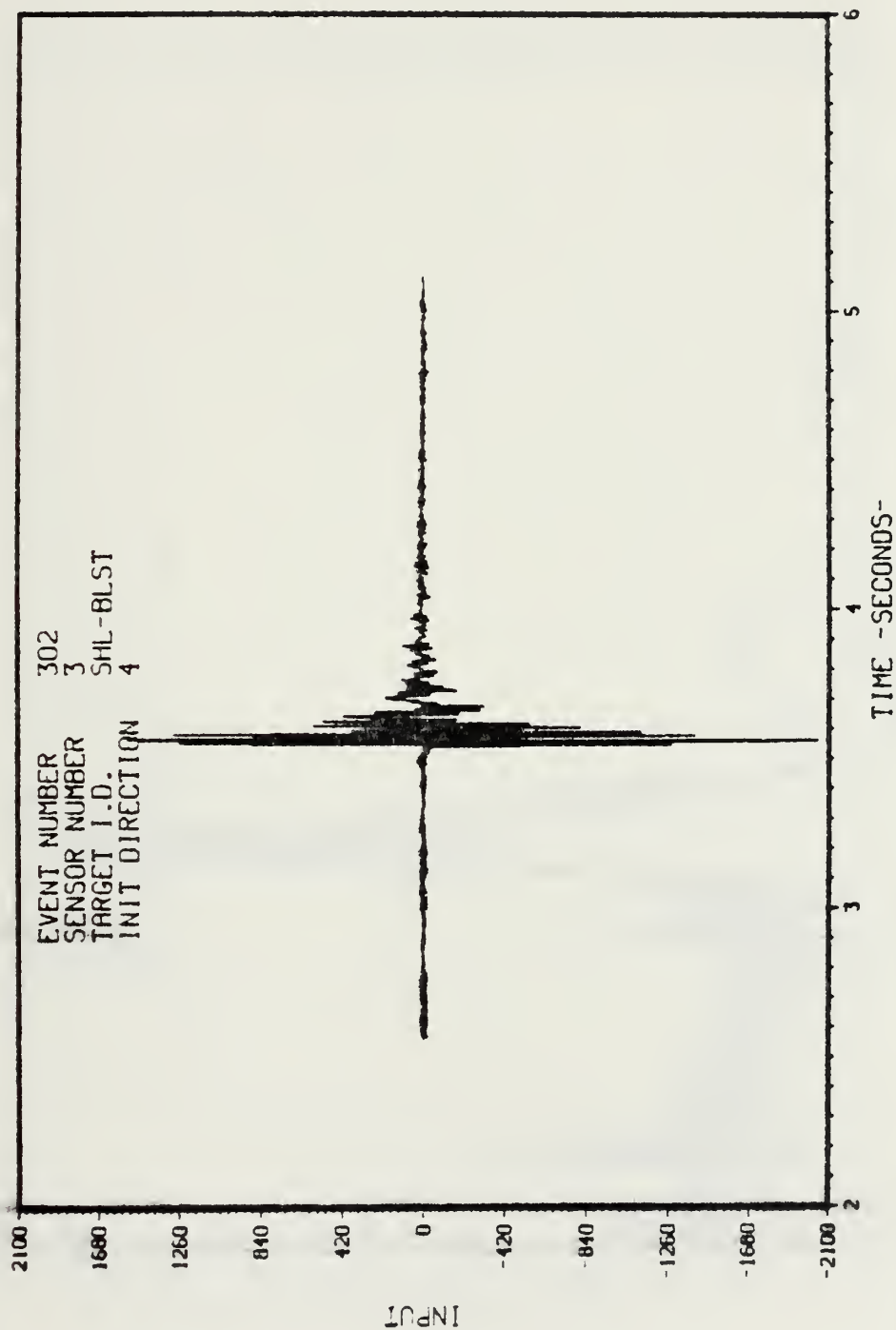


Figure 6.49 Amplitude Response for Event 302



# SENSOR POWER -VS- FREQUENCY

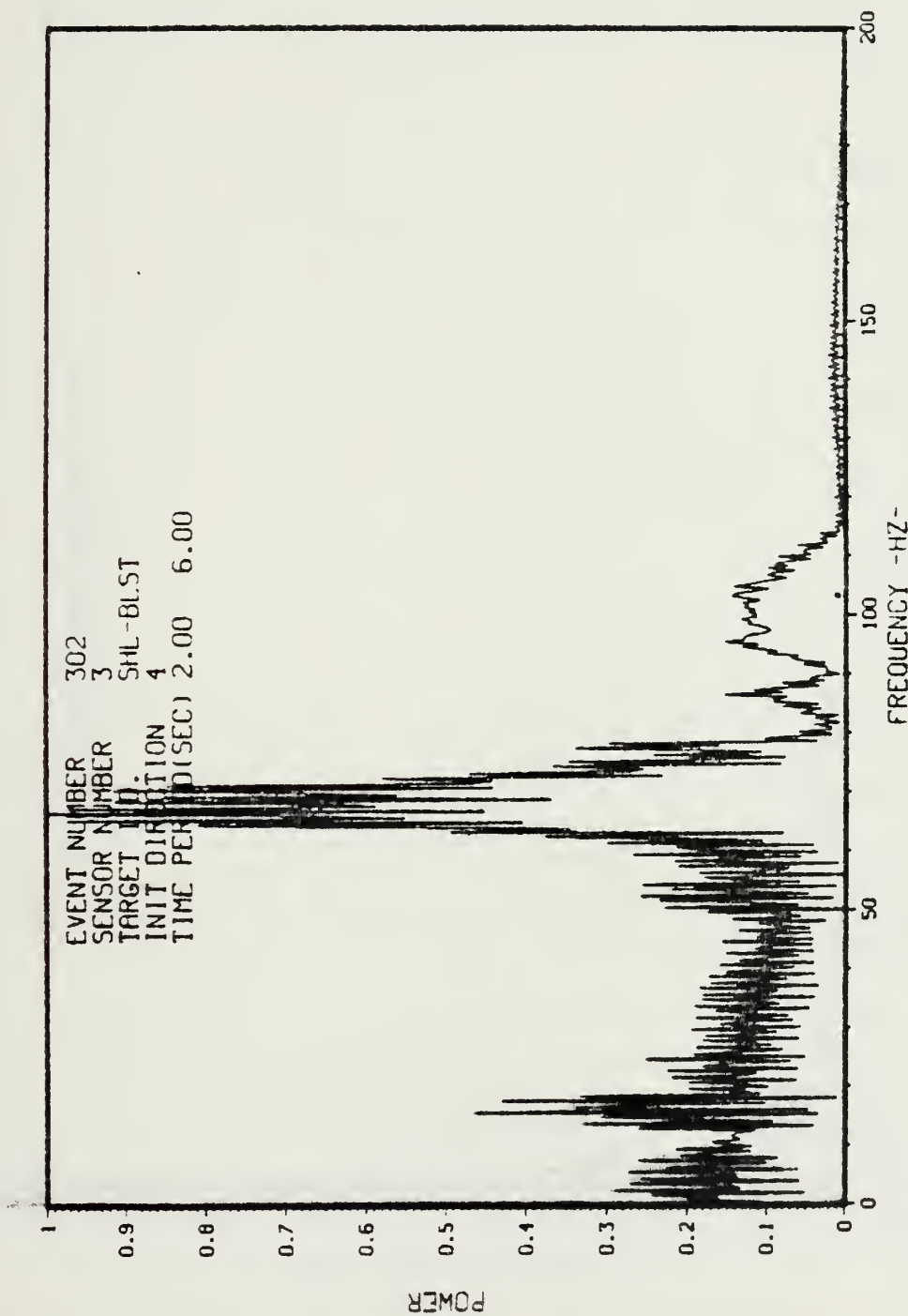


Figure 6.50 Frequency Response for Event 302



# LEAST MEAN SQUARES POLYNOMIAL

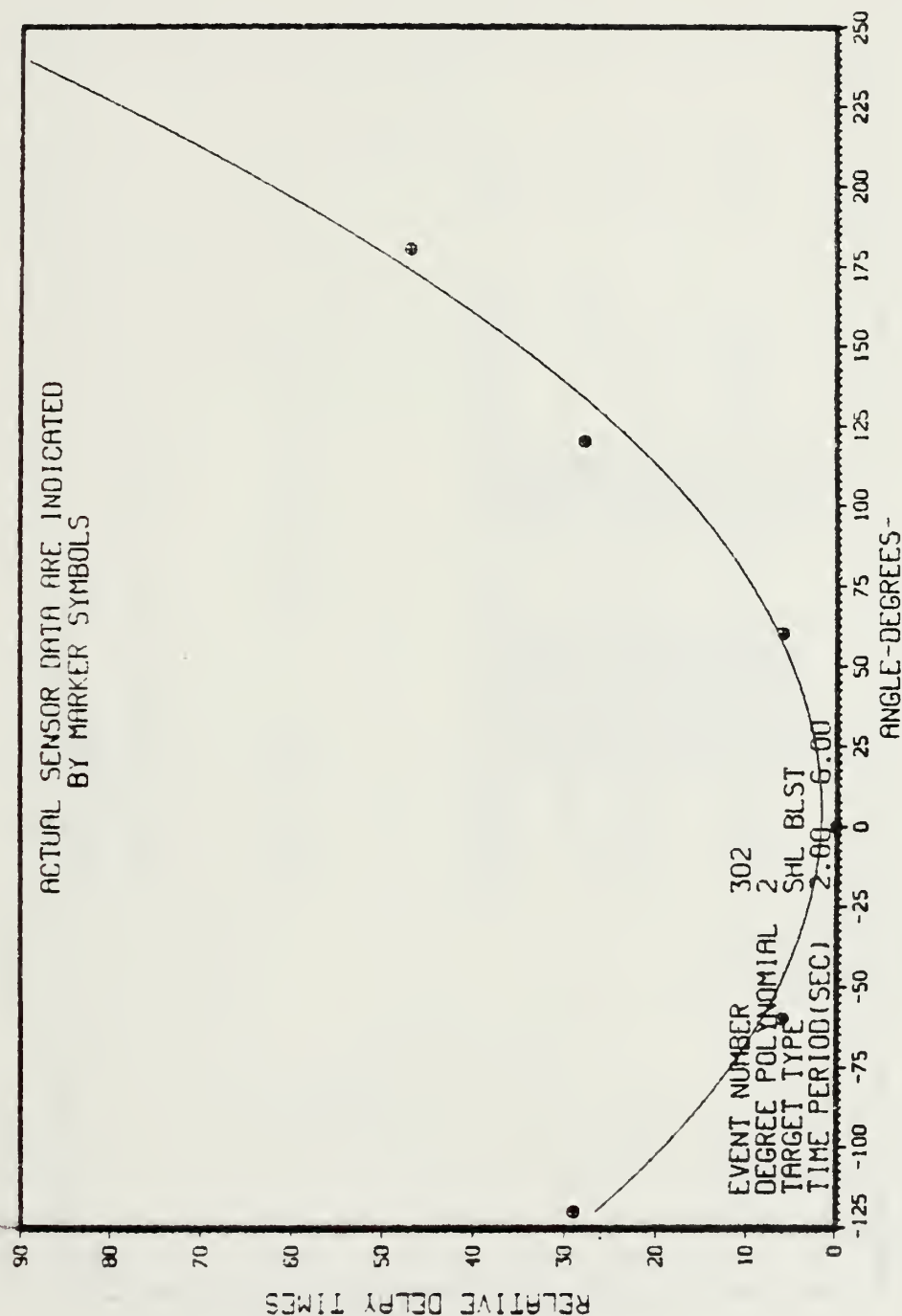


Figure 6.51 LMSP Matched Filter Direction for Event 302





# MULTIPLE TARGET - MATCHED FILTER OUTPUT

EVENT NUMBER 302

TIME PERIOD(SEC) 2.00 6.00

SHELL BLAST DIRECTION - 6.00

SIMULATED TRKD VEHICLE	TARGET FREQUENCY	0.00
AMPLITUDE	0.0000	
DIRECTION	0.0000	
SIMULATED WHLD VEHICLE	TARGET FREQUENCY	0.00
AMPLITUDE	0.0000	
DIRECTION	0.0000	
SIMULATED HELICOPTER	TARGET FREQUENCY	0.00
AMPLITUDE	0.0000	
DIRECTION	0.0000	
SIMULATED PERSONNEL	TARGET FREQUENCY	0.00
AMPLITUDE	0.0000	
DIRECTION	0.0000	

Figure 6.52 LMSP Multiple Target Direction Summary for Event 302



# LEAST MEAN SQUARES POLYNOMIAL

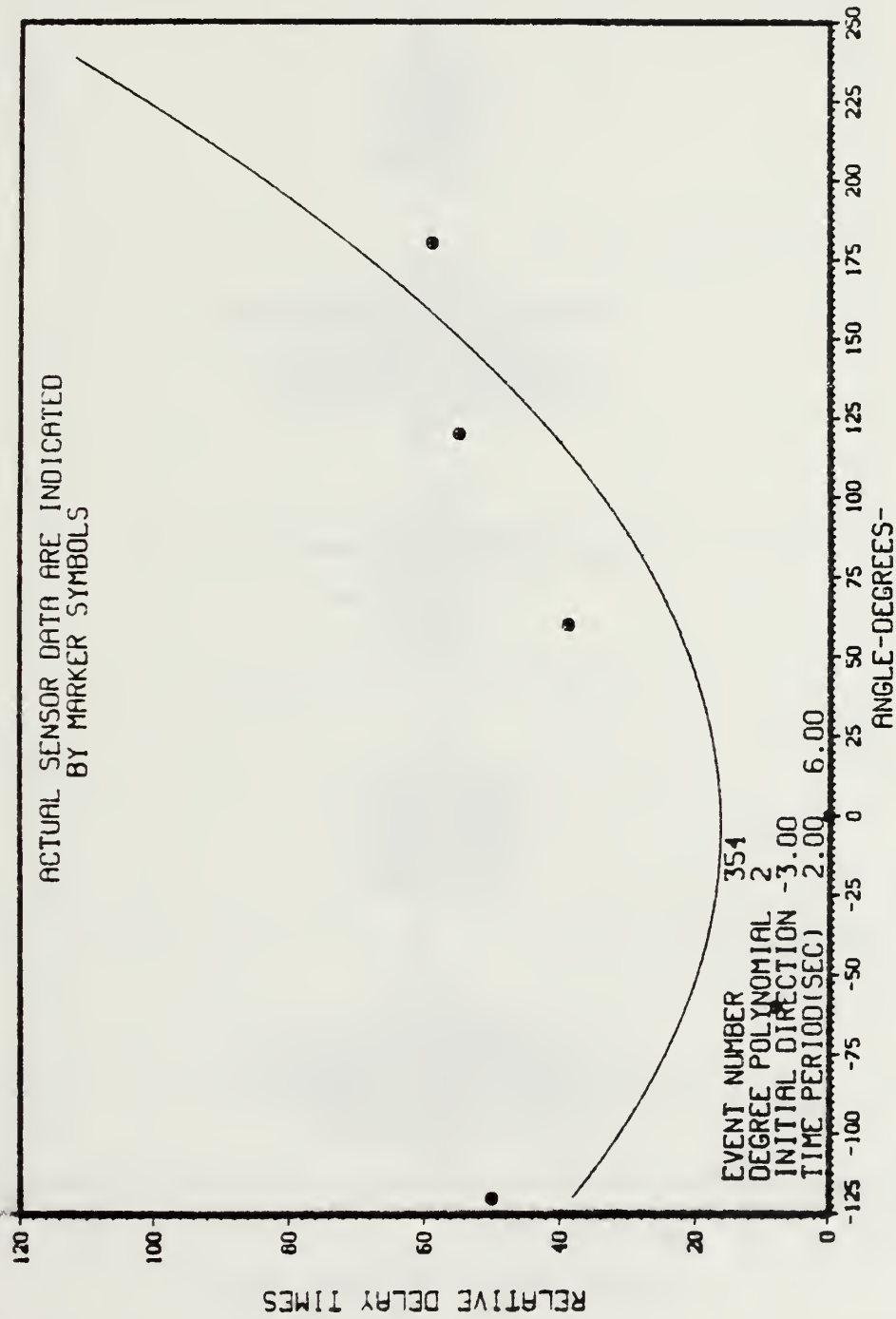


Figure 6.53 LMSP Initial Direction for Event 354 (2 - 6sec)



# MATCHED FILTER RESPONSE

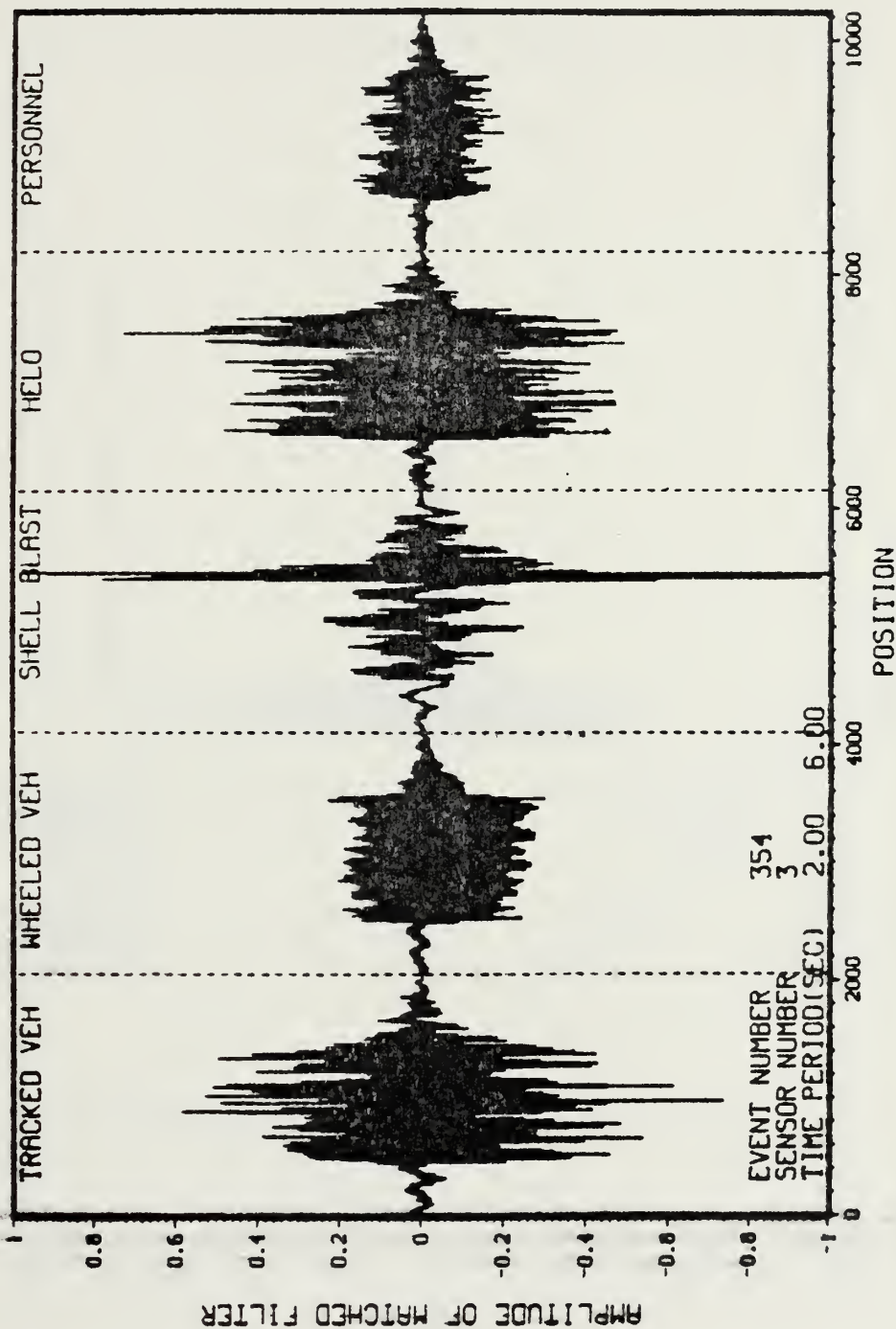


Figure 6.54 Matched Filter Response for Event 354 (2 - 6sec)



# SENSOR INPUT - VS - TIME

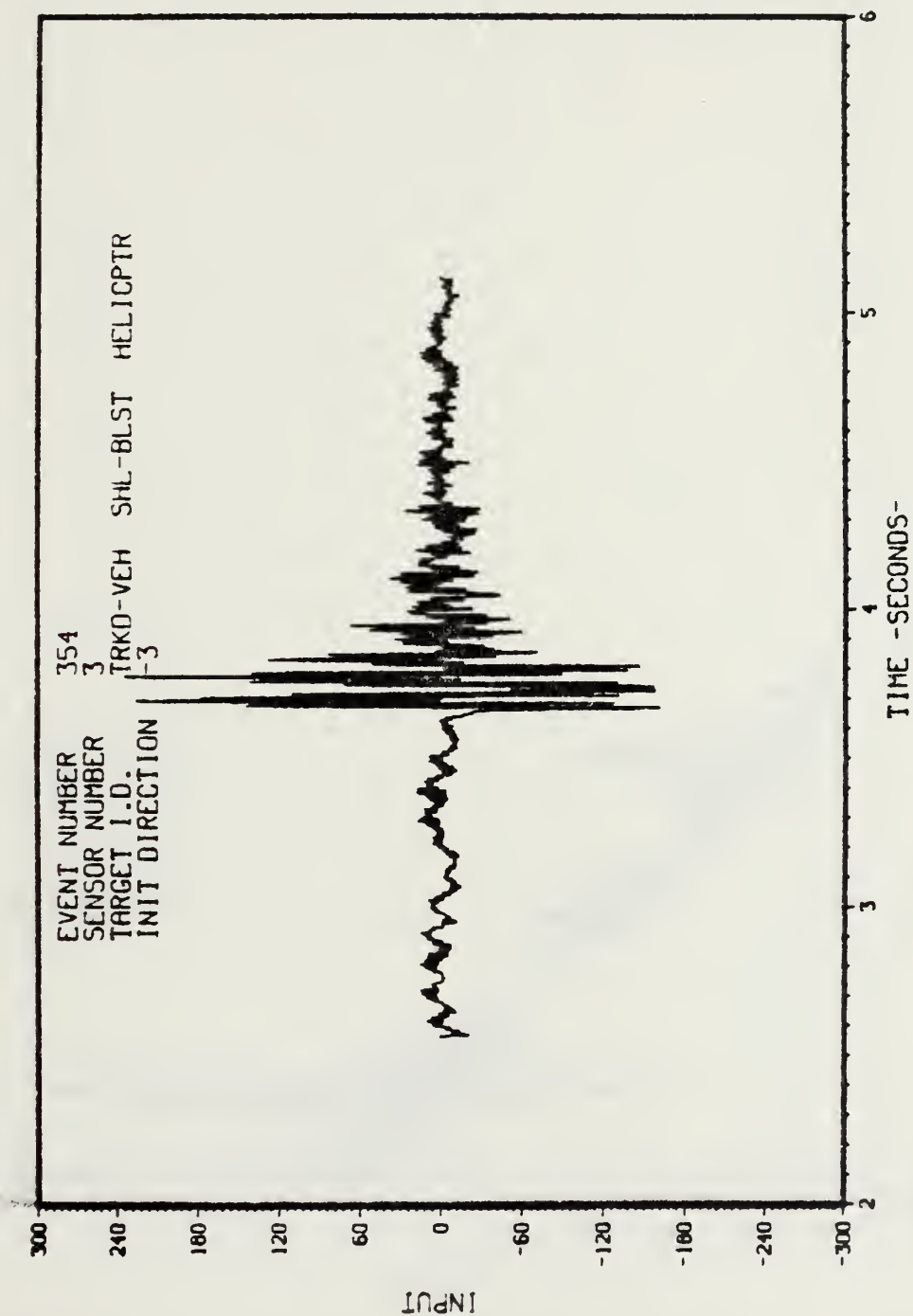


Figure 6.55 Amplitude Response for Event 354 (2 - 6sec)





# SENSOR POWER -VS- FREQUENCY

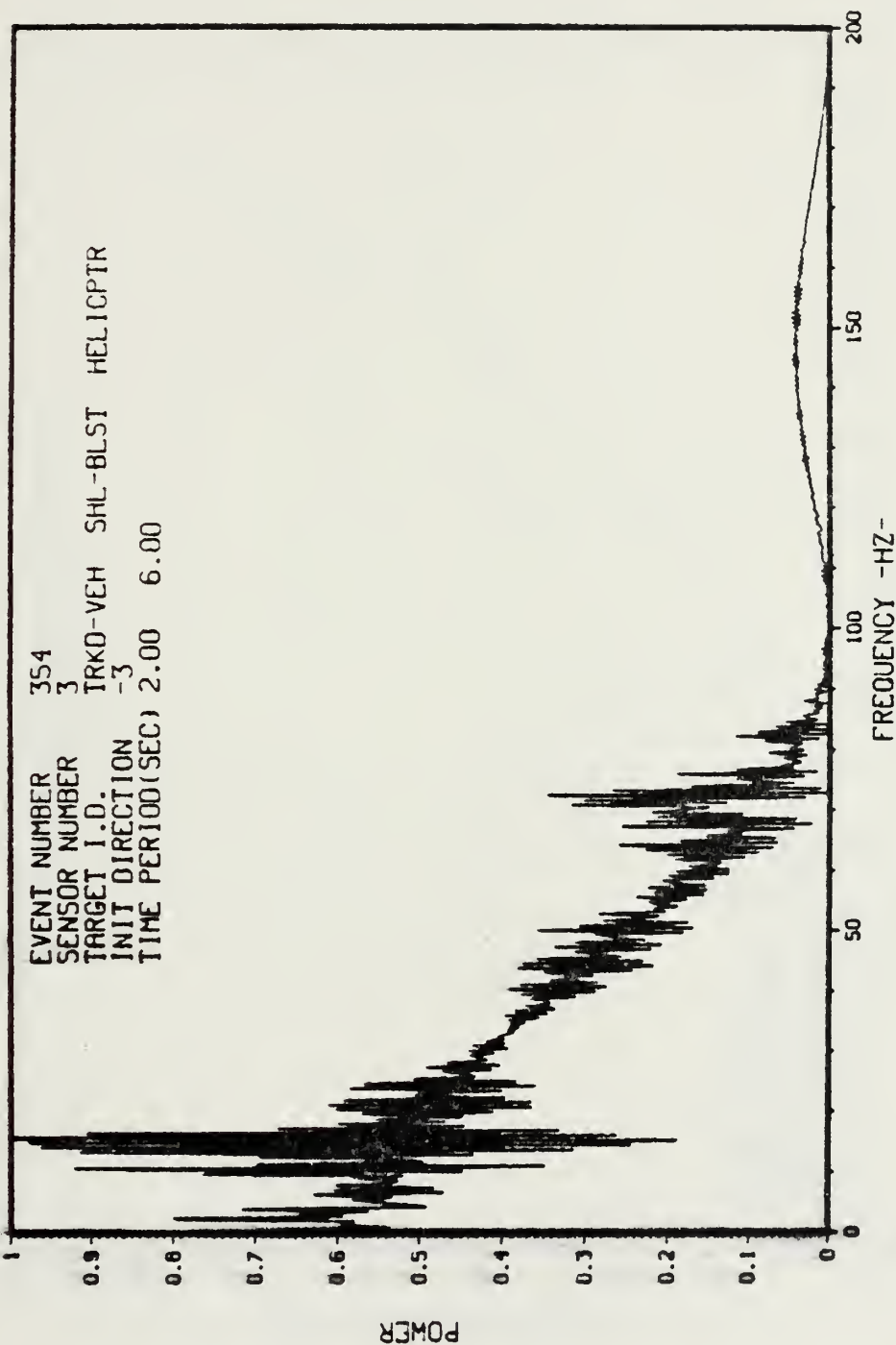


Figure 6.56 Frequency Response for Event 354 (2 - 6sec)



# LEAST MEAN SQUARES POLYNOMIAL

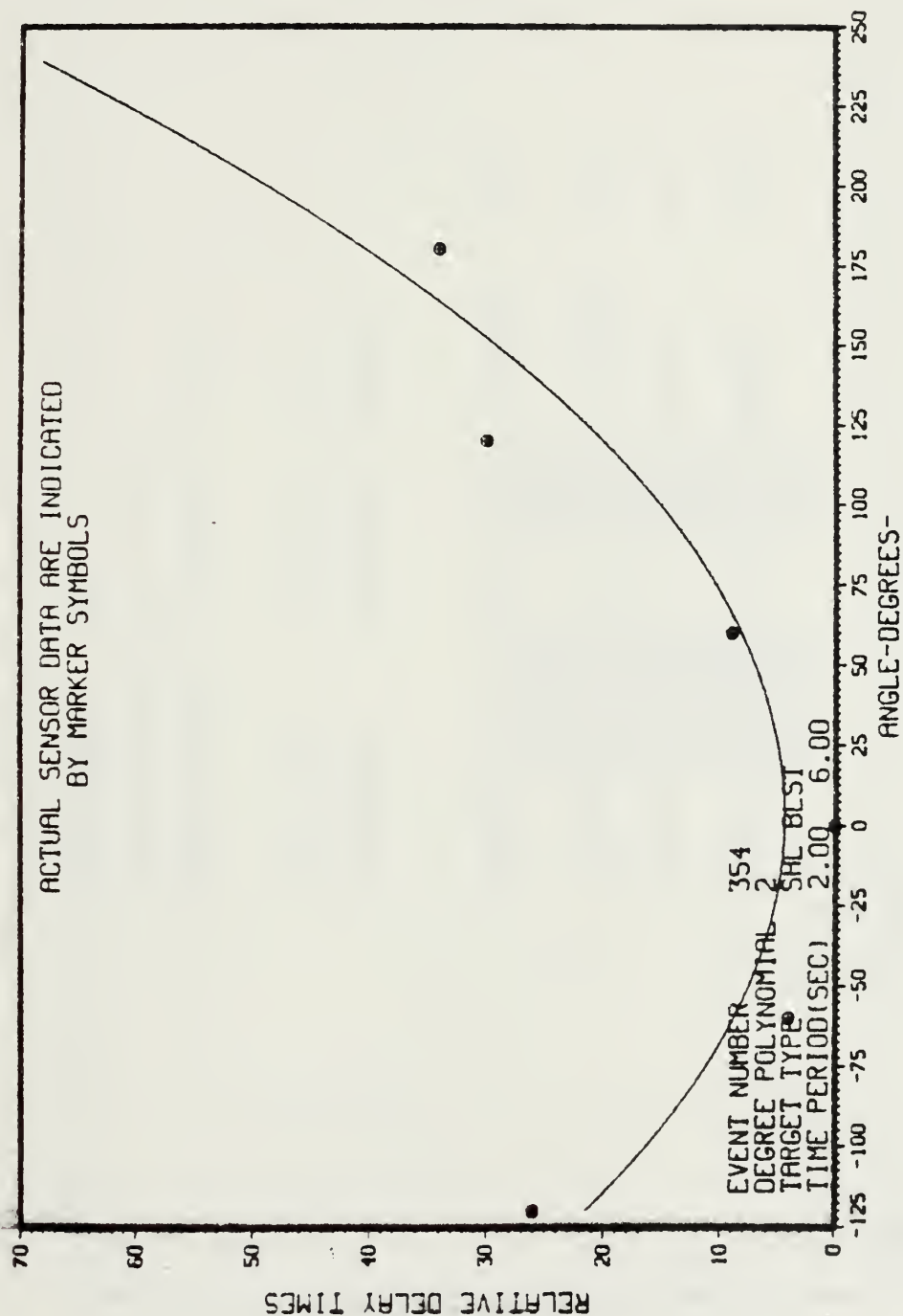


Figure 6.57 LMSP Matched Filter Direction for Event 354 (2 - 6sec)



# MULTIPLE TARGET - MATCHED FILTER OUTPUT

EVENT NUMBER	354	
TIME PERIOD(SEC)	2.00 6.00	
TRACKED VEHICLE	DIRECTION - 332.00	
SHELL BLAST	DIRECTION - 3.00	
HELICOPTER	DIRECTION - 355.00	
SIMULATED TRKD VEHICLE	TARGET FREQUENCY	0.00
AMPLITUDE	0.0000	
DIRECTION	0.0000	
SIMULATED WHLD VEHICLE	TARGET FREQUENCY	0.00
AMPLITUDE	0.0000	
DIRECTION	0.0000	
SIMULATED HELICOPTER	TARGET FREQUENCY	0.00
AMPLITUDE	0.0000	
DIRECTION	0.0000	
SIMULATED PERSONNEL	TARGET FREQUENCY	0.00
AMPLITUDE	0.0000	
DIRECTION	0.0000	

Figure 6.58 LMSP Multiple Target Direction Summary Event 354 (2 - 6sec)



# LEAST MEAN SQUARES POLYNOMIAL

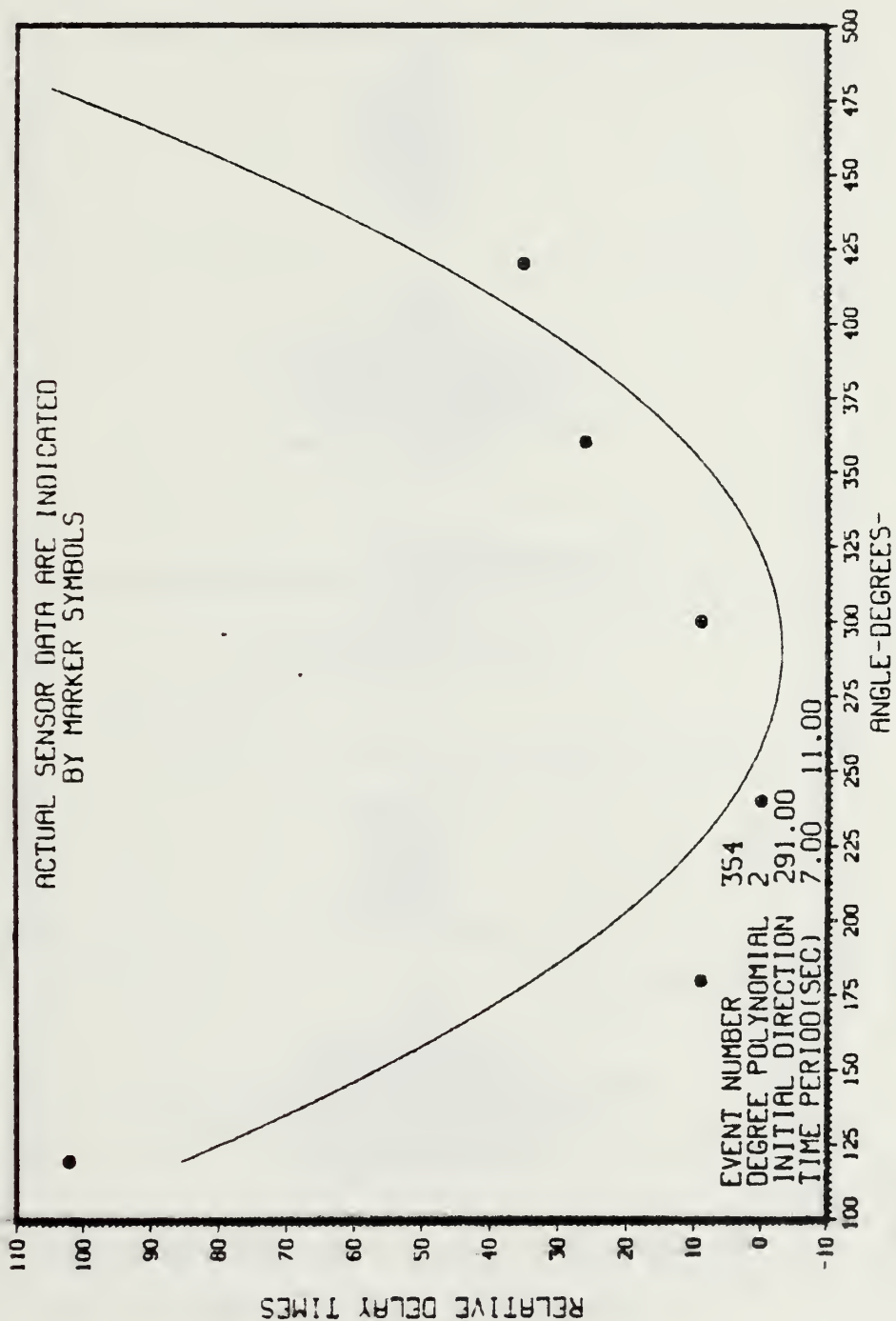


Figure 6.59 LMSP Initial Direction for Event 354 (7 - 11sec)





# MATCHED FILTER RESPONSE

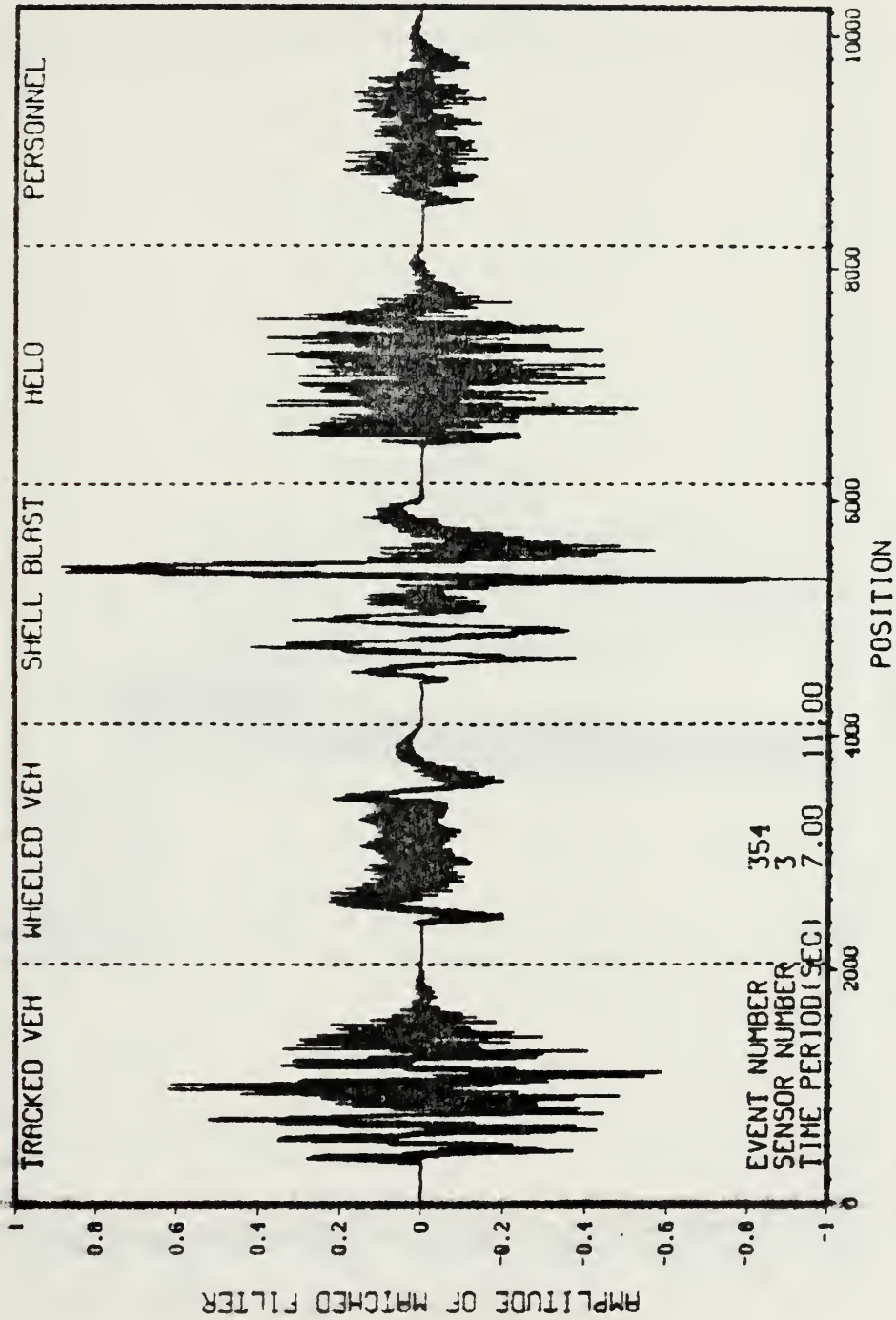


Figure 6.60 Matched Filter Response for Event 354 (7 - 11sec)



# SENSOR INPUT - VS - TIME

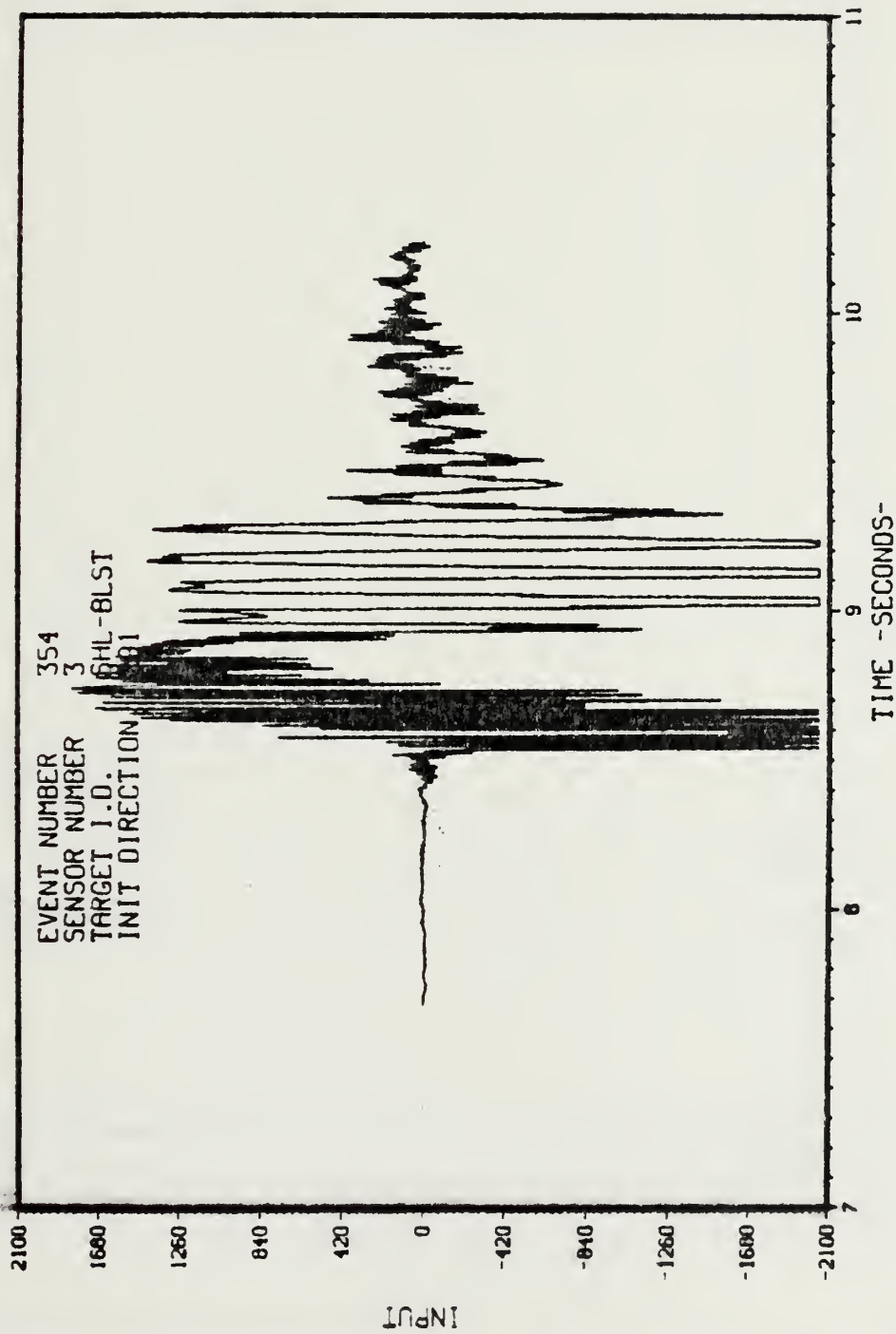


Figure 6.61 Amplitude Response for Event 354 (7 - 11sec)



# SENSOR POWER -VS- FREQUENCY

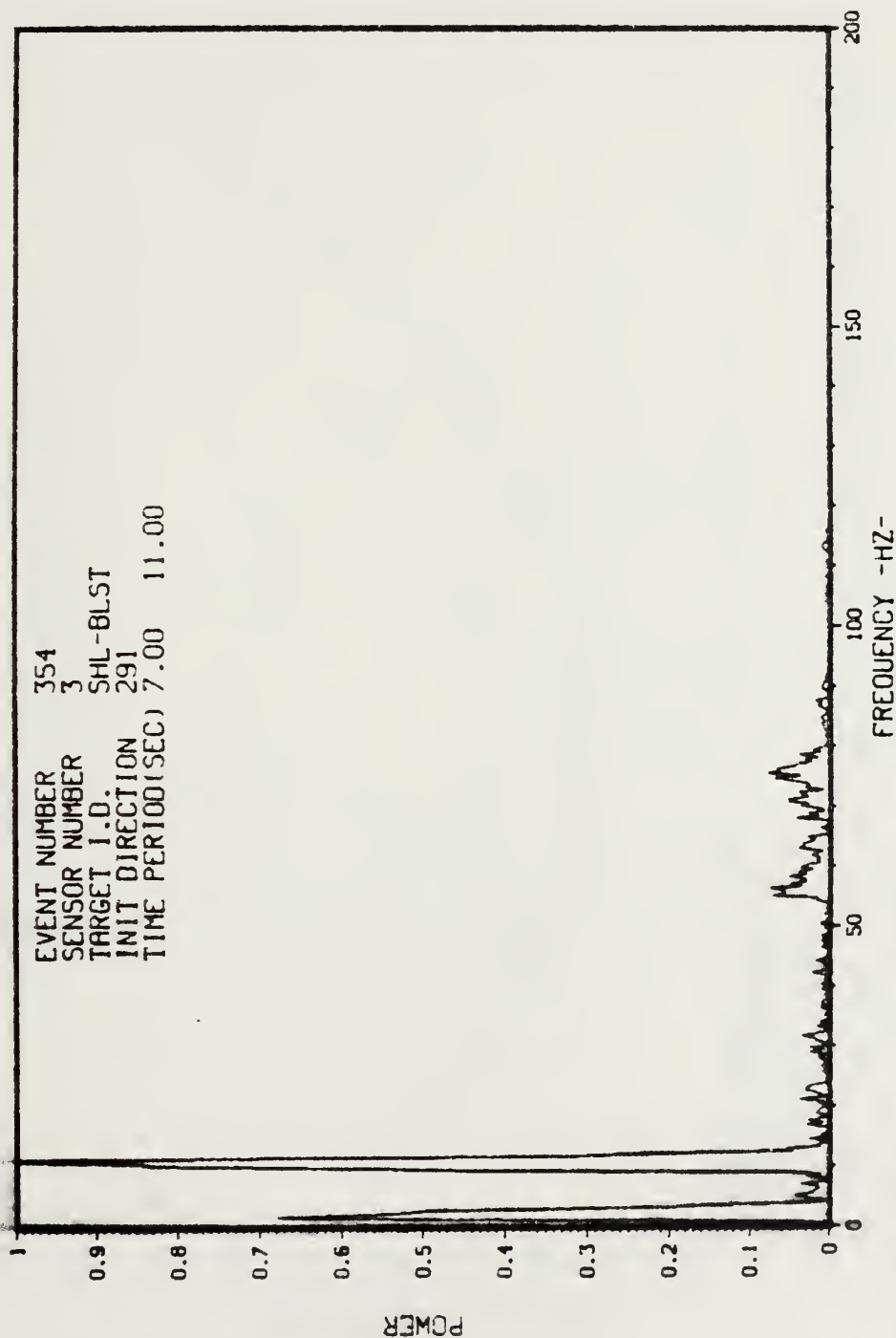


Figure 6.62 Frequency Response for Event 354 (7 - 11sec)



# LEAST MEAN SQUARES POLYNOMIAL

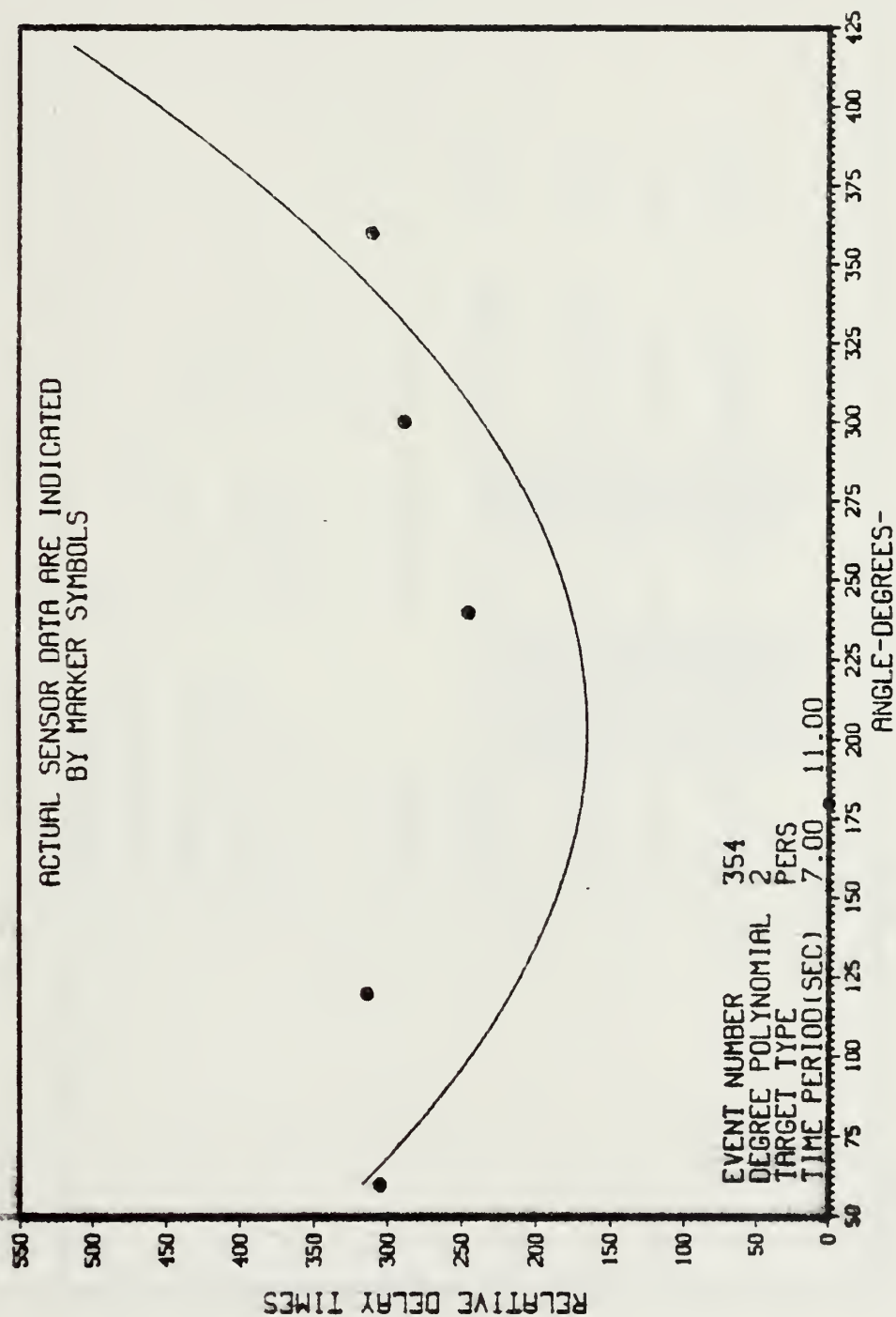


Figure 6.63 LMSP Matched Filter Direction for Event 354 (7 - 11sec)





# MULTIPLE TARGET - MATCHED FILTER OUTPUT

EVENT NUMBER	354
TIME PERIOD(SEC)	7.00 11.00
TRACKED VEHICLE	DIRECTION - 291.00
WHEELED VEHICLE	DIRECTION - 291.00
SHELL BLAST	DIRECTION - 291.00
PERSONNEL	DIRECTION - 204.00
SIMULATED TRKD VEHICLE	TARGET FREQUENCY 0.00
AMPLITUDE	0.0000
DIRECTION	0.0000
SIMULATED WHLD VEHICLE	TARGET FREQUENCY 0.00
AMPLITUDE	0.0000
DIRECTION	0.0000
SIMULATED HELICOPTER	TARGET FREQUENCY 0.00
AMPLITUDE	0.0000
DIRECTION	0.0000
SIMULATED PERSONNEL	TARGET FREQUENCY 0.00
AMPLITUDE	0.0000
DIRECTION	0.0000

Figure 6.64 LMSP Multiple Target Summary Event 354 (7 - 11sec)



## VII. CONCLUSIONS AND RECOMMENDATIONS

The ability of the digital matched filter to detect and correctly identify actual discrete single target types was excellent. The adaptive enhancement of the matched filter scheme was found to sharpen the matched filter responses. The complications of multiple targets and continuous targets proved to be less successful. Lack of high signal to noise ratio sample signals for use as filters reduced the ability of the filters to match the signals. As would be expected, the simulated target identification and direction finding operations met with success for both single and multiple targets.

The simulated data validated the usefulness of the least mean squares curve fitting method for target direction finding. This algorithm was noted to be useful in both the relative peak amplitude response method for recoil/blast targets and the matched filter peak position method for all targets. The highest accuracies were found using second degree polynomials. This was due to the reduced noise sensitivity of lower degree polynomials. Conversely, significant errors were found in the directions determined by the phase difference algorithm. These errors were possibly due to round-off error sensitivity in the software/hardware implementation. Experimental data could not be used to effectively crosscheck this finding since most of the experimental data targets were at zero degrees and the phase difference routine seemed to seek zero degrees.

A significant result was the accuracy of the blast/recoil target direction found using only the peak amplitude responses. Directions could be found using only the relative amplitude peak positions for the array sensors and the



least mean squares curve fitting routine. This result indicated a possible counter-fire application using a greatly simplified system. This finding is felt to be significant since artillery type targets are the highest priority target type. The discrete nature of the blast/recoil seismic signals would also allow for ready separation of even a large number of combined hostile and friendly signal sources. This would allow for observerless adjustment of fire onto hostile targets. Artillery and mortar targets may, in fact, be the only target types detectable at the ranges specified for a long range seismic system.

It is recommended that further study be made in to the possible implementation of the least mean square curve fitting of the peak sensor amplitudes responses in a counter-fire system. Digital matched filters for seismic target identification and direction finding may also prove effective after further experimentation with optimum sample signal filters for the various target types. Additionally, the matched filter response may possibly be enhanced by preprocessing the seismic signals through adaptive noise cancellors.

Acoustic vice seismic matched filtering with directional microphones may be useful in target identification. Once the target has been identified, a matched filter/least mean squares based direction finding scheme could then be attempted.





## APPENDIX A

### USERS MANUAL

The software developed provided for interactive program operation. However, further information must be provided for an initial system setup and correct program operation. To begin with, the seismic data must be transferred from magnetic tape to the IBM 3033's Mass Storage System (MSS). The data must then be transferred to the DISSPLA user's disk for analysis of the program. These data transfers may be accomplished using Job Control Language (JCL) procedures.

The magnetic tape volume must first be scanned to determine the storage format of its files. The JCL procedure TSCAN provides this information. A sample TSCAN job follows:

```
//JLJV1677 JOB (3026,0304),'SMC-1677 JOHNSTON',CLASS=F
// EXEC TSCAN,VOLIN=PARK1,DCBIN='DEN=2',UNITIN='3400-4'
// EXEC TSCAN,VOLIN=PARK2,DCBIN='DEN=2',UNITIN='3400-4'
// EXEC TSCAN,VOLIN=PARK3,DCBIN='DEN=2',UNITIN='3400-4'
// EXEC TSCAN,VOLIN=PARK4,DCBIN='DEN=2',UNITIN='3400-4'
//
```

Once the tape scan is completed, the tape files and comments can be transferred to the MSS. Prior to this transfer however, space in the MSS must be made for these files. The procedure IEFBR14 is used for this purpose. A sample job follows:

```
//JLJTM74A JOB (3026,0304),'SMC1677 JOHNSTON',CLASS=A
//*MAIN ORG=NPGVM1.0131P
// EXEC PGM=IEFBR14
//DD1 DD UNIT=3330V,MSVGP=PUB4B,DISP=(NEW,CATLG),
// SPACE=(CYL,(4,4,3)),DSN=MSS.S3026.P302
```





```

/*
// EXEC PGM=IEFBR14
//DD1 DD UNIT=3330V,MSVGP=PUB4B,DISP=(NEW,CATLG),
//      SPACE=(CYL,(4,4,3)),DSN=MSS.S3026.P314
/*
// EXEC PGM=IEFBR14
//DD1 DD UNIT=3330V,MSVGP=PUB4B,DISP=(NEW,CATLG),
//      SPACE=(CYL,(4,4,3)),DSN=MSS.S3026.P319
/*
//

```

Each event is proceeded by a comment file for that event. These comment files can be identified from the TSCAN output as a file containing only one record. The files containing nine or eighteen records are the sensor data files for the events. Files of nine records in length are events using a circular array of nine sensors designated as a type A33 array. These sensors are all vertical motion-sensing geophones. The eighteen record files contain six sensor groups of three geophones. A circular array is designated type A31 and a linear array is a type A32 array. The three geophones for each group sense either radial, transverse or vertical motion. A JCL routine, using the procedure IEBGENER, transfers the event comment and sensor data. A sample IEBGENER job follows:

```

//JLJ11677 JOB (3026,0304),'JOHNSTON SMC1677',CLASS=F
//*MAIN ORG=NPGVM1.0131P
//*
//* CP/CMS SUBMIT      IEBGENER JCL
//*
//*      COPY TAPE FILES TO MSS.S3026.P319
//*
// EXEC PGM=IEBGENER
//SYSPRINT DD SYSOUT=A
//SYSUT1 DD UNIT=3400-4,VOL=SER=PARK2,DISP=(,PASS),

```



```

//          LABEL=(1,NL,,IN),
//      DCB=(RECFM=FB,LRECL=64,BLKSIZE=2048,DEN=2,OPTCD=Q)
//SYSUT2 DD  DISP=SHR,DSN=MSS.S3026.COMMENTS(COM319)
//SYSIN DD DUMMY
//* * * * *
//COPY  PROC FILE=,MEM=
//      EXEC PGM=IEBGENER
//SYSPRINT DD SYSOUT=A
//SYSUT1 DD UNIT=3400-4,VOL=SER=PARK2,DISP=(,PASS),
//          LABEL=(&FILE,NL,,IN),DCB=(RECFM=F,BLKSIZE=2048,DEN=2)
//SYSUT2 DD  DISP=SHR,DSN=MSS.S3026.P319(&MEM)
//SYSIN DD DUMMY
//      PEND
/*
//* * * * *
//      EXEC COPY,FILE=342,MEM=SEN1
//      EXEC COPY,FILE=343,MEM=SEN2
//      EXEC COPY,FILE=344,MEM=SEN3
//      EXEC COPY,FILE=345,MEM=SEN4
//      EXEC COPY,FILE=346,MEM=SEN5
//      EXEC COPY,FILE=347,MEM=SEN6
//      EXEC COPY,FILE=348,MEM=SEN7
//      EXEC COPY,FILE=349,MEM=SEN8
//      EXEC COPY,FILE=350,MEM=SEN9
//      EXEC COPY,FILE=351,MEM=SEN10
//      EXEC COPY,FILE=352,MEM=SEN11
//      EXEC COPY,FILE=353,MEM=SEN12
//      EXEC COPY,FILE=354,MEM=SEN13
//      EXEC COPY,FILE=355,MEM=SEN14
//      EXEC COPY,FILE=356,MEM=SEN15
//      EXEC COPY,FILE=357,MEM=SEN16
//      EXEC COPY,FILE=358,MEM=SEN17
//      EXEC COPY,FILE=359,MEM=SEN18
//      EXEC COPY,FILE=360,MEM=SEN19
/*

```



//

Transfer of the desired event data from MSS to the DISSPLA user's disk may now be performed. A batch fortran job with the appropriate FILEDEFS to denote the various geophone's data is submitted. The RSCS/NET feature is used to send the output of this routine to the user's reader. A sample fortran job for nine sensors follows:

```
//JLJ83026 JOB (3026,0304),'JOHNSTON',CLASS=A
```

```
//*MAIN ORG=NPGVM1.0090P
```

```
// EXEC FORTXCG,REGION.GO=1024K
```

```
//FORT.SYSIN DD *
```

C

```
LOGICAL*1 INFO1(8),INFO2(8),INFO3(8),INFO4(8),INFO5(8)
LOGICAL*1 INFO6(8),INFO7(8),INFO8(8),INFO9(8)
INTEGER*2 DATA1(1020),DATA2(1020),DATA3(1020),DATA4(1020)
INTEGER*2 DATA5(1020),DATA6(1020),DATA7(1020),DATA8(1020)
INTEGER*2 DATA9(1020),DATB1(4096)
```

C

```
DO 30 J=1,4
```

```
READ(1,100) INFO1,DATA1
READ(2,100) INFO2,DATA2
READ(3,100) INFO3,DATA3
READ(4,100) INFO4,DATA4
READ(8,100) INFO5,DATA5
READ(9,100) INFO6,DATA6
READ(10,100) INFO7,DATA7
READ(11,100) INFO8,DATA8
READ(12,100) INFO9,DATA9
```

```
100 FORMAT(8A1,102(10A2))
```

```
DO 10 I = 10,1020,10
```

```
WRITE(6,101) DATA1(I-9),DATA1(I-8),DATA1(I-7),
1DATA1(I-6),DATA1(I-5),DATA1(I-4),DATA1(I-3),
2DATA1(I-2),DATA1(I-1),DATA1(I)
```



```

10  CONTINUE
    DO 20 I = 10,1020,10
        WRITE(6,101) DATA2(I - 9),DATA2(I - 8),DATA2(I - 7),
1DATA2(I - 6),DATA2(I - 5),DATA2(I - 4),DATA2(I - 3),
2DATA2(I - 2),DATA2(I - 1),DATA2(I)
20  CONTINUE
    DO 40 I = 10,1020,10
        WRITE(6,101) DATA3(I - 9),DATA3(I - 8),DATA3(I - 7),
1DATA3(I - 6),DATA3(I - 5),DATA3(I - 4),DATA3(I - 3),
2DATA3(I - 2),DATA3(I - 1),DATA3(I)
40  CONTINUE
    DO 50 I = 10,1020,10
        WRITE(6,101) DATA4(I - 9),DATA4(I - 8),DATA4(I - 7),
1DATA4(I - 6),DATA4(I - 5),DATA4(I - 4),DATA4(I - 3),
2DATA4(I - 2),DATA4(I - 1),DATA4(I)
50  CONTINUE
    DO 60 I = 10,1020,10
        WRITE(6,101) DATA5(I - 9),DATA5(I - 8),DATA5(I - 7),
1DATA5(I - 6),DATA5(I - 5),DATA5(I - 4),DATA5(I - 3),
2DATA5(I - 2),DATA5(I - 1),DATA5(I)
60  CONTINUE
    DO 70 I = 10,1020,10
        WRITE(6,101) DATA6(I - 9),DATA5(I - 8),DATA6(I - 7),
1DATA6(I - 6),DATA6(I - 5),DATA6(I - 4),DATA6(I - 3),
2DATA6(I - 2),DATA6(I - 1),DATA6(I)
70  CONTINUE
    DO 80 I = 10,1020,10
        WRITE(6,101) DATA7(I - 9),DATA7(I - 8),DATA7(I - 7),
1DATA7(I - 6),DATA7(I - 5),DATA7(I - 4),DATA7(I - 3),
2DATA7(I - 2),DATA7(I - 1),DATA7(I)
80  CONTINUE
    DO 90 I = 10,1020,10
        WRITE(6,101) DATA8(I - 9),DATA8(I - 8),DATA8(I - 7),
1DATA8(I - 6),DATA8(I - 5),DATA8(I - 4),DATA8(I - 3),
2DATA8(I - 2),DATA8(I - 1),DATA8(I)

```





```

90      CONTINUE
      DO 91 I = 10,1020,10
      WRITE (6,101) DATA9(I - 9),DATA9(I - 8),DATA9(I - 7),
1DATA9(I - 6),DATA9(I - 5),DATA9(I - 4),DATA9(I - 3),
2DATA9(I - 2),DATA9(I - 1),DATA9(I)
91      CONTINUE
101     FORMAT(I6,I6,I6,I6,I6,I6,I6,I6,I6,I6)
30      CONTINUE
      STOP
      END

```

```

/*
//GO.FT01F001 DD DISP=SHR,DSN=MSS.S3026.P383(SEN1)
//GO.FT02F001 DD DISP=SHR,DSN=MSS.S3026.P383(SEN2)
//GO.FT03F001 DD DISP=SHR,DSN=MSS.S3026.P383(SEN3)
//GO.FT04F001 DD DISP=SHR,DSN=MSS.S3026.P383(SEN4)
//GO.FT08F001 DD DISP=SHR,DSN=MSS.S3026.P383(SEN5)
//GO.FT09F001 DD DISP=SHR,DSN=MSS.S3026.P383(SEN6)
//GO.FT10F001 DD DISP=SHR,DSN=MSS.S3026.P383(SEN7)
//GO.FT11F001 DD DISP=SHR,DSN=MSS.S3026.P383(SEN8)
//GO.FT12F001 DD DISP=SHR,DSN=MSS.S3026.P383(SEN9)
//GO.SYSIN DD *
/*
//

```

A sample job for a six sensor group array follows:

```

//JLJ83026 JOB (3026,0304),'JOHNSTON',CLASS=A
//*MAIN ORG=NPGVM1.0090P
// EXEC PORTXCG,REGION.GO=1024K
//PORT.SYSIN DD *

```

C

```

LOGICAL*1 INFO1(8),INFO2(8),INFO3(8),INFO4(8),INFO5(8)
LOGICAL*1 INFO6(8),INFO7(8),INFO8(8),INFO9(8)
INTEGER*2 DATA1(1020),DATA2(1020),DATA3(1020),DATA4(1020)
INTEGER*2 DATA5(1020),DATA6(1020),DATA7(1020),DATA8(1020)
INTEGER*2 DATA9(1020),DATB1(4096)

```



C

```
DO 30 J=1,4

    READ(1,100) INFO1,DATA1
    READ(2,100) INFO2,DATA2
    READ(3,100) INFO3,DATA3
    READ(4,100) INFO4,DATA4
    READ(8,100) INFO5,DATA5
    READ(9,100) INFO6,DATA6
100  FORMAT(8A1,102(10A2))
    DO 10 I = 10,1020,10
        WRITE(6,101) DATA1(I - 9),DATA1(I - 8),DATA1(I - 7),
1DATA1(I - 6),DATA1(I - 5),DATA1(I - 4),DATA1(I - 3),
2DATA1(I - 2),DATA1(I - 1),DATA1(I)
10  CONTINUE
    DO 20 I = 10,1020,10
        WRITE(6,101) DATA2(I - 9),DATA2(I - 8),DATA2(I - 7),
1DATA2(I - 6),DATA2(I - 5),DATA2(I - 4),DATA2(I - 3),
2DATA2(I - 2),DATA2(I - 1),DATA2(I)
20  CONTINUE
    DO 40 I = 10,1020,10
        WRITE(6,101) DATA3(I - 9),DATA3(I - 8),DATA3(I - 7),
1DATA3(I - 6),DATA3(I - 5),DATA3(I - 4),DATA3(I - 3),
2DATA3(I - 2),DATA3(I - 1),DATA3(I)
40  CONTINUE
    DO 50 I = 10,1020,10
        WRITE(6,101) DATA4(I - 9),DATA4(I - 8),DATA4(I - 7),
1DATA4(I - 6),DATA4(I - 5),DATA4(I - 4),DATA4(I - 3),
2DATA4(I - 2),DATA4(I - 1),DATA4(I)
50  CONTINUE
    DO 60 I = 10,1020,10
        WRITE(6,101) DATA5(I - 9),DATA5(I - 8),DATA5(I - 7),
1DATA5(I - 6),DATA5(I - 5),DATA5(I - 4),DATA5(I - 3),
2DATA5(I - 2),DATA5(I - 1),DATA5(I)
60  CONTINUE
```



```

DO 70 I = 10,1020,10
WRITE(6,101) DATA6(I - 9),DATA6(I - 8),DATA6(I - 7),
1DATA6(I - 6),DATA6(I - 5),DATA6(I - 4),DATA6(I - 3),
2DATA6(I - 2),DATA6(I - 1),DATA6(I)
70    CONTINUE
101    FORMAT(I6,I6,I6,I6,I6,I6,I6,I6,I6,I6)
30    CONTINUE
      STOP
      END

/*
//GO.FT01F001 DD DISP=SHR,DSN=MSS.S3026.P350(SEN3)
//GO.FT02F001 DD DISP=SHR,DSN=MSS.S3026.P350(SEN6)
//GO.FT03F001 DD DISP=SHR,DSN=MSS.S3026.P350(SEN9)
//GO.FT04F001 DD DISP=SHR,DSN=MSS.S3026.P350(SEN12)
//GO.FT08F001 DD DISP=SHR,DSN=MSS.S3026.P350(SEN15)
//GO.FT09F001 DD DISP=SHR,DSN=MSS.S3026.P350(SEN18)
//GO.SYSIN DD *
/*
//

```

Two files will be returned to user's reader. The first file is the listing and diagnostics file and should be purged. The second file should be named SEN DATA. SEN DATA must now be edited. Delete the first seven lines of the file and issue the command LREC 80 to set the proper file record length.

The interactive program can be run with the complete collection of files listed in the exec MATCH. The MATCH EXEC follows:

```

&TRACE OFF
FORTGI MFILTER
GLOBAL TXTLIB PORTMOD2 MOD2EEH IMSLSP NONIMSL
FILEDEF 10 TERMINAL
FILEDEF 05 DISK SEN DATA (PERM)
FILEDEF 07 DISK COM DATA (PERM)

```



```
FI 4 DISK FILTER DATA (RECFM VS PERM
FILEDEF 18 DISK DISSPLA METAFILE T4 (RECFM VBS LRECL
                                19065 BLOCK 19069
EXEC DISSPLA MFILTER
```

Entry parameters, such as the number of sensors in the array and the sampling rate, can be found in the NOSC data log for the event under study. All other interactive entries are user selected options or are self explanatory.

[Ref. 12]





APPENDIX B  
SAMPLE INTERACTIVE PROGRAM SESSION

match

G1 COMPILER ENTERED

SOURCE ANALYZED

PROGRAM NAME = MAIN

\* NO DIAGNOSTICS GENERATED

SOURCE ANALYZED

PROGRAM NAME = ANGLE

\* NO DIAGNOSTICS GENERATED

SOURCE ANALYZED

PROGRAM NAME = TIMEOUT

\* NO DIAGNOSTICS GENERATED

SOURCE ANALYZED

PROGRAM NAME = FREQOT

\* NO DIAGNOSTICS GENERATED

SOURCE ANALYZED

PROGRAM NAME = MATCH

\* NO DIAGNOSTICS GENERATED

SOURCE ANALYZED

PROGRAM NAME = MYDATA

\* NO DIAGNOSTICS GENERATED

SOURCE ANALYZED

PROGRAM NAME = MAXMIN

\* NO DIAGNOSTICS GENERATED

SOURCE ANALYZED

PROGRAM NAME = SPCTRM

\* NO DIAGNOSTICS GENERATED

SOURCE ANALYZED

PROGRAM NAME = MULTI

\* NO DIAGNOSTICS GENERATED

SOURCE ANALYZED



PROGRAM NAME = MLTPLT  
\* NO DIAGNOSTICS GENERATED  
SOURCE ANALYZED  
PROGRAM NAME = RMS  
\* NO DIAGNOSTICS GENERATED  
SOURCE ANALYZED  
PROGRAM NAME = AVG  
\* NO DIAGNOSTICS GENERATED  
SOURCE ANALYZED  
PROGRAM NAME = SIMULT  
\* NO DIAGNOSTICS GENERATED  
SOURCE ANALYZED  
PROGRAM NAME = LMS  
\* NO DIAGNOSTICS GENERATED  
SOURCE ANALYZED  
PROGRAM NAME = PLT  
\* NO DIAGNOSTICS GENERATED  
SOURCE ANALYZED  
PROGRAM NAME = SOLV  
\* NO DIAGNOSTICS GENERATED  
    \*STATISTICS\* NO DIAGNOSTICS THIS STEP  
DISK 'T' NOT ACCESSED.  
B (126) R/O  
C (127) R/O  
E (128) R/O

... Your Fortran program is now being loaded ...  
... execution will soon follow ...

EXECUTION BEGINS...

ENTER EVENT RECORDING NUMBER-I3-  
383

EVENT NUMBER 383

383. A33. 10 SEPT81 5KM EOD SHOT. SET B. NO DELAY. C141 ON FINAL



AT END OF TAPE."

ENTER SAMPLE RATE IN HERTZ-REAL-  
120.

ENTER LOW LOOK ANGLE IN DEGREES-I3-  
-100

ENTER HIGH LOOK ANGLE IN DEGREES-I3-  
200

ENTER MATCH FILTER THRESHOLD. RANGE OF 0. TO 1.0  
.9

ENTER PLOT SCALING FACTOR-REAL-  
.85

ENTER NUMBER OF SENSORS IN RING 6 OR 9 ONLY-I1-  
9

ENTER SENSOR NUMBER FOR DISPLAY-I1-  
4

ENTER NOISE THRESHOLD LEVEL -REAL-  
1000.

ENTER DATA WINDOW SIZE FOR DIRECTION FINDING-I4-  
0400

FOR COMPRS OUTPUT ENTER -1-. FOR TEK618 ENTER -2-  
1

TO CREATE SIMULATED TARGETS ENTER -1- ELSE -2-  
1

ENTER THE FOUR SIMULATION FREQUENCIES-REAL-

ENTER FREQUENCY  
0

ENTER FREQUENCY  
0



ENTER FREQUENCY

0

ENTER FREQUENCY

120.

ENTER AMPLITUDES FOR EACH FREQUENCY-REAL-

ENTER AMPLITUDE

0

ENTER AMPLITUDE

0

ENTER AMPLITUDE

0

ENTER AMPLITUDE

4000.

ENTER TARGET ANGLE FOR EACH FREQUENCY-I3-

SIX SENSORS ALLOWABLE ANGLES; 0, 60, 120, 180, 240, 300

FOR NINE SENSORS; 0, 40, 80, 120, 160, 200, 240, 280, 320

ENTER ANGLE

0

ENTER ANGLE

0

ENTER ANGLE

0

ENTER ANGLE

120

TO MODIFY AMPLITUDE OF SIGNAL ABOVE NOISE THRESHOLD

ENTER - 1 -, ELSE ENTER - 2 -





2

ENTER DEGREE OF POLYNOMIAL DESIRED -I1-

FOR SIX SENSORS ENTER 2 - 4, FOR NINE ENTER 2 - 7

4

>> USING A PRE-ALLOCATED DATASET FOR UNIT FT17F001.

>> USING A PRE-ALLOCATED DATASET FOR UNIT FT18F001.

CATALOG AS TARGET? IF YES TYPE - 1 -, ELSE - 2 -

2

FOR MATCH FILTER DIREC FINDING ENTER - 1 - ELSE -2-

1

FOR PHASE DELAY METHOD ENTER -1, FOR LMS ENTER -2

2

ENTER DEGREE OF POLYNOMIAL DESIRED -I1-

FOR SIX SENSORS ENTER 2 - 4, FOR NINE ENTER 2 - 7

4

TO VIEW OTHER SENSORS ENTER - 1 -

1

ENTER - 2 - TO CONTINUE TO NEXT TIME FRAME

2



## PROGRAM LISTING

VARIABLE NAME	TYPE	DESCRIPTION
DATAI-9	INTEGER	ARRAYS OF EXPERIMENTAL DATA LOADED FROM A DATA FILE
PARL-9	REAL	ARRAYS FOR SENSORS RELATIVE SPECTRAL POWERS
FORR-11	INTEGER	SENSOR NUMBER FOR DISPLAY OR ANALYSIS
IMK	INTEGER	ARRAY USED BY THE FFT ROUTINE
DIRECT	REAL	VALUE OF INITIAL PRIMARY TARGET DIRECTION
CIRC	REAL	VALUE OF TARGET DIRECTION
LOW, HIGH	INTEGER	LOW AND HIGH ANGLES SPECIFYING THE SECTOR FOR TARGETS OF INTEREST
	INTEGER	VALUE SELECTS CCMPRS OR TEK618 OUTPUT FOR PLCTS
TESTNO	INTEGER	EVENT NUMBER UNDER ANALYSIS OR TO BE PLOTTED
CCMMEN	REAL#4	ARRAYS USED FOR INPUT AND OUTPUT OF COMMENTS OF THE EXPERIMENTAL EVENT
CCMM1	REAL	UNDER EVALUATION
CCMM2	REAL	SAMPLING FREQUENCY
CCSF	REAL	FREQUENCY INCREMENT
XT, XF	REAL	TIMES INCREMENT IN THE CALCULATION OF THE TIME AND FREQUENCY AXIS
TIME	REAL	TIME FREQUENCY ARRAY
FRAI-9, RI-9	REAL	ARRAYS OF EXPERIMENTAL DATA





[illegible]



















```

160 1DATA7(I - 5),DATA7(I - 4),DATA7(I - 3),DATA7(I - 2),
2DATA7(I - 1),DATA7(I)
DO CONTINUE
DO REAL = 10,1020
1DATA7A8(I - 9),DATA8(I - 8),DATA8(I - 7),DATA8(I - 6),
2DATA7A8(I - 5),DATA7A8(I - 4),DATA7A8(I - 3),DATA7A8(I - 2),
DO CONTINUE
DO COMPLEX = 10,1020
1DATA7A9(I - 5),DATA9(I - 4),DATA9(I - 3),DATA9(I - 2),
2DATA7A9(I - 1),DATA9(I)
DO CONTINUE
180
181
C CONVERT THE INTEGER DATA TO REAL AND COMPLEX VALUES
CALL MYCATTIME,DATA1,N,RA1,A1)
CALL MYCATTIME,DATA2,N,RA2,A2)
CALL MYCATTIME,DATA3,N,RA3,A3)
CALL MYCATTIME,DATA4,N,RA4,A4)
CALL MYCATTIME,DATA5,N,RA5,A5)
CALL MYCATTIME,DATA6,N,RA6,A6)
IF (NUNSEN) GO TO 86
CALL MYCATTIME,DATA7,N,RA7,A7)
CALL MYCATTIME,DATA8,N,RA8,A8)
CALL MYCATTIME,DATA9,N,RA9,A9)
C IF SIMULATION IS REQUESTED, CALL THE SIMULATION ROUTINE
IF (INSIMUL).EQ.(1) CALL SIMULT(RA1,RA2,RA3,RA4,RA5,RA6,
1RA7,RA8,RA9,A1,A2,A3,A4,A5,A6,A7,A8,A9,V,A,ND,INOISE,TIME,JL,P,
2REDUCE,NUMSEN)
C CALCULATE THE FFT AND SPECTRAL FREQUENCY POWER FOR EACH SENSORS DATA
CALL FFT2C(A1,M,IMK)
CALL SPCFRM(TIME,RA1,FREQ,A1,N,PWR1,PDE1,PH1)
CALL FFT2C(A2,M,IMK)
CALL SPCFRM(TIME,RA2,FREQ,A2,N,PWK2,PDB2,PH2)
CALL FFT2C(A3,M,IMK)
CALL SPCFRM(TIME,RA3,FREQ,A3,N,PWR3,PDE3,PH3)
CALL FFT2C(A4,M,IMK)
CALL SPCFRM(TIME,RA4,FREQ,A4,N,PWR4,PDE4,PH4)
CALL FFT2C(A5,M,IMK)

```

```

MF 102410
MF 102420
MF 102430
MF 102440
MF 102450
MF 102460
MF 102470
MF 102480
MF 102490
MF 102500
MF 102510
MF 102520
MF 102530
MF 102540
MF 102550
MF 102560
MF 102570
MF 102580
MF 102590
MF 102600
MF 102610
MF 102620
MF 102630
MF 102640
MF 102650
MF 102660
MF 102670
MF 102680
MF 102690
MF 102700
MF 102710
MF 102720
MF 102730
MF 102740
MF 102750
MF 102760
MF 102770
MF 102780
MF 102790
MF 102800
MF 102810
MF 102820
MF 102830
MF 102840
MF 102850
MF 102860
MF 102870
MF 102880

```









[illegible]



MF 1 0 0 3 850  
MF 1 0 0 3 860  
MF 1 0 0 3 870  
MF 1 0 0 3 880  
MF 1 0 0 3 890  
MF 1 0 0 3 900  
MF 1 0 0 3 910  
MF 1 0 0 3 920  
MF 1 0 0 3 930  
MF 1 0 0 3 940  
MF 1 0 0 3 950  
MF 1 0 0 3 960  
MF 1 0 0 3 970  
MF 1 0 0 3 980  
MF 1 0 0 3 990  
MF 1 0 0 4 000  
MF 1 0 0 4 010  
MF 1 0 0 4 020  
MF 1 0 0 4 030  
MF 1 0 0 4 040  
MF 1 0 0 4 050  
MF 1 0 0 4 060  
MF 1 0 0 4 070  
MF 1 0 0 4 080  
MF 1 0 0 4 090  
MF 1 0 0 4 100  
MF 1 0 0 4 110  
MF 1 0 0 4 120  
MF 1 0 0 4 130  
MF 1 0 0 4 140  
MF 1 0 0 4 150  
MF 1 0 0 4 160  
MF 1 0 0 4 170  
MF 1 0 0 4 180  
MF 1 0 0 4 190  
MF 1 0 0 4 200  
MF 1 0 0 4 210  
MF 1 0 0 4 220  
MF 1 0 0 4 230  
MF 1 0 0 4 240  
MF 1 0 0 4 250  
MF 1 0 0 4 260  
MF 1 0 0 4 270  
MF 1 0 0 4 280  
MF 1 0 0 4 290  
MF 1 0 0 4 300  
MF 1 0 0 4 310  
MF 1 0 0 4 320

117 CALL MAXMIN(RA6,1024,K,RAGMAX,L,RIN)  
IF (ABS(RAGMAX)) .GT. (TNOISE)) GO TC 117  
GOAL 1 TO MATCH  
CALL 1 419 H(RA6,NTYP,SCALE,IORR,DIRECT,THRES,BCAT,TESTNO,JL,C,N,  
1 TS,TF,TIME,RAS,DIRECT,SCALE,ICRR,NTYP,TESTNO,TS,TF,C)  
CALL 1 419 H(FREQ,PWR6,DIRECT,SCALE,IORR,NTYP,TESTNO,TS,TF,C)  
C  
C  
C 449  
IF (ICRR) .NE. (7)) GO TC 450  
CALL MAXMIN(RA7,1024,K,RAGMAX,L,RIN)  
IF (ABS(RAGMAX)) .GT. (TNOISE)) GO TC 118  
GOAL 1 TO MATCH  
CALL 1 419 H(RA7,NTYP,SCALE,IORR,DIRECT,THRES,BCAT,TESTNO,JL,C,N,  
1 TS,TF,TIME,RAS,DIRECT,SCALE,ICRR,NTYP,TESTNO,TS,TF,C)  
CALL 1 419 H(FREQ,PWR7,DIRECT,SCALE,IORR,NTYP,TESTNO,TS,TF,C)  
C  
C  
C 450  
IF (ICRR) .NE. (8)) GO TC 451  
CALL MAXMIN(RA8,1024,K,RAGMAX,L,RIN)  
IF (ABS(RAGMAX)) .GT. (TNOISE)) GO TC 119  
GOAL 1 TO MATCH  
CALL 1 419 H(RA8,NTYP,SCALE,ICRR,DIRECT,THRES,BCAT,TESTNO,JL,C,N,  
1 TS,TF,TIME,RAS,DIRECT,SCALE,ICRR,NTYP,TESTNO,TS,TF,C)  
CALL 1 419 H(FREQ,PWR8,DIRECT,SCALE,IORR,NTYP,TESTNO,TS,TF,C)  
C  
C  
C 451  
IF (ICRR) .NE. (9)) GO TC 452  
CALL MAXMIN(RA9,1024,K,RAGMAX,L,RIN)  
IF (ABS(RAGMAX)) .GT. (TNOISE)) GO TC 125  
GOAL 1 TO MATCH  
CALL 1 419 H(RA9,NTYP,SCALE,IORR,DIRECT,THRES,BCAT,TESTNO,JL,C,N,  
1 TS,TF,TIME,RAS,DIRECT,SCALE,ICRR,NTYP,TESTNO,TS,TF,C)  
CALL 1 419 H(FREQ,PWR9,DIRECT,SCALE,IORR,NTYP,TESTNO,TS,TF,C)  
C  
C  
C 452  
IF (ABS(RAGMAX)) .LT. (TNOISE)) GO TC 454





```

837 WRITE(C,637)
   FORMAT(C,15) MNY
   IF((MNY).EQ.(1)) CALL MULTI(RA1,RA2,RA3,RA4,RA5,RA6,RA7,RA8,
1RA9,NTYP,SCALE,IOERR,THRES,BCAT,TESTNO,JL,C,TS,F,V,A,ND,
2NW,NUMSEN,TIME,ITRGET,CIRECT,DIR,DIRC)
   IF((MNY).NE.(1)) GC TO 454
44  WRITE(C,644)
   FORMAT(C,6)
393 READ(C,393) NGL
   FORMAT(11)
DO 666 I21 = 1,5
   NTAR(I21) = C
666 CONTINUE
   IF((NGL).EQ.(1)) GO TO 101
DO 678 JW = 1,5
   NTAR(1) = ITRGET(1,IW)
   NTAR(2) = ITRGET(2,IW)
   NTAR(3) = ITRGET(3,IW)
   NTAR(4) = ITRGET(4,IW)
   NTAR(5) = ITRGET(5,IW)
   NTAR(6) = ITRGET(6,IW)
   IF(NUMSEN.EQ.(6)) GC TC 646
   NTAR(7) = ITRGET(7,IW)
   NTAR(8) = ITRGET(8,IW)
   NTAR(9) = ITRGET(9,IW)
   NG = JW
   IF((NTAR(1)).EQ.(C)) GC TC 678
   CALL LMS(NTAR,DIRC,NUMSEN,C,SCALE,TESTNO,TIME,NG,Y,
1VX,X,TT,INDEX,NCR,TRIX,B,WKAREA)
   CALL PLT(C,SCALE,TESTNC,NUMSEN,TIME,Y,VX,X,TT,INDEX,NOR,DIRC,
1NG)
   DIR(NG) = DIRC
678 CCNT INUE
   GO TO 6C1
C
C PHASE DELAY METHOD
C
101 DO 60 J3 = 1,5
   TC = C
   DC 7C K3 = 1,NUMSEN
   TCEN(K3) = FLOAT(ITRGET(K3,J3))
   TC = FLCAT(ITRGET(K3,J3)) + TC
   CCNT INUE
   TC = TC/FLOAT(NUMSEN)
   CB = C.
   DIVICE = C.
   DO 84C N = 1,NUMSEN

```

```

MFI 04330
MFI 04340
MFI 04350
MFI 04360
MFI 04370
MFI 04380
MFI 04390
MFI 04400
MFI 04410
MFI 04420
MFI 04430
MFI 04440
MFI 04450
MFI 04460
MFI 04470
MFI 04480
MFI 04490
MFI 04500
MFI 04510
MFI 04520
MFI 04530
MFI 04540
MFI 04550
MFI 04560
MFI 04570
MFI 04580
MFI 04590
MFI 04600
MFI 04610
MFI 04620
MFI 04630
MFI 04640
MFI 04650
MFI 04660
MFI 04670
MFI 04680
MFI 04690
MFI 04700
MFI 04710
MFI 04720
MFI 04730
MFI 04740
MFI 04750
MFI 04760
MFI 04770
MFI 04780
MFI 04790
MFI 04800

```



```

DO 5C M = 1, NUMSEN
  IF((M).LE.(N)) GO TO 90
  RE = ((TC - TCEN(M))*X(N) - (TC - TCEN(N))*X(M))
  AA = ((TC - TCEN(N))*Y(M) - (TC - TCEN(N))*Y(N))
  IF((AA).EC.(0)) GO TO 90
  IF((BB).LT.(.000001)) GU TO 90
  DIVIDE = DIVIDE + 1.
  CE = ATAN(BB/AA) + QB
  CONTINUE
90 CONTINUE
840 NUM = NUMSEN - 1
  QB = (CE/(DIVIDE))*(180.0/3.141593)
  DIR(J3) = CE
  CONTINUE
60 CALL MLTPLY(C, SCALE, TESTNU, TS, IF, DIR, V, A, ND, ITRGET)
601
C SELECT TC EVALUATE OTHER SENSORS IN THIS TIME PERIOD OR CONTINUE
C TC THE NEXT TIME PERIOD
454 WRITE(6,51)
  WRITE(6,52)
  FORMAT(10,' TO VIEW OTHER SENSORS ENTER - 1 - ')
51 FORMAT(10,' ENTER - 2 - TO CONTINUE TO NEXT TIME FRAME ')
52
551 READ(10,551)NS
  FORMAT(11)
  IF((NS).NE.(1)) GO TO 10
  WRITE(6,57)
  FORMAT(10,' ENTER NEW SENSCK NUMBER FOR DISPLAY-11- ')
57 READ(10,551)ICRR
  GO TO 55
  CCNT INLE
  CALL DCNEPL
  STCP
  END
10
C SUBROUTINE ANGLE COMPUTES A ROUGH DIRECTION TO THE PRIMARY TARGET
C FOR USE IN DETERMINING WHETHER THE TARGET IS IN
C THE SECTOR OF INTEREST
C TIME DOMAIN ANALYSIS IS USED.
  SUEROUTINE ANGLE (DIRC,R1,R2,R3,R4,R5,R6,R7,R8,R9,NUMSEN,TESTNU,
  1 TIME,C,SCALE,NTAR)
  INTEGER M(9),TESTINC,NTAR(9),NUMSEN,C
  REAL R1(1024),R2(1024),R3(1024),R4(1024),R5(1024),R6(1024),
  1 R7(1024),R8(1024),R5(1024),TIME(1024),DIR(5),DIRC
  DO 12 I = 1,9
    NTAR(I) = 0

```

```

MF104810
MF104820
MF104830
MF104840
MF104850
MF104860
MF104870
MF104880
MF104890
MF104900
MF104910
MF104920
MF104930
MF104940
MF104950
MF104960
MF104970
MF104980
MF104990
MF105000
MF105010
MF105020
MF105030
MF105040
MF105050
MF105060
MF105070
MF105080
MF105090
MF105100
MF105110
MF105120
MF105130
MF105140
MF105150
MF105160
MF105170
MF105180
MF105190
MF105200
MF105210
MF105220
MF105230
MF105240
MF105250
MF105260
MF105270
MF105280

```





12

```

CONTINUE
CALL MAXMIN(R1,1024,M(1),RMAX,L,RMIN)
CALL MAXMIN(R2,1024,M(2),RMAX,L,RMIN)
CALL MAXMIN(R3,1024,M(3),RMAX,L,RMIN)
CALL MAXMIN(R4,1024,M(4),RMAX,L,RMIN)
CALL MAXMIN(R5,1024,M(5),RMAX,L,RMIN)
CALL MAXMIN(R6,1024,M(6),RMAX,L,RMIN)
IF((NUMSEN).EQ.(6)) GOTO 10
CALL MAXMIN(R7,1024,M(7),RMAX,L,RMIN)
CALL MAXMIN(R8,1024,M(8),RMAX,L,RMIN)
CALL MAXMIN(R9,1024,M(9),RMAX,L,RMIN)
DO 11 I2 = 1,NUMSEN
  NTAR(I2) = M(I2)
CONTINUE
RETURN
END

```

10

11

C  
C  
C  
C

SUBROUTINE TIMOUT PLCTS AMPLITUDE VERSUS TIME FOR THE SELECTED  
SENSOR

```

SUBROUTINE TIMOUT (TIME,RA,DIRECT,SCALE,IORR,NTYP,TESTNO,IS,IF,
1C)
REAL RA(1024),TIME(1024)
INTEGER NTYP(6),C,NY,DIRECT,TESTNO
IF((C).EQ.(1)) CALL COMPRS
IF((C).NE.(1)) CALL TEK618
CALL PAGER(11.0,E.5)
CALL NCRCR
CALL BLCWUP(SCALE)
CALL AREA2D(9.C,6.C)
CALL FRAME
CALL XNAME('TIME - SECONDS-',14)
CALL YNAME('INPLT',5)
CALL HEADING('SENSOR NUMBER',14,2.0,5.5)
CALL MESSAGE('IORR',4.C,5.5)
CALL INTNO(IORR,4.C,5.5)
CALL MESSAGE('EVENT NUMBER',12,2.0,5.7)
CALL INTNC(TESTNO,4.0,5.7)
CALL MESSAGE('TARGET I.D.',11,2.0,5.3)
XPCS = 2.80
IF((NTYP(1)).NE.(0)) XPCS = XPCS + 1.2
IF((NTYP(1)).NE.(0))
1CALL MESSAGE('TRKD-VEH',8,XPOS,5.3)
IF((NTYP(2)).NE.(0)) XPOS = XPOS + 1.2
IF((NTYP(2)).NE.(0))
1CALL MESSAGE('WHLD-VEH',8,XPCS,5.3)
IF((NTYP(3)).NE.(0)) XPOS = XPOS + 1.2
IF((NTYP(3)).NE.(0))

```

MF1005390  
MF1005300  
MF1005310  
MF1005320  
MF1005330  
MF1005340  
MF1005350  
MF1005360  
MF1005370  
MF1005380  
MF1005390  
MF1005400  
MF1005410  
MF1005420  
MF1005430  
MF1005440  
MF1005450  
MF1005460  
MF1005470  
MF1005480  
MF1005490  
MF1005500  
MF1005510  
MF1005520  
MF1005530  
MF1005540  
MF1005550  
MF1005560  
MF1005570  
MF1005580  
MF1005590  
MF1005600  
MF1005610  
MF1005620  
MF1005630  
MF1005640  
MF1005650  
MF1005660  
MF1005670  
MF1005680  
MF1005690  
MF1005700  
MF1005710  
MF1005720  
MF1005730  
MF1005740  
MF1005750  
MF1005760



```

1CALL MESSAGE('SHL-BLST',8,XPOS,5.3)
IF((NTYP(4)).NE.(0)) XPCS = XPCS + 1.2
IF((NTYP(4)).NE.(0))
1CALL MESSAGE('HELICPR',8,XPOS,5.3)
IF((NTYP(5)).NE.(0)) XPOS = XPOS + 1.2
IF((NTYP(5)).NE.(0))
1CALL MESSAGE('PERSONNEL',9,XPOS,5.3)
1CALL MESSAGE('INIT CIRECTION',14,2.0,5.1)
CALL INTNC(DIRECT,4.0,5.1)
CALL INTXNS(0.)
CALL YAXANG(10.)
CALL XTICKS(10)
CALL YTICKS(10)
TS = FLCAT(IFIX(TIME(1)))
TF = FLCAT(IFIX(TIME(1024) + 1.))
CALL MAXMIN(RA,1024,K,RAMAX,L,RAMIN)
IAMP = 1
DO 337 NI = 100,5000,100

```

```

337 NI = 100,5000,100
IF((IAMP).NE.(1)) GO TO 337
IF((NI).GE.(ABS(RAMAX))) IAMP = NI
CONTINUE
STEP = IAMP/5.0

```

```

CALL GRAF(TS,1,IF,FLCAT(-IAMP),STEP,FLCAT(IAMP))
CALL CURVE(TIME,RA,1024,0.)
CALL ENPL(0)
WRITE(6,70)

```

```

70 FORMAT(0,'CATALOG AS TARGET? IF YES TYPE - 1 --, ELSE - 2 --')
READ(10,71)NY
FORMAT(1)

```

```

C SEISMIC DATA DESIRED TO BE USED AS A SAMPLE SIGNAL IN THE MATCHED
C FILTER CAN BE STORED IN THE FILTER DATA FILE.
C

```

```

IF((NY).NE.(1)) GO TO 45
DO 44 JJ = 4,1024,4
IF((ABS(RA(JJ))) .LT. (.001)) RA(JJ) = 0
IF((ABS(RA(JJ) - 1))) .LT. (.001)) RA(JJ - 1) = 0
IF((ABS(RA(JJ) - 2))) .LT. (.001)) RA(JJ - 2) = 0
IF((ABS(RA(JJ) - 3))) .LT. (.001)) RA(JJ - 3) = 0
WRITE(4,3)RA(JJ-2),RA(JJ-1),RA(JJ)
FORMAT(3X,F9.2,3X,F9.2,3X,F9.2)
CONTINUE
RETURN
END

```

```

C SUBROUTINE FREQOT PLCTS SPECTRAL POWER VERSUS FREQUENCY
C

```

```

SUBROUTINE FREQCT(FREQ,PWR,DIRECT,SCALE,IORF,NTYP,TESTNC,TS,TF,

```



```

1C) AL PWR(1024), FREQ(1024), C, DIRECT, TESTNO
INTEGER NTYP(6), C, DIRECT, TESTNO
IF((C).EQ.(1)) CALL CCMFAS
IF((C).NE.(1)) CALL TEK618
CALL PAGE(11.0, 8.5)
CALL NCERDR
CALL BLCKUP(SCALE)
CALL AREA2D(9.0, 6.0)
CALL FRAME
CALL XNAME('FREQUENCY -HZ-', 14)
CALL XNAME('POWER', 5)
CALL HEADIN('SENSOR POWER -VS- FREQUENCY', 27, 2.0, 1)
CALL MESSAG('EVENT NUMBER', 13, 2.0, 5.7)
CALL INTC('TESTNO', 4.0, 5.7)
CALL MESSAG('SENSOR NUMBER', 14, 2.0, 5.5)
CALL INTC('IDRR', 4.0, 5.5)
CALL MESSAG('TARGET I.D.', 11, 2.0, 5.3)
XPCS = 2.80
IF((NTYP(1)).NE.(0)) XPCS = XPCS + 1.2
IF((NTYP(1)).NE.(0))
1CALL MESSAG('TRKD-VEH', 8, XPCS, 5.3)
IF((NTYP(2)).NE.(0)) XPCS = XPCS + 1.2
IF((NTYP(2)).NE.(0))
1CALL MESSAG('WHLD-VEH', 8, XPCS, 5.3)
IF((NTYP(3)).NE.(0)) XPCS = XPCS + 1.2
IF((NTYP(3)).NE.(0))
1CALL MESSAG('SHL-BLST', 8, XPCS, 5.3)
IF((NTYP(4)).NE.(0)) XPCS = XPCS + 1.2
IF((NTYP(4)).NE.(0))
1CALL MESSAG('HELICPTR', 8, XPCS, 5.3)
IF((NTYP(5)).NE.(0)) XPCS = XPCS + 1.2
IF((NTYP(5)).NE.(0))
1CALL MESSAG('PERSONNEL', 9, XPCS, 5.3)
1CALL MESSAG('INIT DIRECTION', 14, 2.0, 5.1)
CALL INTC('DIRECT', 4.0, 5.1)
CALL MESSAG('TIME PERIOD(SEC)', 16, 2.0, 4.9)
CALL REALNC('TS', 2, 3.9, 4.9)
CALL REALNC('TF', 2, 4.7, 4.9)
XMAX = 1.0
DO 39 I = 20, 500, 20
IF((XMAX).NE.(1.0)) GO TO 39
IF((1).GE.(IFX(FREQ(512)))) XMAX = FLOAT(1)
CONTINUE
XSTEP = XMAX/4.0
CALL MAXMIN(PWR, 1024, KP, PWRMAX, LP, PWRMIN)
NS = IFIX(XSTEP)
IF((XSTEP).GT.(20.0)) NS = IFIX(FLCAT(NS)/10.0)

```

MF106250  
MF106260  
MF106270  
MF106280  
MF106290  
MF106300  
MF106310  
MF106320  
MF106330  
MF106340  
MF106350  
MF106360  
MF106370  
MF106380  
MF106390  
MF106400  
MF106410  
MF106420  
MF106430  
MF106440  
MF106450  
MF106460  
MF106470  
MF106480  
MF106490  
MF106500  
MF106510  
MF106520  
MF106530  
MF106540  
MF106550  
MF106560  
MF106570  
MF106580  
MF106590  
MF106600  
MF106610  
MF106620  
MF106630  
MF106640  
MF106650  
MF106660  
MF106670  
MF106680  
MF106690  
MF106700  
MF106710  
MF106720



```

CALL INXANG (0.)
CALL YXANGS (NS)
CALL XTICKS (10)
CALL GRAF (0., XSTEP, XMAX, 0., -1, PWRMAX)
CALL CLEVE (FREQ, PWR, 512, 0.)
CALL RESET ('ALL')
CALL RECEPL (0)
CONTINUE
RETURN
END

```

38  
37

C  
C  
C  
C  
C  
C

SUBROUTINE MATCH PERFORMS THE MATCHED FILTERING OF THE SELECTED  
SENSORS DATA. TARGET CLASSIFICATIONS FOUND ARE RETURNED, AS ARE  
THEIR RESPECTIVE PEAK SIGNAL DETECTION POSITIONS.

```

SUBROUTINE MATCH(RMAG,NTYP,SCALE,ICRR,DIRECT,THRES,TCAT,TESTNO,
1JL,C,NT,TS,TF,TIME)
REAL RMAG(NT),CAT(1024),UNIT(11264),PLATE(2048),SCAT(1024),
1RMAT(11264),THRES,XRAY4(2),XRAY3(2),TIME(1024),
2XRAY1(2),XRAY2(2),XRAY3(2),TCAT(512)
INTEGER NTYP(6),C,DIRECT,TESTNO

```

C

```

DATA XRAY1/2048.,2048./
DATA XRAY2/4096.,4096./
DATA XRAY3/6144.,6144./
DATA XRAY4/8192.,8192./
DATA XRAY1/-1.0,1.0/
DO 33 J = 1,1024
PLATE(J) = 0.
PLATE(J) + 1024 = 0.
SCAT(J) = 0.
CAT(J) = 0.
CONTINUE
NH = NT*2
N2 = NT*2
N4 = NT*4
N8 = NT*8
N10 = NT*10
N11 = NT*11
DO 600 MM = 1,N11
RMAT(MM) = 0.0
UNIT(MM) = MM
CONTINUE
DO 201 K = N2,N10,N2
NM = K - NT
DO 202 KK = 1,NT

```

33

600

MF106730  
MF106740  
MF106750  
MF106760  
MF106770  
MF106780  
MF106790  
MF106800  
MF106810  
MF106820  
MF106830  
MF106840  
MF106850  
MF106860  
MF106870  
MF106880  
MF106890  
MF106900  
MF106910  
MF106920  
MF106930  
MF106940  
MF106950  
MF106960  
MF106970  
MF106980  
MF106990  
MF107000  
MF107010  
MF107020  
MF107030  
MF107040  
MF107050  
MF107060  
MF107070  
MF107080  
MF107090  
MF107100  
MF107110  
MF107120  
MF107130  
MF107140  
MF107150  
MF107160  
MF107170  
MF107180  
MF107190  
MF107200







```

202 RMAT(NM + KK) = RMAG(KK)
201 CONTINUE
    NTYP(1) = 0
    NTYP(2) = 0
    NTYP(3) = 0
    NTYP(4) = 0
    NTYP(5) = 0
C
C NEW FILTER SAMPLE SIGNALS ARE LOADED AFTER EACH SUCCESSIVE 2048
C ELEMENTS OF THE WORKING ARRAY *RMAT* ARE CONVOLVED
C
111 DO 400 I=1,N10
    IF((I).EQ.(1)).OR.((I).EQ.(N2)).OR.((I).EQ.(N4)).OR.
    1((I).EQ.(N6)).OR.((I).EQ.(N8)))
    2GO TO 33
    GO TO 55
    IF((I).EQ.(1)) MARK = 1025
    IF((I).EQ.(N2)) MARK = 2045
    IF((I).EQ.(N4)) MARK = 3073
    IF((I).EQ.(N6)) MARK = 4097
    IF((I).EQ.(N8)) MARK = 5121
C
C FILTER DATA REVERSED
C
C DO 777 LL = 1,NT
CAT(LL) = TCAT(-LL + MARK)
CONTINUE
777
C
C EXECUTION TIME MAY BE REDUCED BY SELECTING SMALLER WINDOWS OR
C SEGMENTS AROUND THE PEAK AMPLITUDES OF THE FILTER AND SEISMIC DATA
C
CALL MAXMIN(CAT,1024,LL,CATM,KK,CATMIN)
DO 10 11 = 1,NT
    IF((11 - NH).LE.(0)) LL = NH
    IF((LL).GT.(1024 - NH)) LL = 1024 - NH
    SCAT(11) = CAT(11 - NH + LL)
CONTINUE
10 CALL RMS(SCAT,NT,CATMAX)
99 CALL RMS(RMAG,NT,RAGMAX)
    CALL AVG(SCAT,NT,ACAT)
    RMAT(11) = 0
C
C REMOVAL OF DC BIAS AND NORMALIZATION OF THE FILTER AND SEISMIC DATA
C
C GC 2CC KN = 1,NT
    IF((CATMAX).EQ.(0)).OR.((RAGMAX).EQ.(0))) GO TO 200
C

```

MF107210  
MF107220  
MF107230  
MF107240  
MF107250  
MF107260  
MF107270  
MF107280  
MF107290  
MF107300  
MF107310  
MF107320  
MF107330  
MF107340  
MF107350  
MF107360  
MF107370  
MF107380  
MF107390  
MF107400  
MF107410  
MF107420  
MF107430  
MF107440  
MF107450  
MF107460  
MF107470  
MF107480  
MF107490  
MF107500  
MF107510  
MF107520  
MF107530  
MF107540  
MF107550  
MF107560  
MF107570  
MF107580  
MF107590  
MF107600  
MF107610  
MF107620  
MF107630  
MF107640  
MF107650  
MF107660  
MF107670  
MF107680



```

C DISCRETE CONVOLUTION PREFORMED
C
      RMAT(I) = ((RMAT(I + KN))/(ABS(RAGMAX)))*
      1/((SCAT(KN) - ACAT)/(CATMAX)) + RMAT(I)
      CONTINUE
      CONTINUE
      CALL MAXMIN(RMAT,N11,LZ,RATMAX,KZ,RATMIN)
      DO 390 NN = 1,N11
      IF ((RATMAX).EQ.(0)) GO TO 390
      RMAT(NN) = RMAT(NN)/(ABS(RATMAX))
      CONTINUE
390
C CLASSIFICATION OF TARGETS BY TARGET TYPE
C
      DO 302 J1 = N2,N10,N2
      DO 301 I1 = 1,N2
      PLATE(I1) = RMAT(J1 - N2 + I1)
      CONTINUE
      CALL MAXMIN(PLATE,N2,LP,PMAX,LS,PMIN)
      IF ((ABS(PMAX)).GE.(THRES)) NTYP(J1/N2) = LP
301
302
C MATCHED FILTER OUTPUT PLCTING
C
      IF ((IDFR).EQ.(0)) GC TC 391
      IF ((C).EQ.(1)) CALL CCMPS
      IF ((C).NE.(1)) CALL TEK618
      CALL PAGE(11.0,8.5)
      CALL NCERDR
      CALL BLCKUP(SCALE)
      CALL AREA2D(9.0,6.0)
      CALL FRAME
      CALL XNAME('POSITION',8)
      CALL YNAME('AMPLITUDE',8)
      CALL FNAME('MATCHED FILTER RESPONSE',23,2.0,1)
      CALL MESSAG('TRACKED VEH',11,2.25,5.8)
      CALL MESSAG('WHEEL VEH',11,2.00,5.8)
      CALL MESSAG('SHELL BLAST',11,4.00,5.8)
      CALL MESSAG('SHELL',4,6.0,5.8)
      CALL MESSAG('PERSONNEL',9,7.55,5.8)
      CALL MESSAG('SENSOR NUMBER',13,2.25,2.25)
      CALL MESSAG('EVENT',2,NUMBER,12,2.25,4.5)
      CALL MESSAG('TESTING',2.5,4.5)
      CALL MESSAG('TIME PERIOD(SEC)',16,2.25,0.05)
      TS = FLCAT(IFIX(TIME(1)))
      TF = FLCAT(IFIX(TIME(1024) + 1.))
      CALL REALNO(TS,2,2.4,0.05)

```

MF107690  
 MF107700  
 MF107710  
 MF107720  
 MF107730  
 MF107740  
 MF107750  
 MF107760  
 MF107770  
 MF107780  
 MF107790  
 MF107800  
 MF107810  
 MF107820  
 MF107830  
 MF107840  
 MF107850  
 MF107860  
 MF107870  
 MF107880  
 MF107890  
 MF107900  
 MF107910  
 MF107920  
 MF107930  
 MF107940  
 MF107950  
 MF107960  
 MF107970  
 MF107980  
 MF107990  
 MF108000  
 MF108010  
 MF108020  
 MF108030  
 MF108040  
 MF108050  
 MF108060  
 MF108070  
 MF108080  
 MF108090  
 MF108100  
 MF108110  
 MF108120  
 MF108130  
 MF108140  
 MF108150  
 MF108160







```

C
C
C
C
C
SUBROUTINE MAXMIN FINDS THE MAXIMUM AND MINIMUM VALUES FOR THE ARRAY
PASSED TO IT. IT ALSO RETURNS THE ELEMENT NUMBERS ASSOCIATED WITH
THE MAXIMUM AND MINIMUM VALUES.
MF108650
MF108660
MF108670
MF108680
MF108690
MF108700
MF108710
MF108720
MF108730
MF108740
MF108750
MF108760
MF108770
MF108780
MF108790
MF108800
MF108810
MF108820
MF108830
MF108840
MF108850
MF108860
MF108870
MF108880
MF108890
MF108900
MF108910
MF108920
MF108930
MF108940
MF108950
MF108960
MF108970
MF108980
MF108990
MF109000
MF109010
MF109020
MF109030
MF109040
MF109050
MF109060
MF109070
MF109080
MF109090
MF109100
MF109110
MF109120

SUBROUTINE MAXMIN(A,N,K,AMAX,L,AMIN)
REAL A(N)
AMAX = A(1)
AMIN = A(1)
K=1
L=1
DO 10 I=2,N
  IF ((A(I)).LE.(AMAX)) GO TO 20
  IF (AMAX=A(I))
    K=I
    AMIN=A(I)
  IF ((A(I)).GE.(AMIN)) GO TO 10
  AMIN=A(I)
  L=I
CONTINUE
IF ((ABS(AMIN)).GT.(ABS(AMAX))) AMAX = AMIN
RETURN
ENC
20
10
C
C
C
SUBROUTINE SPECTRM COMPUTES THE NORMALIZED POWER FOR THE COMPLEX ARRAY
PASSED TO IT.
MF109130
MF109140
MF109150
MF109160
MF109170
MF109180
MF109190
MF109200
MF109210
MF109220
MF109230
MF109240
MF109250
MF109260
MF109270
MF109280
MF109290
MF109300
MF109310
MF109320
MF109330
MF109340
MF109350
MF109360
MF109370
MF109380
MF109390
MF109400
MF109410
MF109420
MF109430
MF109440
MF109450
MF109460
MF109470
MF109480
MF109490
MF109500
MF109510
MF109520
MF109530
MF109540
MF109550
MF109560
MF109570
MF109580
MF109590
MF109600
MF109610
MF109620
MF109630
MF109640
MF109650
MF109660
MF109670
MF109680
MF109690
MF109700
MF109710
MF109720
MF109730
MF109740
MF109750
MF109760
MF109770
MF109780
MF109790
MF109800
MF109810
MF109820
MF109830
MF109840
MF109850
MF109860
MF109870
MF109880
MF109890
MF109900
MF109910
MF109920
MF109930
MF109940
MF109950
MF109960
MF109970
MF109980
MF109990
MF110000

SUBROUTINE SPECTRM(T,RA,F,A,N,PWR,PWRDB,PHASE)
REAL T(N),RA(N),F(N),PWR(N),PHASE(N)
COMPLEX A(N)
DO 10 K=1,N
  PWR(K)=CABS(A(K))**2
  AR=REAL(A(K))
  AI=AIMAG(A(K))
  IF (AR.EQ.C.0.AND.AI.EC.0.0) GC TO 40
  PHASE(K)=ATAN2(AI,AR)
  GC TC 50
PHASE(K)=0.0
CONTINUE
CONTINUE
N2=N/2
CALL MAXMIN(PWR,N,KF,PMAX,LP,PMIN)
C NCRMALIZE POWER SPECTRUM
DO 60 J=1,N
  PWR(J)=PWR(J)/AES(PMAX)
CONTINUE
RETURN
END
60
C

```





```

C      SUBROUTINE MULTI IS THE MULTIPLE TARGET DIRECTION ROUTINE.
C      DIRECTIONS ARE COMPUTED FOR UP TO FIVE TARGET CLASSES. FOR SINGLE
C      TARGETS, ADAPTIVE MATCHED FILTERING IS PERFORMED ALLCING FOR
C      IMPROVED ACCURACY.
C
C      SUBROUTINE MULTI(RMAG1,RMAG2,RMAG3,RMAG4,RMAG5,RMAG6,RMAG7,
1    RMAG8,RMAG9,NTYP,SCALE,IORR,THRES,ECAT,TESTNO,JL,C,IS,TF,
2    V,A,ND,NW,NUMSEN,TIME,IIRGET,DIRECT,CIR,DIRC)
C      INTEGER NTYP(6),C,NW,IIIRGET(9,5),DIRECT,
1    INTR,ND(4),TESTINC,NUMSEN
C      REAL RMAG1(1024),RMAG2(1024),RMAG3(1024),RMAG4(1024),RMAG5(1024),
1    RMAG6(1024),RMAG7(1024),RMAG8(1024),RMAG9(1024),
2    BCCAT(512C),CCAT(512C),TIME(1024),DIR(5),DIRC,
3    X(9),Y(9),THETA(9),T(9),V(4),A(4),RMAG(1024)
C
C      NSEN = 1
C      NH = NW/2
C      DO 6 I1 = 1,512C
C      CCAT(I1) = BCCAT(I1)
C      CONTINUE
C
C      ADAPTIVE MATCHED FILTERING FOR A SINGLE TARGET IS ACCOMPLISHED
C      BY USING THE SELECTED SENSOR'S SEISMIC DATA AS THE MATCHED FILTER
C      WHEN COMPUTING THE IDENTIFIED TARGET'S DIRECTION.
C
C      NTR = C
C      DO 888 I14 = 1,4
C      IF((V(I14)).NE.(0)) GC TC 5
C      CONTINUE
C      DO 377 JV = 1,5
C      IF((NTYP(JV)).NE.(0)) NTR = NTR + 1
C      CONTINUE
C      IF((INTYP(1)).EQ.(0)) GC TO 1
C      IF((INTR).NE.(1)) GC TC 1
C      NTR = NTR + 1
C      DO 151 I2 = 1,1024
C      CCAT(I2) = RMAG1(I2)
C      CONTINUE
C      IF((INTYP(2)).EQ.(0)) GC TO 2
C      IF((INTR).NE.(1)) GC TO 2
C      NTR = NTR + 1
C      DO 102 I3 = 1,1024
C      CCAT(I3) = RMAG2(I3)
C      CONTINUE
C      IF((INTYP(3)).EQ.(0)) GC TO 3
C      IF((INTR).NE.(1)) GC TO 3
C      NTR = NTR + 1

```

```

MF105130
MF105140
MF105150
MF105160
MF105170
MF105180
MF105190
MF105200
MF105210
MF105220
MF105230
MF105240
MF105250
MF105260
MF105270
MF105280
MF105290
MF105300
MF105310
MF105320
MF105330
MF105340
MF105350
MF105360
MF105370
MF105380
MF105390
MF105400
MF105410
MF105420
MF105430
MF105440
MF105450
MF105460
MF105470
MF105480
MF105490
MF105500
MF105510
MF105520
MF105530
MF105540
MF105550
MF105560
MF105570
MF105580
MF105590
MF105600

```



```

103      DC 103 I4 = 1,1024
3          CCAT(I4 + 2048) = RMAG3(I4)
          CCNTINLE
          IF((NTYP(4)),EQ.(0)) GC TO 4
          IF((NTR).NE.(1)) GC TC 4
          NTR = NTR + 1
104      DC 104 I5 = 1,1024
4          CCAT(I5 + 3072) = RMAG4(I5)
          CCNTINLE
          IF((NTYP(5)),EQ.(0)) GC TO 5
          IF((NTR).NE.(1)) GC TO 5
105      DC 105 I6 = 1,1024
5          CCAT(I6 + 4096) = RMAG5(I6)
          CCNTINLE
127      DO 127 J2 = 1,1024
          RMAG(J2) = 0.
          CCNTINLE
          II = 0
          C
          C
          C      FOR WINDING OF DATA, FIND THE POSITION OF THE PEAK AMPLITUDE
          C
          C      IF((IORR).EQ.(1)) CALL MAXMIN(RMAG1,1024,LM,RMAX,LM,RMIN)
          C      IF((IORR).EQ.(2)) CALL MAXMIN(RMAG2,1024,LM,RMAX,LM,RMIN)
          C      IF((IORR).EQ.(3)) CALL MAXMIN(RMAG3,1024,LM,RMAX,LM,RMIN)
          C      IF((IORR).EQ.(4)) CALL MAXMIN(RMAG4,1024,LM,RMAX,LM,RMIN)
          C      IF((IORR).EQ.(5)) CALL MAXMIN(RMAG5,1024,LM,RMAX,LM,RMIN)
          C      IF((IORR).EQ.(6)) CALL MAXMIN(RMAG6,1024,LM,RMAX,LM,RMIN)
          C      IF((IORR).EQ.(7)) CALL MAXMIN(RMAG7,1024,LM,RMAX,LM,RMIN)
          C      IF((IORR).EQ.(8)) CALL MAXMIN(RMAG8,1024,LM,RMAX,LM,RMIN)
          C      IF((IORR).EQ.(9)) CALL MAXMIN(RMAG9,1024,LM,RMAX,LM,RMIN)
          C
          C      REPEATED CALLS TO THE MATCHED FILTER ROUTINE ARE MADE WITH WINDOWED
          C      DATA FROM ALL SENSORS.
          C
          C      DO 555 IX = 1,9
          C      CC 666 IY = 1,5
          C      IIRGET(IX,IY) = 0
          C      CCNTINLE
          C      CONTINUE
          C      IF((LM - NH).LE.(0)) LM = NH
          C      IF((LM).GT.(1024 - NH)) LM = 1024 - NH
          C      DO 111 I7 = 1,NH
          C      RMAG(I7) = RMAG1(LM - NH + I7)
          C      CCNTINLE
          C      NTYP(1) = 0
          C      NTYP(2) = 0
          C      NTYP(3) = 0
          C      NTYP(4) = 0
          C
          C      666
          C      555
          C
          C      111

```



```

NTYP(5) = 0
CALL MATCH(RMAG,NTYP,SCALE,II,DIRECT,THRES,CCAT,TESTNO,JL,C,NW,
1TS,TF,TIME)
1ITARGET(1,1) = NTYP(1)
1ITARGET(1,2) = NTYP(2)
1ITARGET(1,3) = NTYP(3)
1ITARGET(1,4) = NTYP(4)
1ITARGET(1,5) = NTYP(5)
DO I12 = 1, Nw
RMAG(I8) = RMAG2(LM - NH + I8)
CONTINUE = 0
NTYP(1) = 0
NTYP(2) = 0
NTYP(3) = 0
NTYP(4) = 0
NTYP(5) = 0
CALL MATCH(RMAG,NTYP,SCALE,II,DIRECT,THRES,CCAT,TESTNO,JL,C,NW,
1TS,TF,TIME)
1ITARGET(2,1) = NTYP(1)
1ITARGET(2,2) = NTYP(2)
1ITARGET(2,3) = NTYP(3)
1ITARGET(2,4) = NTYP(4)
1ITARGET(2,5) = NTYP(5)
DO I13 = 1, Nw
RMAG(I9) = RMAG3(LM - NH + I9)
CONTINUE = 0
NTYP(1) = 0
NTYP(2) = 0
NTYP(3) = 0
NTYP(4) = 0
NTYP(5) = 0
CALL MATCH(RMAG,NTYP,SCALE,II,DIRECT,THRES,CCAT,TESTNO,JL,C,NW,
1TS,TF,TIME)
1ITARGET(3,1) = NTYP(1)
1ITARGET(3,2) = NTYP(2)
1ITARGET(3,3) = NTYP(3)
1ITARGET(3,4) = NTYP(4)
1ITARGET(3,5) = NTYP(5)
DO I14 = 1, Nw
RMAG(IA) = RMAG4(LM - NH + IA)
CONTINUE = 0
NTYP(1) = 0
NTYP(2) = 0
NTYP(3) = 0
NTYP(4) = 0
NTYP(5) = 0
CALL MATCH(RMAG,NTYP,SCALE,II,DIRECT,THRES,CCAT,TESTNO,JL,C,NW,
1TS,TF,TIME)

```

```

MF11C090
MF11C100
MF11C110
MF11C120
MF11C130
MF11C140
MF11C150
MF11C160
MF11C170
MF11C180
MF11C190
MF11C200
MF11C210
MF11C220
MF11C230
MF11C240
MF11C250
MF11C260
MF11C270
MF11C280
MF11C290
MF11C300
MF11C310
MF11C320
MF11C330
MF11C340
MF11C350
MF11C360
MF11C370
MF11C380
MF11C390
MF11C400
MF11C410
MF11C420
MF11C430
MF11C440
MF11C450
MF11C460
MF11C470
MF11C480
MF11C490
MF11C500
MF11C510
MF11C520
MF11C530
MF11C540
MF11C550
MF11C560

```



MF11C570  
MF11C580  
MF11C590  
MF11C600  
MF11C610  
MF11C620  
MF11C630  
MF11C640  
MF11C650  
MF11C660  
MF11C670  
MF11C680  
MF11C690  
MF11C700  
MF11C710  
MF11C720  
MF11C730  
MF11C740  
MF11C750  
MF11C760  
MF11C770  
MF11C780  
MF11C790  
MF11C800  
MF11C810  
MF11C820  
MF11C830  
MF11C840  
MF11C850  
MF11C860  
MF11C870  
MF11C880  
MF11C890  
MF11C900  
MF11C910  
MF11C920  
MF11C930  
MF11C940  
MF11C950  
MF11C960  
MF11C970  
MF11C980  
MF11C990  
MF11C1000  
MF11C1010  
MF11C1020  
MF11C1030  
MF11C1040

```

115  ITRGET(4,1) = NTYP(1)
      ITRGET(4,2) = NTYP(2)
      ITRGET(4,3) = NTYP(3)
      ITRGET(4,4) = NTYP(4)
      ITRGET(4,5) = NTYP(5)
      DO 115 IB = 1, NW
        RMAG(IB) = RMAG5(LM - NH + IB)
      CONTINUE
      NTYP(1) = 0
      NTYP(2) = 0
      NTYP(3) = 0
      NTYP(4) = 0
      NTYP(5) = 0
      CALL MATCH(RMAG, NTYP, SCALE, II, DIRECT, THRES, CCAT, TESTNO, JL, C, NW,
1      ITS, TF, TIME)
      ITRGET(5,1) = NTYP(1)
      ITRGET(5,2) = NTYP(2)
      ITRGET(5,3) = NTYP(3)
      ITRGET(5,4) = NTYP(4)
      ITRGET(5,5) = NTYP(5)
      DO 116 IC = 1, NW
        RMAG(IC) = RMAG6(LM - NH + IC)
      CONTINUE
      NTYP(1) = 0
      NTYP(2) = 0
      NTYP(3) = 0
      NTYP(4) = 0
      NTYP(5) = 0
      CALL MATCH(RMAG, NTYP, SCALE, II, DIRECT, THRES, CCAT, TESTNO, JL, C, NW,
1      ITS, TF, TIME)
      ITRGET(6,1) = NTYP(1)
      ITRGET(6,2) = NTYP(2)
      ITRGET(6,3) = NTYP(3)
      ITRGET(6,4) = NTYP(4)
      ITRGET(6,5) = NTYP(5)
      IF((NUMSEN).EQ.(6)) GO TO 101
      DO 117 IC = 1, NW
        RMAG(IC) = RMAG7(LM - NH + IC)
      CONTINUE
      NTYP(1) = 0
      NTYP(2) = 0
      NTYP(3) = 0
      NTYP(4) = 0
      NTYP(5) = 0
      CALL MATCH(RMAG, NTYP, SCALE, II, DIRECT, THRES, CCAT, TESTNO, JL, C, NW,
1      ITS, TF, TIME)
      ITRGET(7,1) = NTYP(1)
      ITRGET(7,2) = NTYP(2)

```





MF111C50  
MF111C60  
MF111C70  
MF111C80  
MF111C90  
MF111100  
MF111110  
MF111120  
MF111130  
MF111140  
MF111150  
MF111160  
MF111170  
MF111180  
MF111190  
MF111200  
MF111210  
MF111220  
MF111230  
MF111240  
MF111250  
MF111260  
MF111270  
MF111280  
MF111290  
MF111300  
MF111310  
MF111320  
MF111330  
MF111340  
MF111350  
MF111360  
MF111370  
MF111380  
MF111390  
MF111400  
MF111410  
MF111420  
MF111430  
MF111440  
MF111450  
MF111460  
MF111470  
MF111480  
MF111490  
MF111500  
MF111510  
MF111520

```

118      ITRGET(7,3) = NTYP(3)
      ITRGET(7,4) = NTYP(4)
      ITRGET(7,5) = NTYP(5)
      DO 1118 IE = 1,NH
      RMAG(IE) = RMAG8(LM - NH + IE)
      CONTINUE = 0
      NTYP(1) = 0
      NTYP(2) = 0
      NTYP(3) = 0
      NTYP(4) = 0
      NTYP(5) = 0
      CALL MATCH(RMAG,NTYP,SCALE,II,DIRECT,THRES,CCAT,TESTNO,JL,C,NW,
1      TS,TF,TIME)
      ITRGET(8,1) = NTYP(1)
      ITRGET(8,2) = NTYP(2)
      ITRGET(8,3) = NTYP(3)
      ITRGET(8,4) = NTYP(4)
      ITRGET(8,5) = NTYP(5)
      DO 1119 IF = 1,NH
      RMAG(IF) = RMAG9(LM - NH + IF)
      CONTINUE = 0
      NTYP(1) = 0
      NTYP(2) = 0
      NTYP(3) = 0
      NTYP(4) = 0
      NTYP(5) = 0
      CALL MATCH(RMAG,NTYP,SCALE,II,DIRECT,THRES,CCAT,TESTNO,JL,C,NW,
1      TS,TF,TIME)
      ITRGET(9,1) = NTYP(1)
      ITRGET(9,2) = NTYP(2)
      ITRGET(9,3) = NTYP(3)
      ITRGET(9,4) = NTYP(4)
      ITRGET(9,5) = NTYP(5)
      NTYP(1) = 0
      NTYP(2) = 0
      NTYP(3) = 0
      NTYP(4) = 0
      NTYP(5) = 0
      DC 675 IH = 1,55.
      DIR(IH) = 955.
      CONTINUE
      RETURN
      END
C
C
C      MULTIPLE DIRECTIONAL OUTPUT PLCTING
      SUBROUTINE MLTPLT(C,SCALE,TESTNC,TS,TF,CIR,V,A,ND,ITRGET)
      INTEGER C,NC(4),ITRGET(5,5)

```



```

REAL DIR(5),V(4),A(4)
IF((C).EQ.(1)) CALL CMPPRS
IF((C).NE.(1)) CALL TEK618
CALL PAGE(11.0,8.5)
CALL NCERDR
CALL BLCWUP(SCALE)
CALL AREA2D(10.C,6.C)
CALL FRAME
CALL HEADIN('MULTIPLE TARGET - MATCHED FILTER OUTPUT',35,2.0,1)
CALL MESSAGE('EVENT NUMBER',13,3.0,5.8)
CALL INTO('TESTINO,5.0,5.8)
CALL MESSAGE('TIME PERIOD(SEC)',16,3.0,5.4)
CALL REALNO('TS,2.4,5.5,5.4)
CALL REALNC('TF,2.5,7.5,5.4)
IF(((I)TRGET(1,1)).NE.(0)).AND.((DIR(1)).NE.(999.)))
1 IF(((I)TRGET(1,1)).NE.(0)).AND.((DIR(1)).NE.(999.)))
1 IF(((I)TRGET(1,2)).NE.(0)).AND.((DIR(2)).NE.(999.)))
1 IF(((I)TRGET(1,2)).NE.(0)).AND.((DIR(2)).NE.(999.)))
1 IF(((I)TRGET(1,3)).NE.(0)).AND.((DIR(3)).NE.(999.)))
1 IF(((I)TRGET(1,3)).NE.(0)).AND.((DIR(3)).NE.(999.)))
1 IF(((I)TRGET(1,4)).NE.(0)).AND.((DIR(4)).NE.(999.)))
1 IF(((I)TRGET(1,4)).NE.(0)).AND.((DIR(4)).NE.(999.)))
1 IF(((I)TRGET(1,5)).NE.(0)).AND.((DIR(5)).NE.(999.)))
1 IF(((I)TRGET(1,5)).NE.(0)).AND.((DIR(5)).NE.(999.)))
1 CALL MESSAGE('SIMULATED TRKD VEHICLE TARGET FREQUENCY',35,3.0,2.8)
CALL REALNC('DIR(5),2.6,5.3,4)
CALL REALNC('AMPLITUDE',9,4.0,2.6)
CALL MESSAGE('DIRECTION',9,4.0,2.4)
CALL REALNC('A(1),4,5.5,2.6)
D = FLCAT(NC(1))
CALL REALNC('D,4,5.5,2.4)
CALL REALNC('SIMULATED WHLD VEHICLE TARGET FREQUENCY',35,3.0,2.2)
CALL REALNC('V(2),2,8.0,2.2)
CALL MESSAGE('AMPLITUDE',9,4.0,2.0)
CALL REALNC('DIRECTION',9,4.0,1.80)
D = FLCAT(NC(2))
CALL REALNC('D,4,5.5,1.8)

```

```

MF1111530
MF1111540
MF1111550
MF1111560
MF1111570
MF1111580
MF1111590
MF1111600
MF1111610
MF1111620
MF1111630
MF1111640
MF1111650
MF1111660
MF1111670
MF1111680
MF1111690
MF1111700
MF1111710
MF1111720
MF1111730
MF1111740
MF1111750
MF1111760
MF1111770
MF1111780
MF1111790
MF1111800
MF1111810
MF1111820
MF1111830
MF1111840
MF1111850
MF1111860
MF1111870
MF1111880
MF1111890
MF1111900
MF1111910
MF1111920
MF1111930
MF1111940
MF1111950
MF1111960
MF1111970
MF1111980
MF1111990
MF1112000

```



```

CALL MESSAGE('SIMULATED HELICOPTER TARGET FREQUENCY',37,3.0,1.0)
CALL REALNC(V(3),2,8.0,1.0)
CALL MESSAGE('AMPLITUDE',9,4.0,1.4)
CALL MESSAGE('DIRECTION',9,4.0,1.2)
CALL REALNC(A(3),4,5.5,1.4)
D = FLCAI(NC(3))
CALL REALNC(D,4,5.5,1.2)
CALL MESSAGE('SIMULATED PERSONNEL TARGET FREQUENCY',36,3.0,1.0)
CALL REALNC(V(4),2,8.0,1.0)
CALL MESSAGE('AMPLITUDE',9,4.0,0.8)
CALL MESSAGE('DIRECTION',9,4.0,0.6)
CALL REALNC(A(4),4,5.5,0.8)
D = FLCAI(NC(4))
CALL REALNC(D,4,5.5,0.6)
CALL ENCLPL(0)
RETURN
END

C
C
C
SUBROUTINE RMS COMPUTES THE ROOT MEAN SQUARE VALUE OF THE N-ARRAY
DATA PASSED TO IT
C
C
C
SUBROUTINE RMS(A,N,TMAX)
REAL A(N)
TMAX = 0.
DO 200 I = 1,N
    TMAX = (A(I))**2 + TMAX
CONTINUE
TMAX = SQRT(TMAX)
RETURN
END
200

C
C
C
SUBROUTINE AVG COMPUTES THE AVERAGE VALUE OF THE N-ARRAY DATA PASSED
TO IT
C
C
C
SUBROUTINE AVG(A,N,AAVG)
REAL A(N)
AAVG = 0.
DO 100 I = 1,N
    AAVG = A(N) + AAVG
CONTINUE
AAVG = AAVG/FLOAT(N)
RETURN
END
100

C
C
C
SUBROUTINE SIMULATE ALLOWS FOR THE MODIFICATION OF EXPERIMENTAL
DATA TO INCLUDE UP TO FOUR SIMULATED TARGETS, AND MODIFICATION OF
SEISMIC SIGNAL AMPLITUDES ABOVE THE SELECTED NOISE LEVEL.

```

```

MF112C10
MF112C20
MF112C30
MF112C40
MF112C50
MF112C60
MF112C70
MF112C80
MF112C90
MF112100
MF112110
MF112120
MF112130
MF112140
MF112150
MF112160
MF112170
MF112180
MF112190
MF112200
MF112210
MF112220
MF112230
MF112240
MF112250
MF112260
MF112270
MF112280
MF112290
MF112300
MF112310
MF112320
MF112330
MF112340
MF112350
MF112360
MF112370
MF112380
MF112390
MF112400
MF112410
MF112420
MF112430
MF112440
MF112450
MF112460
MF112470
MF112480

```





```

SUBROUTINE SIMULT(RA1,RA2,RA3,RA4,RA5,RA6,RA7,RA8,RA9,
1A1,A2,A3,A4,A5,A6,A7,A8,A9,
2V,A,ND,TNCISE,TIME,P,REDUCE,NUMSEN)
INTEGR ND(4),NUMSEN
REAL RA1(1024),RA2(1024),RA3(1024),RA4(1024),RA5(1024),RA6(1024),
1RA7(1024),RA8(1024),RA9(1024),
2V(4),A(4),TNCISE,TIME(1024),P(9,4),REDUCE
COMPLEX A1(1024),A2(1024),A3(1024),A4(1024),A5(1024),
1A6(1024),A7(1024),A8(1024),A9(1024)
WRITE(6,10)
FORMAT(0),*ENTER THE FOUR SIMULATION FREQUENCIES-REAL-*
10 WRITE(6,11)
FORMAT(0),*ENTER FREQUENCY*
11 READ(10,12)V(1)
WRITE(6,11)
READ(10,12)V(2)
WRITE(6,11)
READ(10,12)V(3)
WRITE(6,11)
READ(10,12)V(4)
FORMAT(10,12)V(4)
12 READ(10,12)V(4)
FORMAT(10,12)V(4)
13 WRITE(6,13)
FORMAT(0),*ENTER AMPLITUDES FOR EACH FREQUENCY-REAL-*
14 WRITE(6,14)
FORMAT(0),*ENTER AMPLITUDE*
READ(10,15)A(1)
WRITE(6,14)
READ(10,15)A(2)
WRITE(6,14)
READ(10,15)A(3)
WRITE(6,14)
READ(10,15)A(4)
FORMAT(10,15)A(4)
15 WRITE(6,15)
FORMAT(10,15)A(4)
WRITE(6,16)
WRITE(6,18)
WRITE(6,19)
FORMAT(0),*ENTER TARGET ANGLE FOR EACH FREQUENCY-13-*
16 FORMAT(0),*SIX SENSORS ALLOWABLE ANGLES:0,60,120,180,240,300*
18 FORMAT(0),*FOR NINE SENSORS:0,40,80,120,160,200,240,280,320*
19 WRITE(6,17)
FORMAT(0),*ENTER ANGLE*
17 READ(10,15)ND(1)
WRITE(6,17)
READ(10,15)ND(2)
WRITE(6,17)
READ(10,15)ND(3)
WRITE(6,17)
READ(10,15)ND(4)
WRITE(6,17)

```













MF11143530  
MF11143540  
MF11143550  
MF11143560  
MF11143570  
MF11143580  
MF11143590  
MF11144000  
MF11144010  
MF11144020  
MF11144030  
MF11144040  
MF11144050  
MF11144060  
MF11144070  
MF11144080  
MF11144090  
MF11144100  
MF11144110  
MF11144120  
MF11144130  
MF11144140  
MF11144150  
MF11144160  
MF11144170  
MF11144180  
MF11144190  
MF11144200  
MF11144210  
MF11144220  
MF11144230  
MF11144240  
MF11144250  
MF11144260  
MF11144270  
MF11144280  
MF11144290  
MF11144300  
MF11144310  
MF11144320  
MF11144330  
MF11144340  
MF11144350  
MF11144360  
MF11144370  
MF11144380  
MF11144390  
MF11144400

94  
P(2,1) = -76.3  
P(3,1) = -21.3  
P(4,1) = 0.  
P(5,1) = -21.3  
P(6,1) = -76.7  
P(7,1) = -138.7  
P(8,1) = -180.  
P(9,1) = -180.  
IF((NC(I)).NE.(160)) GO TO 95  
P(1,1) = -180.  
P(2,1) = -138.7  
P(3,1) = -76.3  
P(4,1) = -21.3  
P(5,1) = 0.  
P(6,1) = -21.3  
P(7,1) = -76.7  
P(8,1) = -138.7  
P(9,1) = -180.  
IF((NC(I)).NE.(200)) GO TO 96  
P(1,1) = -180.  
P(2,1) = -138.7  
P(3,1) = -76.3  
P(4,1) = -21.3  
P(5,1) = 0.  
P(6,1) = -21.3  
P(7,1) = -76.7  
P(8,1) = -138.7  
P(9,1) = -180.  
IF((NC(I)).NE.(240)) GO TO 97  
P(1,1) = -138.7  
P(2,1) = -138.7  
P(3,1) = -180.  
P(4,1) = -138.7  
P(5,1) = -76.3  
P(6,1) = -21.3  
P(7,1) = -21.3  
P(8,1) = -76.7  
P(9,1) = -138.7  
IF((NC(I)).NE.(280)) GO TO 98  
P(1,1) = -76.7  
P(2,1) = -138.7  
P(3,1) = -180.  
P(4,1) = -180.  
P(5,1) = -138.7  
P(6,1) = -76.3  
P(7,1) = -21.3  
P(8,1) = -21.3  
P(9,1) = -76.7  
IF((NC(I)).NE.(280)) GO TO 98  
P(1,1) = -76.7  
P(2,1) = -138.7  
P(3,1) = -180.  
P(4,1) = -180.  
P(5,1) = -138.7  
P(6,1) = -76.3  
P(7,1) = -21.3  
P(8,1) = -21.3  
P(9,1) = -76.7



98

```

IF((AC(I)).NE.(320)) GO TO 41
P(1,I) = -21.3
P(2,I) = -76.7
P(3,I) = -138.7
P(4,I) = -180.
P(5,I) = -180.7
P(6,I) = -138.7
P(7,I) = -76.3
P(8,I) = -21.3
P(9,I) = 0.

```

C

ADDITION OF THE SIMULATED SIGNALS TO EACH SENSORS DATA

```

DO 2 J = 1,1024
  RA1(J) = RA1(J) + (A(I)*COS(2*PI*V(I))*TIME(J) + PP*P(1,I))
  RA2(J) = RA2(J) + (A(I)*COS(2*PI*V(I))*TIME(J) + PP*P(2,I))
  RA3(J) = RA3(J) + (A(I)*COS(2*PI*V(I))*TIME(J) + PP*P(3,I))
  RA4(J) = RA4(J) + (A(I)*COS(2*PI*V(I))*TIME(J) + PP*P(4,I))
  RA5(J) = RA5(J) + (A(I)*COS(2*PI*V(I))*TIME(J) + PP*P(5,I))
  RA6(J) = RA6(J) + (A(I)*COS(2*PI*V(I))*TIME(J) + PP*P(6,I))
  IF((NLMSEN).EQ.(6)) GO TO 2
  RA7(J) = RA7(J) + (A(I)*COS(2*PI*V(I))*TIME(J) + PP*P(7,I))
  RA8(J) = RA8(J) + (A(I)*COS(2*PI*V(I))*TIME(J) + PP*P(8,I))
  RA9(J) = RA9(J) + (A(I)*COS(2*PI*V(I))*TIME(J) + PP*P(9,I))
CONTINUE
CONTINUE

```

2

SUPPRESSION OR ENHANCEMENT OF SEISMIC SIGNALS ABOVE THE NOISE LEVEL

```

DO 3 K = 1,1024
  IF((AES(RA1(K)))<.GT.(TNOISE)) RA1(K) = RA1(K)/REDUCE
  IF((AES(RA2(K)))<.GT.(TNOISE)) RA2(K) = RA2(K)/REDUCE
  IF((AES(RA3(K)))<.GT.(TNOISE)) RA3(K) = RA3(K)/REDUCE
  IF((AES(RA4(K)))<.GT.(TNOISE)) RA4(K) = RA4(K)/REDUCE
  IF((AES(RA5(K)))<.GT.(TNOISE)) RA5(K) = RA5(K)/REDUCE
  IF((AES(RA6(K)))<.GT.(TNOISE)) RA6(K) = RA6(K)/REDUCE
  IF((NLMSEN).EQ.(6)) GO TO 3
  IF((AES(RA7(K)))<.GT.(TNOISE)) RA7(K) = RA7(K)/REDUCE
  IF((AES(RA8(K)))<.GT.(TNOISE)) RA8(K) = RA8(K)/REDUCE
  IF((AES(RA9(K)))<.GT.(TNOISE)) RA9(K) = RA9(K)/REDUCE
CONTINUE
DO 20 K1 = 1,1024
  ABC = 0.
  A1(K1) = CMPLX(RA1(K1),ABC)
  A2(K1) = CMPLX(RA2(K1),ABC)
  A3(K1) = CMPLX(RA3(K1),ABC)
  A4(K1) = CMPLX(RA4(K1),ABC)
  A5(K1) = CMPLX(RA5(K1),ABC)

```

3

```

MF114410
MF114420
MF114430
MF114440
MF114450
MF114460
MF114470
MF114480
MF114490
MF114500
MF114510
MF114520
MF114530
MF114540
MF114550
MF114560
MF114570
MF114580
MF114590
MF114600
MF114610
MF114620
MF114630
MF114640
MF114650
MF114660
MF114670
MF114680
MF114690
MF114700
MF114710
MF114720
MF114730
MF114740
MF114750
MF114760
MF114770
MF114780
MF114790
MF114800
MF114810
MF114820
MF114830
MF114840
MF114850
MF114860
MF114870
MF114880

```





```

20      A6(K1) = CMPLX(RA6(K1),AEC)
30      IF((NUMSEN).EQ.(6)) GO TO 20
      A7(K1) = CMPLX(RA7(K1),ABC)
      A8(K1) = CMPLX(RA8(K1),ABC)
      A9(K1) = CMPLX(RA9(K1),ABC)
      CONTINUE
      RETURN
      END
C
C      LEAST MEAN SQUARES POLYNOMIAL CURVE FITTING ALGORITHM
C
      SUBROUTINE LMS (NTAR,DIRC,NUMSEN,C,SCALE,TESTNC,TIME,NFRM,Y,
      1VX,X,T,INDEX,NCR,TRIX,B,WKAREA)
      DIMENSION TRIX(5,9),B(5),WKAREA(108)
      INTEGER NTAR(9),T(5),C,NHALF,MIN,NUMSEN,TESTNC,NFRM
      REAL P,FMIN,S,XS(16),X(9),A(9),Y(360),
      1VX(360),T(5),TIME(1024),DIRC,SCALE,C
C
C      FIND FIRST SENSOR TO MATCH THE INPUT SIGNAL
C
      MIN = NTAR(1)
      MARK = 1
      IF((NTAR(1)).LT.(1)) GO TO 66
      DO 57 I17 = 1,9
      1(I17) = 0
      1(I17) = 0
      WRITE(6,53) NTAR(I17)
      CONTINUE
      FCFORMAT(17) = 2,NUMSEN
      DO 11 I2 = 2,NUMSEN
      IF((NTAR(I2)).GE.(MIN)) GO TO 11
      MIN = NTAR(I2)
      MARK = I2
      CONTINUE
      DO 46 I8 = 1,360
      Y(I8) = C
      VX(I8) = 0.
      CONTINUE
      CENTER THE PARABOLA
      IF((MIN).EQ.(0)) GO TO 66
      DO 21 K1 = 1,NUMSEN
      INA = 1
      IF((NUMSEN).EQ.(6)) INA = 0
      N = NUMSEN/2 - MARK + K1 + INA
      IF((N).GT.(NUMSEN)) N = N - NUMSEN
      IF((N).LT.(1)) N = N + NUMSEN

```



```

21      T(N) = NTAR(K1)
      CONTINUE
      DO 41 L = 1, NUMSEN
      T(L) = T(L) - MIN
      T(L) = FLOAT(T(L))
41      CONTINUE
      DO 10 I2 = 1, 16
      XS(I2) = 0.
10      CONTINUE
      X(1) = C
      LN = NUMSEN - 1
      DO 130 I4 = 1, LN
      IF((NUMSEN).EQ.(6)) X(I4 + 1) = (FLCAT(I4*60))/360.
      IF((NUMSEN).EQ.(9)) X(I4 + 1) = (FLCAT(I4*40))/320.
130      CONTINUE
      C
      C
      C      LOAD THE MATRICES FOR THE LEAST MEAN SQUARES POLYNOMIAL SOLUTION
      C
      IF((NUMSEN.EQ.6) X(7) = 0
      IF((NUMSEN.EQ.6) X(8) = 0
      IF((NUMSEN.EQ.6) X(9) = 0
      NTC = 2*NUMSEN - 2
      DO 20 N1 = 1, NTC
      DO 30 K3 = 1, NUMSEN
      XS(N1) = X(K3)*N1 + XS(N1)
30      CONTINUE
20      CONTINUE
      DO 47 I2A = 1, 9
      DO 45 I3A = 1, 9
      CO 45 I3A = 1, 9
      CO 47 I2A = 1, 9
      TRINUE
49      CONTINUE
47      CONTINUE
      DO 50 I1 = 1, NUMSEN
      TRIX(1, I1) = NUMSEN
      DO 50 I2 = 2, NUMSEN
      TRIX(1, I2) = XS(N2 - 1)
50      CONTINUE
      DO 40 I2 = 1, NUMSEN
      TRIX(2, I2) = XS(I2) + 1)
      TRIX(3, I2) = XS(I2) + 2)
      TRIX(4, I2) = XS(I2) + 3)
      TRIX(5, I2) = XS(I2) + 4)
      TRIX(6, I2) = XS(I2) + 5)
      TRIX(7, I2) = XS(I2) + 6)
      TRIX(8, I2) = XS(I2) + 7)
      IF((NUMSEN).EQ.(6)) GC TC 40
      TRINUE
40      CONTINUE
      DO 60 I6 = 1, 9

```







```

120      PMIN = F
CONTINUE NUMSEN/2
NHALF = MIN1 + (MARK - INA)*CIVIDE
DIRC = 1, NUMSEN
DO 77 IB = 1, NUMSEN
  X(IB) = X(IB)*FLOAT(INDEX) + FLOAT(MARK - NUMSEN/2 - INA)*DIVIDE
CONTINUE
RETURN
ENC

C
C
C      OUTPUT PLCTTING FCR THE LEAST MEAN SQUARES SUBROUTINE
      SUBROUTINE PLT (C, SCALE, TESTNO, NUMSEN, TIME, YY, VXR, BX, TTB, INDEX,
1NOR, DIRC, NFRM)
      INTEGER C, TESTNO, INDEX, NCR, NFRM
      REAL YY(INDEX), TTB, NUMSEN, TIME(1024), SCALE
      IF((C).EQ.(1)) CALL CCMPRS
      IF((C).NE.(1)) CALL TEK618
      CALL PAGE(11.0, 8.5)
      CALL NCRDR (SCALE)
      CALL BLCKUP (SCALE)
      CALL AREA2C(9.0, 6.0)
      CALL FRAME
      CALL XNAME('ANGLE-DEGREES-', 14)
      CALL YNAME('RELATIVE DELAY TIMES', 20)
      CALL HEADING('LEAST MEAN SQUARES POLYNOMIAL', 25, 2.0, 1)
      CALL MESSAGE('EVENT NUMBER', 12, .25, .65)
      CALL INTC(TESTNO, 2.5, .65)
      CALL MESSAGE('DEGREE POLYNOMIAL', 17, .25, .45)
      CALL INTC(NOR, 2.5, .45)

C
      IF((NFRM).EQ.(0))CALL MESSAGE('INITIAL CIRECTION', 17, .25, .25)
      IF((NFRM).EQ.(0))CALL REALNO(DIRC, 2, 4, .25)
      IF((NFRM).NE.(0))CALL MESSAGE('TARGET TYPE', 11, .25, .25)
      IF((NFRM).EQ.(1))CALL MESSAGE('TRK VEH', 7, 2, .25)
      IF((NFRM).EQ.(2))CALL MESSAGE('WHL VEH', 8, 2, .25)
      IF((NFRM).EQ.(3))CALL MESSAGE('SHL BLST', 8, 2, .25)
      IF((NFRM).EQ.(4))CALL MESSAGE('HELD', 4, 2, .25)
      IF((NFRM).EQ.(5))CALL MESSAGE('PERS', 4, 2, .25, .25)
      CALL MESSAGE('PERIOD(SEC)', 16, .25, .05)
      S = FLCCAT('FIX(TIME(1024) + 1.))
      F = FLCCAT('S, 2, 4, .05)
      CALL REALNO(S, 2, 4, .05)
      CALL REALNO(F, 2, 3, .2, .05)
      CALL MESSAGE('ACTUAL SENSOR DATA ARE INDICATED', 52, 2.5, 5.7)
      CALL MESSAGE('BY MARKER SYMBOLS', 17, 3.3, 5.5)
      CALL INTX

```

MF1116330  
MF1116340  
MF1116350  
MF1116360  
MF1116370  
MF1116380  
MF1116390  
MF1116400  
MF1116410  
MF1116420  
MF1116430  
MF1116440  
MF1116450  
MF1116460  
MF1116470  
MF1116480  
MF1116490  
MF1116500  
MF1116510  
MF1116520  
MF1116530  
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MF1116550  
MF1116560  
MF1116570  
MF1116580  
MF1116590  
MF1116600  
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MF1116620  
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MF1116670  
MF1116680  
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MF1116720  
MF1116730  
MF1116740  
MF1116750  
MF1116760  
MF1116770  
MF1116780  
MF1116790  
MF1116800









## LIST OF REFERENCES

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Multiple target identification and direction finding using matched filtering techniques.

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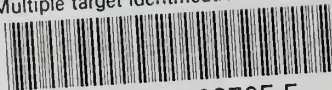
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